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Low-Speed Aerodynamic Characteristics of a 1/8-Scale X-29A Airplane Model at High Angles of Attack and Sideslip

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SUMMARY

A 1/8-scale model of the X-29A airplane was tested in the Ames 12-Foot Pressure Wind Tunnel at a Mach number of 0.20 and Reynolds numbers of 0.13×10^6 to 2.00×10^6 based on a fuselage forebody depth of 0.4 ft. For the test series presented herein, the angle of attack ranged from 40° to 90° and the angle of sideslip ranged from -10° to 30° for the erect attitude. Tests with the model inverted covered angles of attack from -40° to -90° and angles of sideslip from -30° to 10° . Data were obtained for the basic design and for several forebody strakes. An alternate forebody design was also tested. The results provided information for selection of forebody strakes for compensation of Reynolds number effect on the 1/25-scale free-spinning model tested in the Langley Spin Tunnel.

INTRODUCTION

Reynolds number effects on the high angle of attack, crossflow characteristics of a fuselage forebody on a small-scale model can cause appreciably different side forces, yawing moments, and pitching moments from those obtained on a full-scale airplane. (See refs. 1 and 2.) In the course of conducting free-spinning investigations in the Langley Spin Tunnel on small-scale models, the Reynolds number effects for some configurations have been so marked that the spin recovery characteristics determined from model tests were not representative of the full-scale airplane. The F-5A airplane, which has essentially the same forebody as the X-29A, exhibited these effects. (See ref. 3.)

Spinning is an aerodynamic phenomenon in which dynamic forces and moments are extremely important. Methods for the prediction of Reynolds number effects on dynamic data are, however, very limited at best, so experimental methods are employed to develop the necessary information. Typically, a wind-tunnel Reynolds number investigation is conducted to determine whether there are Reynolds number effects on the static data which could significantly influence the spin-tunnel results. When such effects are identified, various forebody modifications are tested on the model in an attempt to make the pertinent data at low Reynolds numbers representative of data at high Reynolds numbers. Such information is then used to design a forebody modification to be used on the spin-tunnel model.

In this investigation, a 1/8-scale X-29A forward-swept-wing airplane model was tested in the Ames 12-Foot Pressure Wind Tunnel to determine static longitudinal and lateral-directional aerodynamic characteristics over a range of Reynolds number from subcritical to supercritical conditions. The angle-of-attack ranges tested were 40° to 90° and -40° to -90° . The corresponding angle-of-sideslip ranges tested were -10° to 30° and 10° to -30° , respectively.

The approach used in this study was to identify the Reynolds number effects on the basic configurations and then to conduct tests using the component buildup technique to isolate the source of the effects. On the basis of this information, tests were conducted on various forebody modifications, including strakes and an alternate forebody shape, to give the desired results. The data are presented with minimum analysis and discussion.

SYMBOLS

BL		butt-line station
C_A		body-axis axial-force coefficient
C_l		body-axis rolling-moment coefficient
C_m		pitching-moment coefficient
C_N		body-axis normal-force coefficient
C_n		body-axis yawing-moment coefficient
C_Y		body-axis side-force coefficient
\bar{c}		wing reference chord, in.
FS		fuselage station
L,R		left, right
q	(Q in computer-generated appendix)	dynamic pressure, psf
R_N	(RN in computer-generated appendix)	Reynolds number per foot
\bar{V}		free-stream velocity
WL		waterline station
x,y,z		body axes
α	(ALPHA in computer-generated appendix)	angle of attack, deg
β	(BETA in computer-generated appendix)	angle of sideslip, deg
δ_a		left or right flaperon deflection, deg
δ_c		left or right canard deflection, deg
δ_R		rudder deflection, deg
δ_s		strake flap deflection, deg

TEST FACILITY

The Ames 12-Foot Pressure Wind Tunnel is a variable-density, low-turbulence, continuous-flow wind tunnel that operates in the Mach number range of 0.10 to 0.94. The wind tunnel is powered by a two-stage, axial-flow fan driven by electric motors

totaling 12 000 hp. Airspeed in the test section is controlled by varying the rotation speed of the fan. Eight fine-mesh screens in the settling chamber, together with a contraction ratio of 25:1, provide an airstream of exceptionally low turbulence level.

MODEL DESCRIPTION

The model was a 1/8-scale version of the X-29A airplane. The geometry of the model is given in table I and figure 1, and model-sting installation is shown in figure 2. Details of the forebody strakes are shown in figures 3 and 4, and the alternate forebody is shown in figure 5. Photographs of the model are shown in figure 6.

The X-29A airplane is a forward-swept-wing flight-demonstrator aircraft designed by the Grumman Aerospace Corporation for the Defense Advanced Research Projects Agency. In addition to incorporating a forward wing sweep of 29.3° , geometric features include horizontal canard control surfaces capable of symmetric and asymmetric deflections of the left- and right-hand surfaces; twin side-mounted external compression inlets with a bifurcated internal-flow duct feeding a single engine with the engine nozzle at the rear of the fuselage; strakes mounted on the side of the fuselage aft of the wing-body juncture, including trailing-edge deflectable strake flaps; single centerline-mounted vertical tail and rudder; and wing trailing-edge flaps, flaperons, and ailerons. The canards, rudder, fuselage strakes, and wing trailing-edge flaps on the model have deflection capabilities for determining the control effectiveness of these surfaces. The canards incorporate independent remote-control actuation for deflections ranging from -60° to $+30^\circ$. The cruise wing trailing edge incorporates double-hinged ailerons and flaperons, and control-surface deflections are variable as a result of using common-flap-segment hardware. Simulated flap actuator fairings provide structural support for the control surfaces. Individual mounting brackets are used to provide rudder and strake flap deflection capability.

The cruise and maneuver wings have common geometries from the root out to BL 64 (39-percent span), with the exception that the maneuver wing has a smooth cambered trailing edge. The outboard panels of the cruise and maneuver wings differ only in twist and trailing-edge design.

Boundary-layer transition strips were not applied for this test. The forward fuselage section is removable at FS 283 and was modified to incorporate Langley designed lateral and ventral strakes. Model mounting at the aft end required a deviation from the true aircraft contours to accommodate the sting.

INSTRUMENTATION

Model forces and moments were measured with a six-component strain-gage balance. Prior to the test, static loads in each plane and combined static loads were applied to the balance to simulate the range of loads and center-of-pressure locations anticipated during the test. Remote actuation of the canards was accomplished by means of a control console located in the tunnel control room and two standard feedback potentiometers (one per canard) mounted within the model. Potentiometer output

was indicated on a digital voltmeter in the control console. An angle-of-attack transmitter was installed within the model and was used for primary angle-of-attack measurements.

TESTING AND PROCEDURE

The investigation was performed at a Mach number of 0.20 over a range of fuselage-forebody depth Reynolds numbers from 0.13×10^6 to 2.00×10^6 . Data were obtained at angles of attack from 40° to 90° and at angles of sideslip from -10° to 30° , with the model erect and rolled 180° .

Forces and moments were sensed by an internally mounted six-component strain-gage balance. No axial-force corrections were applied for base and cavity pressure. An angle transducer mounted on the support system was used to measure model angles of attack. The effects of control-surface deflections were investigated.

DATA REDUCTION

The six-component force and moment data were reduced about the model moment reference center in the body-axis system. The axis system is defined in figure 7, and the moment reference center was at $-0.05\bar{c}$, FS 56.78, WL 8.25, BL 0 (full scale: FS 454.27, WL 66, BL 0). The balance center was at FS 56.78, WL 8.96, BL 0. The model was sting-mounted on a turntable in the test-section floor; therefore, angle of attack and angle of sideslip could be varied. For any specific sting-support arrangement, the model angle of attack could be varied 50° , and angle of sideslip could be varied 40° . Angle-of-attack measurements were made using an angle-of-attack transmitter mounted in the model and a tilt sensor mounted on the base of the support system. Angle-of-sideslip measurements were made using a potentiometer to measure turntable rotation angle. Computed angles included corrections to account for elastic deflection of the balance and sting.

For these tests, the model ducts were blocked, so that no airflow passed through the inlets or duct exit. Also, because no measurements were made of base or cavity pressure, no adjustments were made to the measured data to account for any effects due to these pressures. These tests were conducted with natural boundary-layer transition; that is, transition was not induced artificially.

Although it is known that large flow angles are induced by the turntable bump (fig. 2), no attempt was made to assess these flow angles, and no flow-angle corrections were made to the test results. Using the method described in reference 4, angle of attack and the longitudinal aerodynamic coefficients were corrected for the effects of tunnel-wall interference.

Blockage corrections based on the methods described in references 5 and 6 were computed and applied to determine corrected free-stream Mach number and dynamic pressure. For large angles, the blockage corrections include not only the incremental effects of model volume, model support-system drag, and model zero-lift drag but also an increment due to the separated wake as computed by the method of reference 6. These blockage corrections were applied to clear-tunnel calibrations based on the measurement of settling-chamber total pressure and wall static pressure upstream of the location of the model in the test section.

RESULTS AND DISCUSSION

Presentation of Data

To expedite publishing the results of the investigation, the data are presented with limited analysis. The model attitude schedules and an outline of the associated data run schedules are presented in tables II and III, respectively. Selected data are presented in figures 8 and 9 for the baseline configuration, in figures 10 and 11 for the forebody modifications, in figures 12 and 13 for negative angles of attack, and in figures 14 through 17 for the component buildup. The complete test results are tabulated in the appendix.

Longitudinal Characteristics

Figure 8 shows the effects of Reynolds number variation on the longitudinal characteristics of the basic configuration. Some effect on normal-force coefficient is observed, but much more significant changes are apparent in the pitching-moment-coefficient data. This effect consists of large positive increments of pitching-moment coefficients above approximately $\alpha \approx 50^\circ$ for the low Reynolds number tests compared with the data for the high Reynolds number tests. For most canard deflections, this pitching-moment increment is sufficiently large to produce a change in sign of the model pitching-moment coefficient. The change in the data from low Reynolds number behavior to high Reynolds number behavior occurs between $R_N = 0.6 \times 10^6$ and 0.9×10^6 per foot.

Results of component buildup tests with fuselage and canards (fig. 14) and fuselage alone (fig. 16) show similar effects of Reynolds number to those for the complete model. These effects indicate that the fuselage is the source of the observed phenomenon.

Lateral-Directional Characteristics

Figure 9 shows the effects of Reynolds number variation on the lateral-directional characteristics for the basic configuration at angles of attack from 40° to 90° . The data show that the rolling-moment coefficient is relatively insensitive to Reynolds number; however, the side-force and yawing-moment coefficients are greatly affected above $\alpha = 50^\circ$. For spin analysis, the yawing-moment coefficient is the more significant parameter. Except for the lowest Reynolds number tests, the slope of C_n versus β is negative through zero sideslip from $\alpha = 50^\circ$ to 75° . (See figs. 9(a) through 9(f).) At $\alpha = 80^\circ$ and 85° (figs. 9(g) and 9(h) and appendix), the change in slope of C_n versus β from positive to negative occurs between Reynolds numbers of about 1.3 and 2.2×10^6 per foot. The side-force and yawing-moment data for component tests shown in figure 15 (body plus canard) and in figures 16 and 17 (body alone) are more erratic, which indicates interactions between the various components.

Forebody Modifications

Dynamic free-spinning tests are conducted at low Reynolds numbers. When investigations such as reported herein indicate significant Reynolds number effects at high angles of attack, particularly on yawing-moment data, an attempt is made to

modify the model to compensate for these effects. From past experience, typical modifications consist of strakes attached to the forebody. For this test series, in addition to evaluating several forebody strake configurations, an alternate forebody shape was designed based on the two-dimensional work of Polhamus (ref. 2). This alternate forebody shape was expected to exhibit the desired characteristics.

Figures 10 and 11 show the test results for the forebody modifications at low Reynolds number compared with the baseline configuration at high Reynolds number. Plots of yawing-moment coefficient versus sideslip show that the ventral strake is effective at all angles of attack tested. The alternate forebody provides a reasonable match at $\alpha > 70^\circ$, and the lateral strake performs acceptably at $\alpha > 80^\circ$. The pitching-moment coefficient is also best matched by the ventral strake. The alternate forebody is less satisfactory but is much better than the angled or lateral strakes.

Negative Angle of Attack

Figures 12 and 13 present the results of Reynolds number variation on the baseline configuration for high negative angles of attack. Effects analogous to those observed in the positive high-angle-of-attack tests are shown. The increments in pitching-moment coefficient at low Reynolds number are slightly smaller beyond $\alpha = -65^\circ$ than those for the high Reynolds number data. The reversals in the slope of C_n versus sideslip data at low Reynolds number are evident at $\alpha = -80^\circ$ and -60° . (See figs. 13(a) and 13(b).) Forebody modifications were not tested at negative angles of attack.

CONCLUSIONS

Results of wind-tunnel tests of a 1/8-scale model of the X-29A airplane at high positive and negative angles of attack in the Ames 12-Foot Pressure Wind Tunnel have led to the following observations:

1. Significant Reynolds number effects on pitching-moment characteristics are observed above 50° angle of attack. The fuselage is the primary source of these effects.
2. Significant Reynolds number effects on yawing-moment characteristics are observed above 50° angle of attack.
3. A ventral strake mounted on the forebody produces results at low Reynolds number similar to those obtained for the baseline configuration at high Reynolds number.
4. Reynolds number effects on pitching and yawing moments at high negative angles of attack are analogous to those observed at high positive angles of attack.

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TABLE I.- DIMENSIONAL DATA

	Airplane	Model
Length, ft	48	6
Wing:		
Reference area, ft ²	185	2.89
Exposed area, ft ²	160	3.50
Span, ft	27.2	3.4
Aspect ratio	4.0	4.0
Mean aerodynamic chord, in.	86.6	10.83
Leading-edge sweep, deg	-29.27	-29.27
1/4-chord sweep, deg	-33.73	-33.73
Taper ratio	0.4	0.4
Airfoil section:		
Root chord thickness, percent	6.7	6.7
Root thickness (side of body), percent	6.2	6.2
Tip chord thickness, percent	5.0	5.0
Canard:		
Reference area, ft ²	37.00	0.58
Aspect ratio	1.47	1.47
Leading-edge sweep, deg	42	42
1/4-chord sweep, deg	23.08	23.08
Taper ratio	0.319	0.319
Airfoil section:		
Root chord thickness, percent	5	5
Tip chord thickness, percent	3.5	3.5
Vertical tail:		
Reference area, ft ²	34	0.53
Aspect ratio	2.68	2.68
Leading-edge sweep, deg	47	47
Taper ratio	0.30	0.30
Airfoil section:		
Root chord thickness, percent	4	4
Tip chord thickness, percent	4	4

TABLE II.- MODEL ATTITUDE SCHEDULES

[See table III]

Schedule	α , deg	β , deg
A1	40, 50, 60, 65, 70, 75, 80, 85, 90	
A2	40, 50, 60, 70, 80, 90	
A3	-40, -50, -60, -70, -80, -90	
A4	-40, -50, -60, -65, -70, -75, -80, -85, -90	
B1		-10, -8, -4, 0, 4, 8, 10, 15, 20, 30
B2		-10, -5, 0, 5, 10, 15, 20
B3		10, 8, 4, 0, -4, -8, -10, -15, -20, -30

TABLE III.- RUN SCHEDULE

Run	R_N , per foot	α	β	δ_c , deg	δ_a , deg	δ_s , deg	δ_R , deg	Configuration
6	Atm	A2	0	Off	0	0	0	Canards off
7	↓	40	B2	↓	↓	↓	↓	↓
8	↓	60	B2	↓	↓	↓	↓	↓
9	3.0×10^6	A2	0	↓	↓	↓	↓	↓
10	↓	40	B2	↓	↓	↓	↓	↓
11	↓	60	B2	↓	↓	↓	↓	↓
12	↓	80	B2	↓	↓	↓	↓	↓
13	5.0×10^6	A2	0	↓	↓	↓	↓	↓
14	↓	80	B2	↓	↓	↓	↓	↓
15	↓	60	B2	↓	↓	↓	↓	↓
16	↓	40	B2	↓	↓	↓	↓	↓
17	Atm	A2	0	↓	↓	↓	↓	↓
18	↓	80	B2	↓	↓	↓	↓	↓
19	↓	60	B2	↓	↓	↓	↓	↓
20	↓	40	B2	↓	↓	↓	↓	↓
21	↓	A1	0	-60	25	30	↓	Baseline
22	↓	40	B1	↓	↓	↓	↓	↓
23	↓	50	↓	↓	↓	↓	↓	↓
24	↓	60	↓	↓	↓	↓	↓	↓
25	↓	65	↓	↓	↓	↓	↓	↓
26	↓	70	↓	↓	↓	↓	↓	↓
27	↓	75	↓	↓	↓	↓	↓	↓
28	↓	80	↓	↓	↓	↓	↓	↓
29	↓	85	↓	↓	↓	↓	↓	↓
30	↓	90	↓	↓	↓	↓	↓	↓
31	↓	A1	25	↓	↓	↓	↓	↓
32	↓	A2	0	-40	↓	↓	↓	↓
33	↓	90	B1	↓	↓	↓	↓	↓
34	↓	85	↓	↓	↓	↓	↓	↓
35	↓	80	↓	↓	↓	↓	↓	↓
36	↓	75	↓	↓	↓	↓	↓	↓
37	↓	70	↓	↓	↓	↓	↓	↓
38	↓	65	↓	↓	↓	↓	↓	↓
39	↓	60	↓	↓	↓	↓	↓	↓
40	↓	50	↓	↓	↓	↓	↓	↓
41	↓	40	↓	↓	↓	↓	↓	↓
42	↓	A2	0	-25	↓	↓	↓	↓
43	↓	90	B1	↓	↓	↓	↓	↓
44	↓	85	↓	↓	↓	↓	↓	↓
45	↓	80	↓	↓	↓	↓	↓	↓
46	↓	75	↓	↓	↓	↓	↓	↓
47	↓	70	↓	↓	↓	↓	↓	↓
48	↓	65	↓	↓	↓	↓	↓	↓
49	↓	60	↓	↓	↓	↓	↓	↓
50	↓	50	↓	↓	↓	↓	↓	↓
51	↓	40	↓	↓	↓	↓	↓	↓

TABLE III.- Continued

Run	R_N , per foot	α	β	δ_c , deg	δ_a , deg	δ_s , deg	δ_R , deg	Configuration
52	Atm	A2	0	-20	25	30	0	Baseline
53	↓	90	B1	↓	↓	↓	↓	↓
54	↓	85	↓	↓	↓	↓	↓	↓
55	↓	80	↓	↓	↓	↓	↓	↓
56	↓	75	↓	↓	↓	↓	↓	↓
57	↓	70	↓	↓	↓	↓	↓	↓
58	↓	65	↓	↓	↓	↓	↓	↓
59	↓	60	↓	↓	↓	↓	↓	↓
60	↓	50	↓	↓	↓	↓	↓	↓
61	↓	40	↓	↓	↓	↓	↓	↓
62	5.0×10^6	A2	0	-60	↓	↓	↓	↓
63	↓	90	B1	↓	↓	↓	↓	↓
64	↓	85	↓	↓	↓	↓	↓	↓
65	↓	80	↓	↓	↓	↓	↓	↓
66	↓	75	↓	↓	↓	↓	↓	↓
67	↓	70	↓	↓	↓	↓	↓	↓
68	↓	65	↓	↓	↓	↓	↓	↓
69	↓	60	↓	↓	↓	↓	↓	↓
70	↓	50	↓	↓	↓	↓	↓	↓
71	↓	40	↓	↓	↓	↓	↓	↓
72	↓	A2	0	-40	↓	↓	↓	↓
73	↓	90	B1	↓	↓	↓	↓	↓
74	↓	85	↓	↓	↓	↓	↓	↓
75	↓	80	↓	↓	↓	↓	↓	↓
76	↓	75	↓	↓	↓	↓	↓	↓
77	↓	70	↓	↓	↓	↓	↓	↓
78	↓	65	↓	↓	↓	↓	↓	↓
79	↓	60	↓	↓	↓	↓	↓	↓
80	↓	50	↓	↓	↓	↓	↓	↓
81	↓	40	↓	↓	↓	↓	↓	↓
82	↓	A2	0	-20	↓	↓	↓	↓
83	↓	90	B1	↓	↓	↓	↓	↓
84	↓	85	↓	↓	↓	↓	↓	↓
85	↓	80	↓	↓	↓	↓	↓	↓
86	↓	75	↓	↓	↓	↓	↓	↓
87	↓	70	↓	↓	↓	↓	↓	↓
88	↓	65	↓	↓	↓	↓	↓	↓
89	↓	60	↓	↓	↓	↓	↓	↓
90	↓	50	↓	↓	↓	↓	↓	↓
91	↓	40	↓	↓	↓	↓	↓	↓
92	3.4×10^6	A2	0	-60	↓	↓	↓	↓
93	↓	90	B1	↓	↓	↓	↓	↓
94	↓	85	↓	↓	↓	↓	↓	↓
95	↓	80	↓	↓	↓	↓	↓	↓
96	↓	75	↓	↓	↓	↓	↓	↓
97	↓	70	↓	↓	↓	↓	↓	↓

TABLE III.- Continued

Run	R_N , per foot	α	β	δ_c , deg	δ_a , deg	δ_s , deg	δ_R , deg	Configuration
98	3.4×10^6	65	B1	-60	25	30	0	Baseline
99	↓	60	↓	↓	↓	↓	↓	↓
100	↓	50	↓	↓	↓	↓	↓	↓
101	↓	40	↓	↓	↓	↓	↓	↓
102	2.2×10^6	A2	0	↓	↓	↓	↓	↓
103	↓	90	B1	↓	↓	↓	↓	↓
104	↓	85	↓	↓	↓	↓	↓	↓
105	↓	80	↓	↓	↓	↓	↓	↓
106	↓	75	↓	↓	↓	↓	↓	↓
107	↓	70	↓	↓	↓	↓	↓	↓
108	↓	65	↓	↓	↓	↓	↓	↓
109	↓	60	↓	↓	↓	↓	↓	↓
110	↓	50	↓	↓	↓	↓	↓	↓
111	↓	40	↓	↓	↓	↓	↓	↓
112	Atm	A2	0	↓	↓	↓	↓	↓
113	Atm	40	B1	↓	↓	↓	↓	↓
114	0.35×10^6	A2	0	↓	↓	↓	↓	↓
115	↓	90	B1	↓	↓	↓	↓	↓
116	↓	85	↓	↓	↓	↓	↓	↓
117	↓	80	↓	↓	↓	↓	↓	↓
118	↓	75	↓	↓	↓	↓	↓	↓
119	↓	70	↓	↓	↓	↓	↓	↓
120	↓	65	↓	↓	↓	↓	↓	↓
121	↓	60	↓	↓	↓	↓	↓	↓
122	↓	50	↓	↓	↓	↓	↓	↓
123	↓	40	↓	↓	↓	↓	↓	↓
124	↓	A2	0	↓	↓	↓	↓	↓
125	↓	A2	0	-40	↓	↓	↓	↓
126	↓	40	B1	↓	↓	↓	↓	↓
127	↓	50	↓	↓	↓	↓	↓	↓
128	↓	60	↓	↓	↓	↓	↓	↓
129	↓	65	↓	↓	↓	↓	↓	↓
130	↓	70	↓	↓	↓	↓	↓	↓
131	↓	75	↓	↓	↓	↓	↓	↓
132	↓	80	↓	↓	↓	↓	↓	↓
133	↓	85	↓	↓	↓	↓	↓	↓
134	↓	90	↓	↓	↓	↓	↓	↓
135	↓	A2	0	-20	↓	↓	↓	↓
136	↓	90	B1	↓	↓	↓	↓	↓
137	↓	85	↓	↓	↓	↓	↓	↓
138	↓	80	↓	↓	↓	↓	↓	↓
139	↓	75	↓	↓	↓	↓	↓	↓
140	↓	70	↓	↓	↓	↓	↓	↓
141	↓	65	↓	↓	↓	↓	↓	↓
142	↓	60	↓	↓	↓	↓	↓	↓
143	↓	50	↓	↓	↓	↓	↓	↓

TABLE III.- Continued

Run	R_N , per foot	α	β	δ_c , deg	δ_a , deg	δ_s , deg	δ_R , deg	Configuration
144	0.35×10^6	40	B1	-20	25	30	0	Baseline
145	0.6×10^6	A2	0	-60				
146		90	B1					
147		85						
148		80						
149		75						
150		70						
151		65						
152		60						
153		50						
154		40						
155	0.9×10^6	A2	0					
156		90	B1					
157		85						
158		80						
159		75						
160		70						
161		65						
162		60						
163		50						
164		40						
165	1.1×10^6	A2	0					
166		90	B1					
167		85						
168		80						
169		75						
170		70						
171		65						
172		60						
173		50						
174		40						
175	0.6×10^6	A2	0					Ventral strake (A) on
176		90	B1					
177		85						
178		80						
179		75						
180		70						
181		65						
182		60						
183		50						
184		40						
185		A2	0					Angled strake (C) on
186		90	B1					
187		85						
188		80						
189		75						

TABLE III.- Continued

Run	R_N , per foot	α	β	δ_c , deg	δ_a , deg	δ_s , deg	δ_R , deg	Configuration
190	0.6×10^6 ↓	70	Bl	-60	25	30	0	Angled strake (C) on
191		65	↓	↓	↓	↓	↓	↓
192		60	↓	↓	↓	↓	↓	↓
193		50	↓	↓	↓	↓	↓	↓
194		40	↓	↓	↓	↓	↓	↓
195		A2	0	↓	↓	↓	↓	Lateral strake (B) on
196		90	Bl	↓	↓	↓	↓	↓
197		85	↓	↓	↓	↓	↓	↓
198		80	↓	↓	↓	↓	↓	↓
199		75	↓	↓	↓	↓	↓	↓
200		70	↓	↓	↓	↓	↓	↓
201		65	↓	↓	↓	↓	↓	↓
202		60	↓	↓	↓	↓	↓	↓
203		50	↓	↓	↓	↓	↓	↓
204		40	↓	↓	↓	↓	↓	↓
205		A1	0	↓	↓	↓	↓	Nose strake off
206		90	Bl	↓	↓	↓	↓	↓
207		85	↓	↓	↓	↓	↓	↓
208		80	↓	↓	↓	↓	↓	↓
209		75	↓	↓	↓	↓	↓	↓
210		70	↓	↓	↓	↓	↓	↓
211		65	↓	↓	↓	↓	↓	↓
212		60	↓	↓	↓	↓	↓	↓
213		50	↓	↓	↓	↓	↓	↓
214		40	↓	↓	↓	↓	↓	↓
215		A1	0	↓	↓	↓	↓	Alternate forebody
216		90	Bl	↓	↓	↓	↓	↓
217		85	↓	↓	↓	↓	↓	↓
218		80	↓	↓	↓	↓	↓	↓
219		75	↓	↓	↓	↓	↓	↓
220		70	↓	↓	↓	↓	↓	↓
221		65	↓	↓	↓	↓	↓	↓
222		60	↓	↓	↓	↓	↓	↓
223		50	↓	↓	↓	↓	↓	↓
224		40	↓	↓	↓	↓	↓	↓
225	2.2×10^6 ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓ ↓	A2	0	↓	↓	↓	↓	Nose strake off
226		90	Bl	↓	↓	↓	↓	↓
227		85	↓	↓	↓	↓	↓	↓
228		80	↓	↓	↓	↓	↓	↓
229		75	↓	↓	↓	↓	↓	↓
230		70	↓	↓	↓	↓	↓	↓
231		65	↓	↓	↓	↓	↓	↓
232		60	↓	↓	↓	↓	↓	↓
233		50	↓	↓	↓	↓	↓	↓
234		40	↓	↓	↓	↓	↓	↓
235		A2	0	↓	↓	↓	-30	Baseline

TABLE III.- Continued

Run	R_N , per foot	α	β	δ_c , deg	δ_a , deg	δ_s , deg	δ_R , deg	Configuration
236	2.2×10^6	90	B1	-60	25	30	-30	Baseline
237	↓	85	↓	↓	↓	↓	↓	
238	↓	80	↓	↓	↓	↓	↓	
239	↓	75	↓	↓	↓	↓	↓	
240	↓	70	↓	↓	↓	↓	↓	
241	↓	65	↓	↓	↓	↓	↓	
242	↓	60	↓	↓	↓	↓	↓	
243	↓	50	↓	↓	↓	↓	↓	
244	↓	40	↓	↓	↓	↓	↓	
245	↓	A1	0	↓	↓	0	0	
246	↓	↓	↓	-40	↓	↓	↓	
247	↓	↓	↓	-20	↓	↓	↓	
248	0.6×10^6	↓	↓	-20	↓	↓	↓	
249	↓	↓	↓	-40	↓	↓	↓	
250	↓	↓	↓	-60	↓	↓	↓	
251	2.2×10^6	↓	↓	-60	10	↓	↓	
252	↓	↓	↓	-40	↓	↓	↓	
253	↓	↓	↓	-20	↓	↓	↓	
254	0.6×10^6	↓	↓	-20	↓	↓	↓	
255	↓	↓	↓	-40	↓	↓	↓	
256	↓	↓	↓	-60	↓	↓	↓	
257	2.2×10^6	↓	↓	-60	0	↓	↓	
258	↓	↓	↓	-40	↓	↓	↓	
259	↓	↓	↓	-20	↓	↓	↓	
260	0.6×10^6	↓	↓	-20	↓	↓	↓	
261	↓	↓	↓	-40	↓	↓	↓	
262	↓	↓	↓	-60	↓	↓	↓	
263	2.2×10^6	A2	↓	↓	25L -10R	30	↓	
264	↓	80	B1	↓	↓	↓	↓	
265	↓	60	↓	↓	↓	↓	↓	
266	↓	50	↓	↓	↓	↓	↓	
267	↓	40	↓	↓	↓	↓	↓	
268	↓	A2	0	-45L -5R	25	↓	↓	
269	↓	80	B1	↓	↓	↓	↓	
270	↓	60	↓	↓	↓	↓	↓	
271	↓	40	↓	↓	↓	↓	↓	
272	0.6×10^6	A2	0	↓	↓	↓	↓	
273	↓	80	B1	↓	↓	↓	↓	
274	↓	60	↓	↓	↓	↓	↓	
275	↓	40	↓	↓	↓	↓	↓	
276	2.2×10^6	40	↓	0	↓	↓	↓	
277	↓	50	↓	↓	↓	↓	↓	
278	↓	A2	0	↓	↓	↓	↓	
279	↓	90	B1	↓	↓	↓	↓	

TABLE III.- Continued

Run	R_N , per foot	α	β	δ_c , deg	δ_a , deg	δ_s , deg	δ_R , deg	Configuration
280	2.2×10^6	85	B1	0	25	30	0	Baseline
281	↓	80	↓	↓	↓	↓	↓	
282	↓	75	↓	↓	↓	↓	↓	
283	↓	70	↓	↓	↓	↓	↓	
284	↓	65	↓	↓	↓	↓	↓	
285	↓	60	↓	↓	↓	↓	↓	
286	Atm	A1	0	↓	↓	↓	↓	
287	0.6×10^6	A2	0	↓	↓	↓	↓	
288	↓	90	B1	↓	↓	↓	↓	
289	↓	85	↓	↓	↓	↓	↓	
290	↓	80	↓	↓	↓	↓	↓	
291	↓	75	↓	↓	↓	↓	↓	
292	↓	70	↓	↓	↓	↓	↓	
293	↓	65	↓	↓	↓	↓	↓	
294	↓	60	↓	↓	↓	↓	↓	
295	↓	50	↓	↓	↓	↓	↓	
296	↓	40	↓	↓	↓	↓	↓	
299	3.4×10^6	A3	0	0	-10	-30	↓	
300	↓	-80	B3	↓	↓	↓	↓	
301	↓	-60	↓	↓	↓	↓	↓	
302	↓	-40	↓	↓	↓	↓	↓	
303	↓	A3	0	30	↓	↓	↓	
304	↓	-80	B3	↓	↓	↓	↓	
305	↓	-60	↓	↓	↓	↓	↓	
306	↓	-40	↓	↓	↓	↓	↓	
307	5.0×10^6	A3	0	↓	↓	↓	↓	
308	↓	-80	B3	↓	↓	↓	↓	
309	↓	-60	↓	↓	↓	↓	↓	
310	↓	-40	↓	↓	↓	↓	↓	
311	↓	A3	0	0	↓	↓	↓	
312	↓	-80	B3	↓	↓	↓	↓	
313	↓	-60	↓	↓	↓	↓	↓	
314	↓	-40	↓	↓	↓	↓	↓	
315	Atm	A3	0	↓	↓	↓	↓	
316	↓	-80	B3	↓	↓	↓	↓	
317	↓	-60	↓	↓	↓	↓	↓	
318	↓	-40	↓	↓	↓	↓	↓	
319	↓	A3	0	30	↓	↓	↓	
320	↓	-80	B3	↓	↓	↓	↓	
321	↓	-60	↓	↓	↓	↓	↓	
322	↓	-40	↓	↓	↓	↓	↓	
323	0.6×10^6	A3	0	↓	↓	↓	↓	
324	↓	-80	B3	↓	↓	↓	↓	
325	↓	-60	↓	↓	↓	↓	↓	
326	↓	-40	↓	↓	↓	↓	↓	
327	↓	A3	0	0	↓	↓	↓	

TABLE III.- Continued

Run,	R_N , per foot	α	β	δ_c , deg	δ_a , deg	δ_s , deg	δ_R , deg	Configuration
328	0.6×10^6	-80	B3	0	-10	-30	0	Baseline
329	↓	-60	↓	↓	↓	↓	↓	
330	↓	-40	↓	↓	↓	↓	↓	
331	0.35×10^6	A3	0	↓	↓	↓	↓	
332	0.35×10^6	↓	↓	30	↓	↓	↓	
333	Atm	↓	↓	↓	↓	↓	-30	
334	↓	-80	B3	↓	↓	↓	↓	
335	↓	-60	↓	↓	↓	↓	↓	
336	↓	-40	↓	↓	↓	↓	↓	
337	0.6×10^6	A3	0	↓	↓	↓	↓	
338	↓	-80	B3	↓	↓	↓	↓	
339	↓	-60	↓	↓	↓	↓	↓	
340	↓	-40	↓	↓	↓	↓	↓	
341	↓	A3	0	↓	25L -10R	↓	0	
342	↓	-80	B3	↓	↓	↓	↓	
343	↓	-60	↓	↓	↓	↓	↓	
344	↓	-40	↓	↓	↓	↓	↓	
345	Atm	A3	0	↓	↓	↓	↓	
346	↓	-80	B3	↓	↓	↓	↓	
347	↓	-60	↓	↓	↓	↓	↓	
348	↓	-40	↓	↓	↓	↓	↓	
349	↓	A4	0	↓	0	↓	↓	
350	0.6×10^6	↓	↓	↓	↓	↓	0	
351	Atm	↓	↓	↓	↓	↓	↓	
352	0.6×10^6	↓	↓	↓	↓	↓	↓	Canards off
353	↓	A2	↓	Off	↓	↓	↓	
354	↓	80	B1	↓	↓	↓	↓	
355	↓	60	↓	↓	↓	↓	↓	
356	↓	40	↓	↓	↓	↓	↓	
357	3.0×10^6	A2	30	↓	↓	↓	↓	
358	Atm	A2	30	↓	↓	↓	↓	Canards, vertical tail off
359	2.2×10^6	40	B1	↓	↓	↓	Off	
360	↓	60	↓	↓	↓	↓	↓	
361	↓	80	↓	↓	↓	↓	↓	
362	Atm	40	↓	↓	↓	↓	↓	
363	↓	60	↓	↓	↓	↓	↓	
364	↓	80	↓	↓	↓	↓	↓	
365	0.6×10^6	40	↓	↓	↓	↓	↓	
366	↓	60	↓	↓	↓	↓	↓	
367	↓	80	↓	↓	↓	↓	↓	Body and canards
369	2.2×10^6	A1	0	-60	Off	Off	↓	
370	↓	80	B1	↓	↓	↓	↓	
371	↓	60	↓	↓	↓	↓	↓	
372	↓	40	↓	↓	↓	↓	↓	
373	↓	A1	0	-40	↓	↓	↓	

TABLE III.- Continued

Run	R_N , per foot	α	β	δ_c , deg	δ_a , deg	δ_s , deg	δ_R , deg	Configuration
374	2.2×10^6	80	B1	-40	Off	Off	Off	Body and canards
375	↓	60	↓	↓	↓	↓	↓	
376		40	↓	↓	↓	↓	↓	
377		A1	0	-20	↓	↓	↓	
378		80	B1	↓	↓	↓	↓	
379		60	↓	↓	↓	↓	↓	
380		40	↓	↓	↓	↓	↓	
381		A1	0	↓	↓	↓	↓	
382		80	B1	↓	↓	↓	↓	
383		60	↓	↓	↓	↓	↓	
384		40	↓	↓	↓	↓	↓	
385		A1	0	-40	↓	↓	↓	
386		80	B1	↓	↓	↓	↓	
387		60	↓	↓	↓	↓	↓	
388		40	↓	↓	↓	↓	↓	
389		A1	0	-60	↓	↓	↓	
390		80	B1	↓	↓	↓	↓	
391		60	↓	↓	↓	↓	↓	
392		40	↓	↓	↓	↓	↓	
393	0.35×10^6	A1	0	↓	↓	↓	↓	
394		80	B1	↓	↓	↓	↓	
395		60	↓	↓	↓	↓	↓	
396		40	↓	↓	↓	↓	↓	
397		A1	0	-40	↓	↓	↓	
398		80	B1	↓	↓	↓	↓	
399		60	↓	↓	↓	↓	↓	
400		40	↓	↓	↓	↓	↓	
401		A1	0	-20	↓	↓	↓	
402		80	B1	↓	↓	↓	↓	
403		60	↓	↓	↓	↓	↓	
404		40	↓	↓	↓	↓	↓	
405	0.6×10^6	A1	0	↓	↓	↓	↓	
406		80	B1	↓	↓	↓	↓	
407		60	↓	↓	↓	↓	↓	
408		40	↓	↓	↓	↓	↓	
409		A1	0	-40	↓	↓	↓	
410		80	B1	↓	↓	↓	↓	
411		60	↓	↓	↓	↓	↓	
412		40	↓	↓	↓	↓	↓	
413		A1	0	-60	↓	↓	↓	
414		80	B1	↓	↓	↓	↓	
415		60	↓	↓	↓	↓	↓	
416		40	↓	↓	↓	↓	↓	
417	2.2×10^6	A1	0	0	↓	↓	↓	
418		80	B1	↓	↓	↓	↓	
419		60	B1	↓	↓	↓	↓	

TABLE III.- Concluded

Run	R_N , per foot	α	β	δ_c , deg	δ_a , deg	δ_s , deg	δ_R , deg	Configuration
420	2.2×10^6	40	B1	0	Off	Off	Off	Body and canards
421	0.35×10^6	A1	0	↓	↓	↓	↓	
422	↓	80	B1					
423	↓	60	↓					
424	↓	40	↓					
425	0.6×10^6	A1	0					
426	↓	80	B1					
427	↓	60	↓					
428	↓	40	↓					
429	Atm	A1	0					
430	↓	80	B1					
431	↓	60	↓	↓	↓	↓	↓	Body alone
432	↓	40	↓					
433	6.3×10^6	A1	0					
434	↓	80	B1					
435	↓	60	↓					
436	↓	40	↓					
437	5.0×10^6	A1	0					
438	↓	80	B1					
439	↓	60	↓					
440	↓	40	↓					
441	2.2×10^6	A1	0					
442	↓	80	B1					
443	↓	60	↓					
444	↓	40	↓					
445	0.35×10^6	A1	0					
446	↓	80	B1					
447	↓	60	↓					
448	↓	40	↓					
449	0.6×10^6	A1	0					
450	↓	80	B1					
451	↓	60	↓					
452	↓	40	↓					
453	Atm	A1	0					
454	↓	80	B1					
455	↓	60	↓					
456	↓	40	↓					

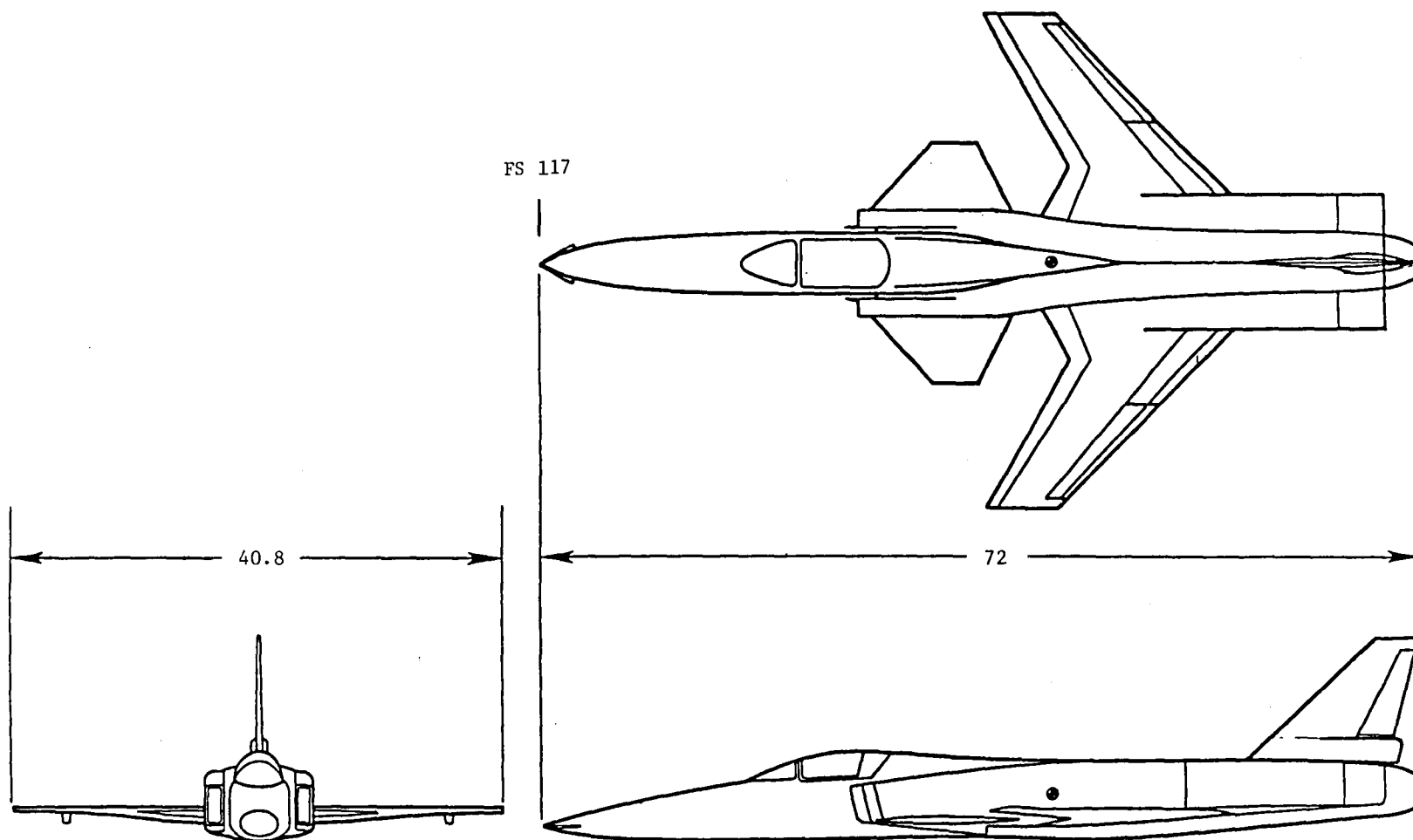


Figure 1.- Three-view sketch of basic model. Moment reference point shown is FS 454.27 ($-0.05\bar{c}$).
(Dimensions are in inches.)

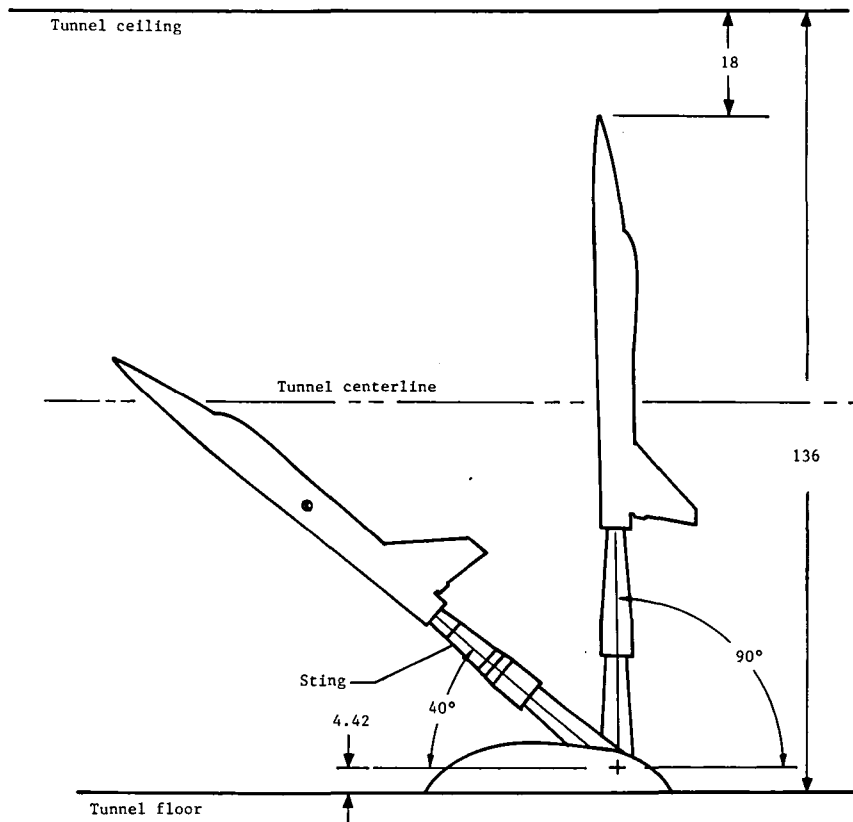
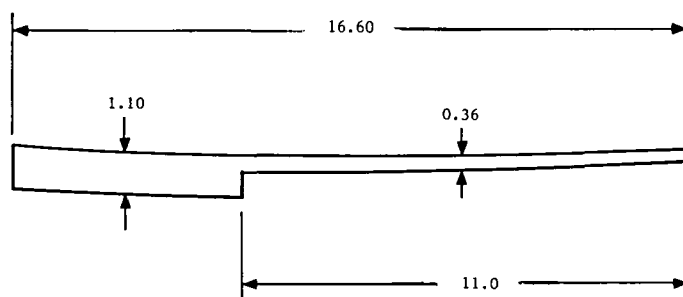
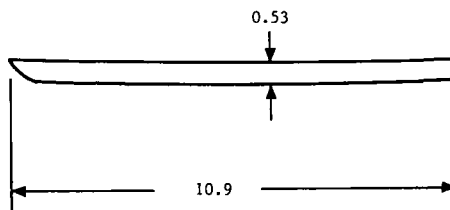


Figure 2.- Model and sting configuration for maximum and minimum angles of attack. Linear dimensions are in inches.



Strake A (ventral strake)



Strakes B and C

Figure 3.- Forebody strakes. Dimensions are in inches.

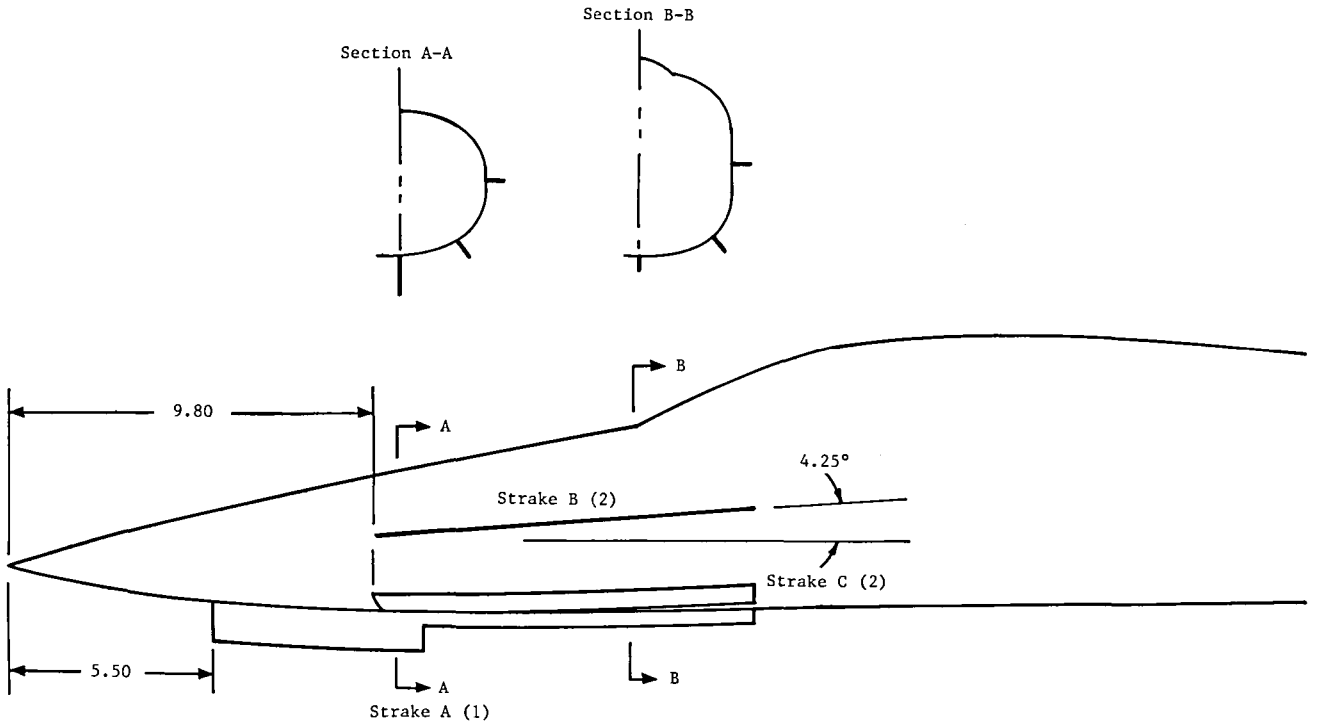


Figure 4.- Placement of various forebody strakes.
Linear dimensions are in inches.

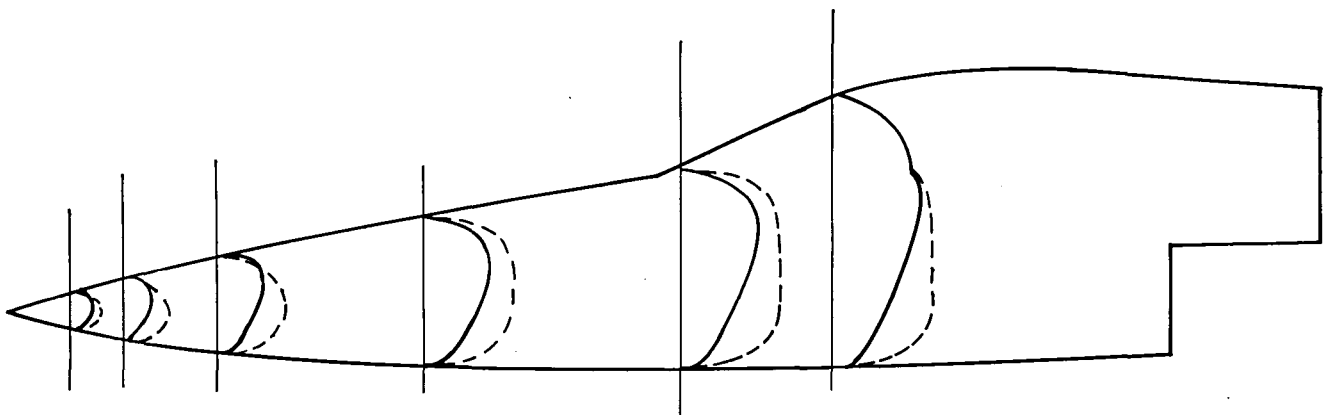
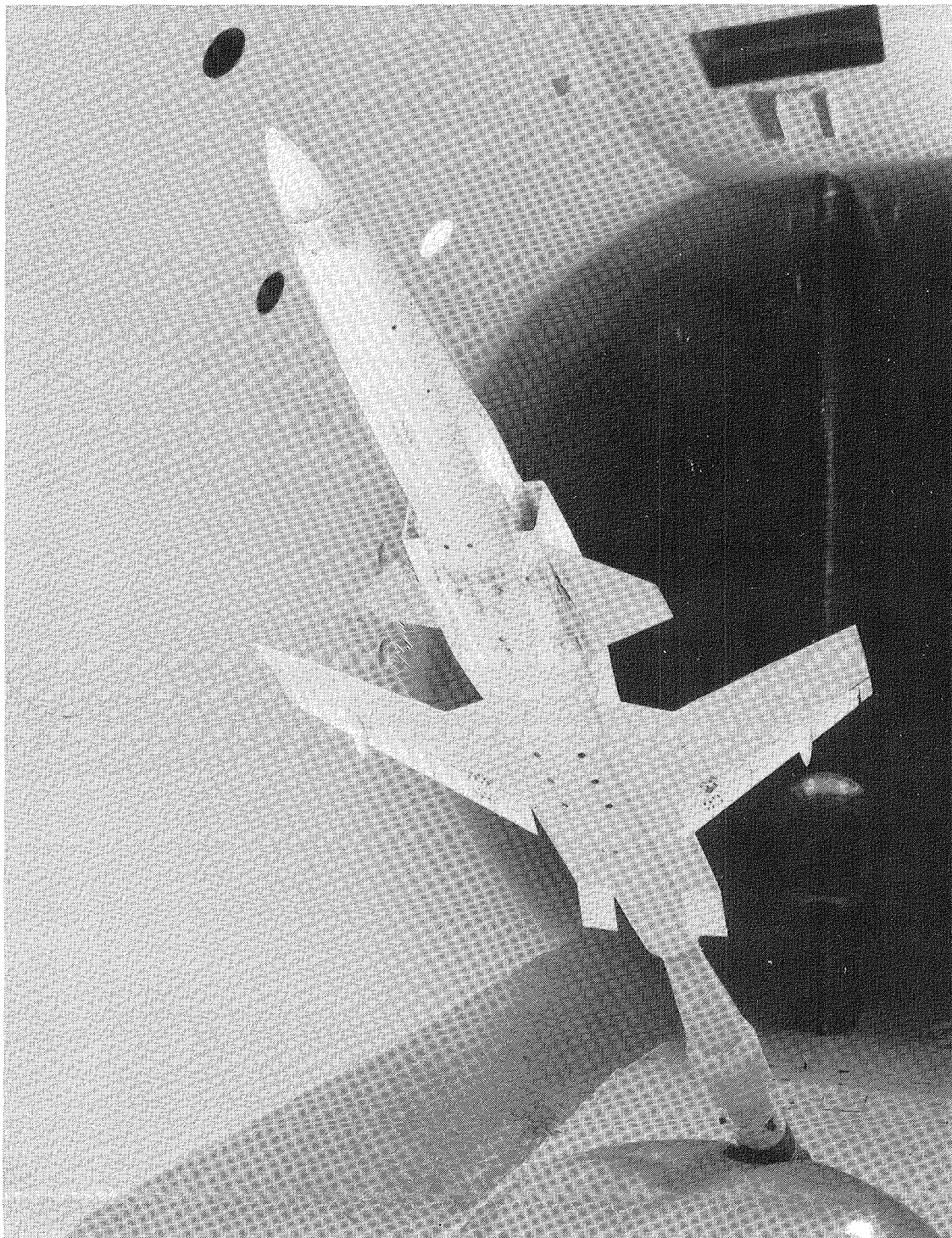


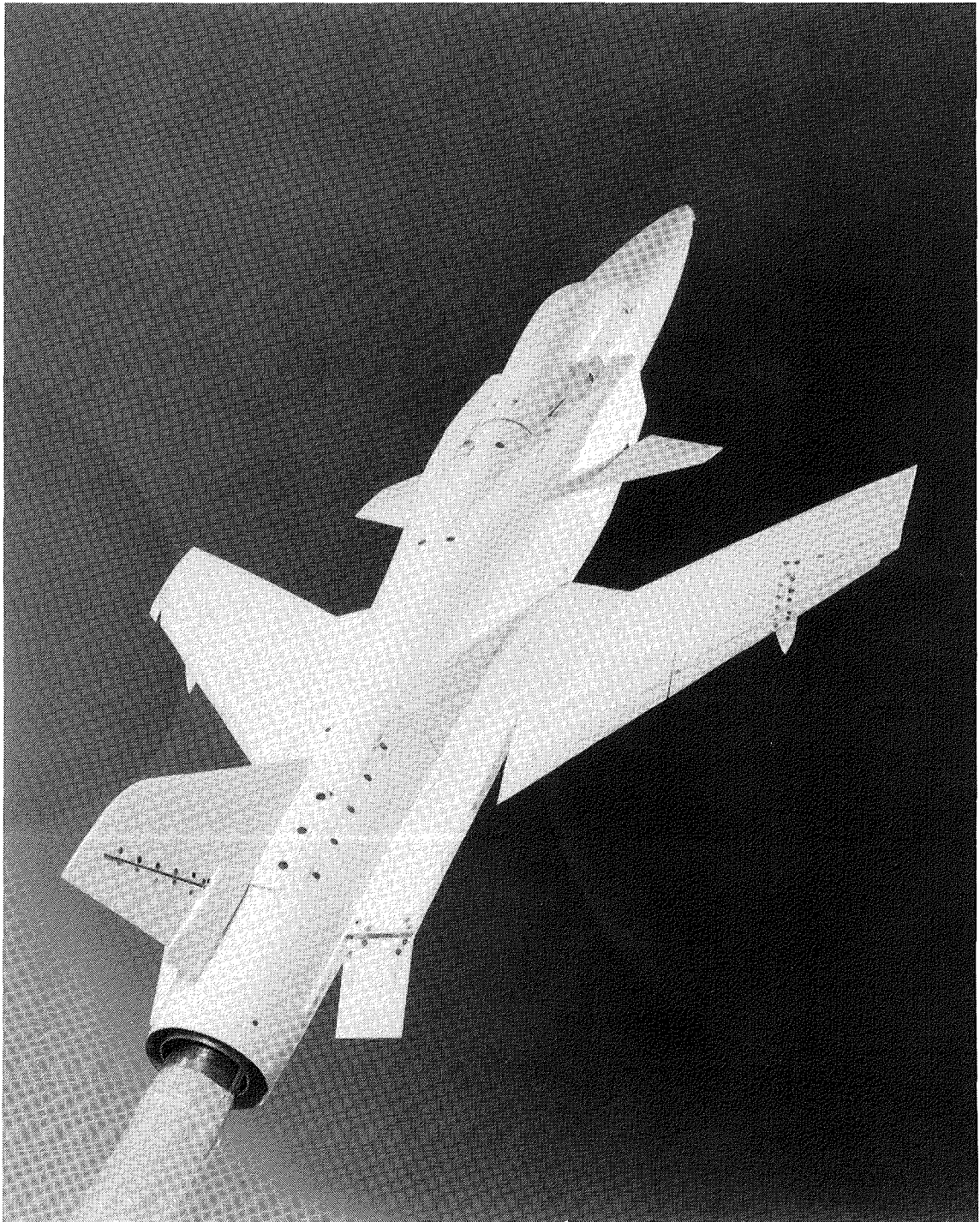
Figure 5.- Alternate forebody cross-sectional shape.
Dashed lines show basic configuration.



L-86-301

(a) High-angle-of-attack support system.

Figure 6.- Model installation.



L-86-302

(b) Sting entry and various control surfaces deflected.

Figure 6.- Concluded.

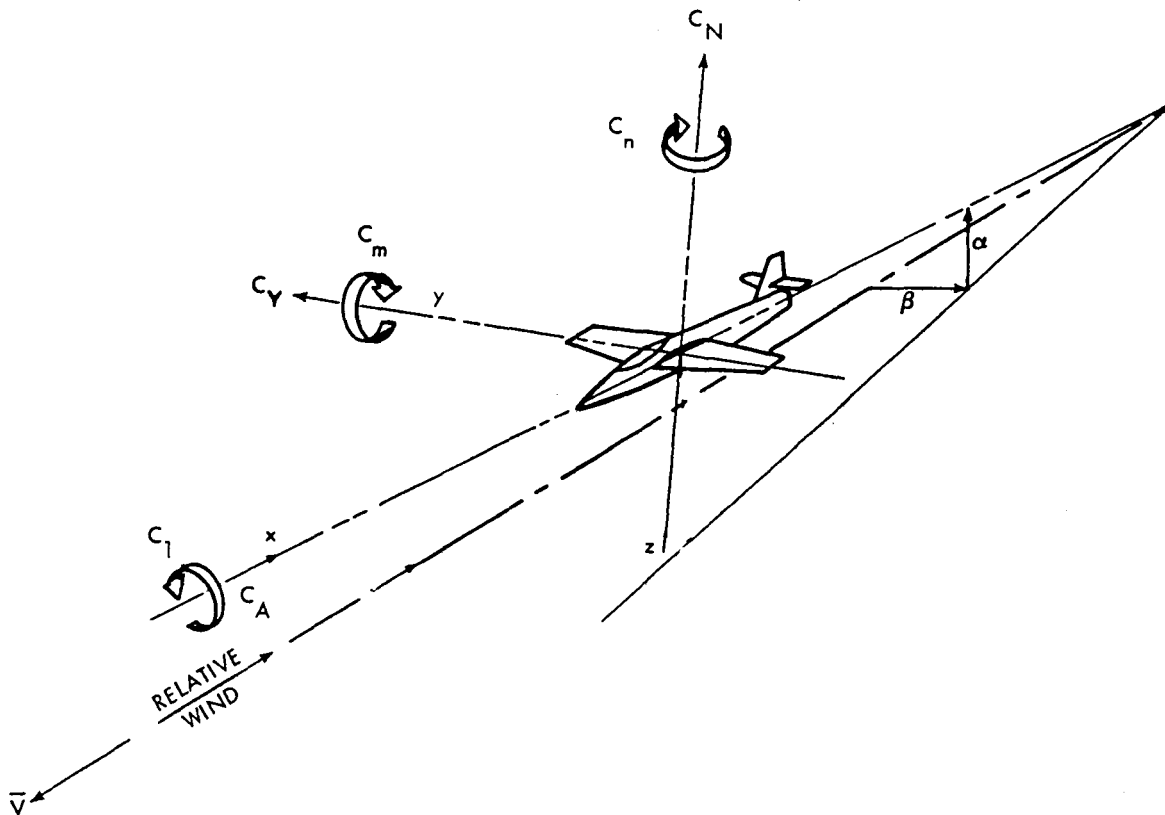
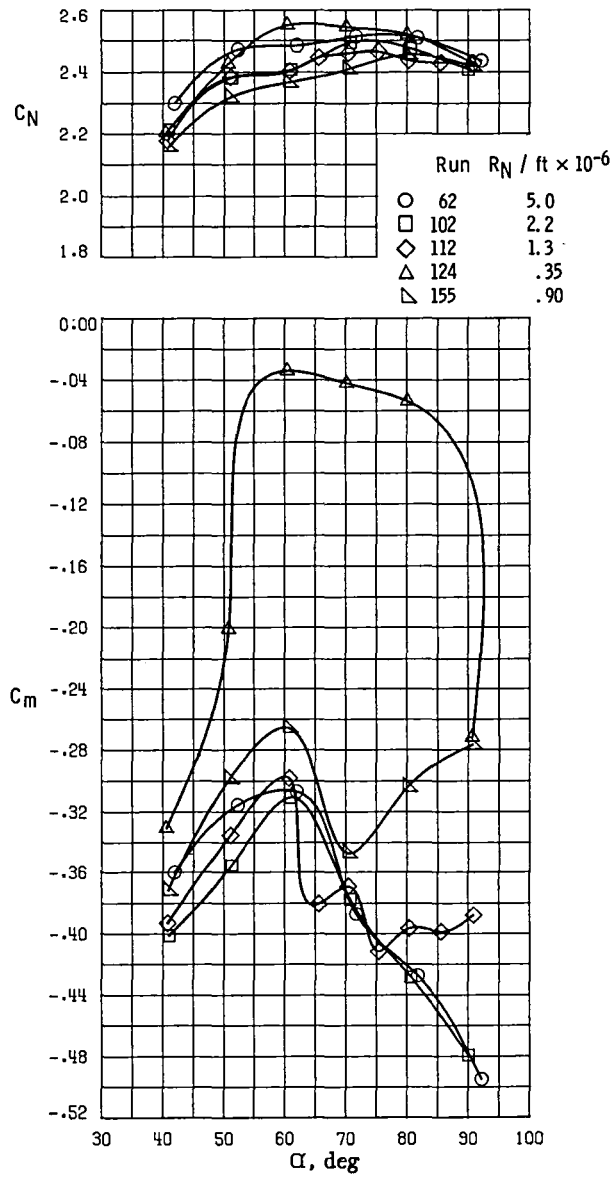
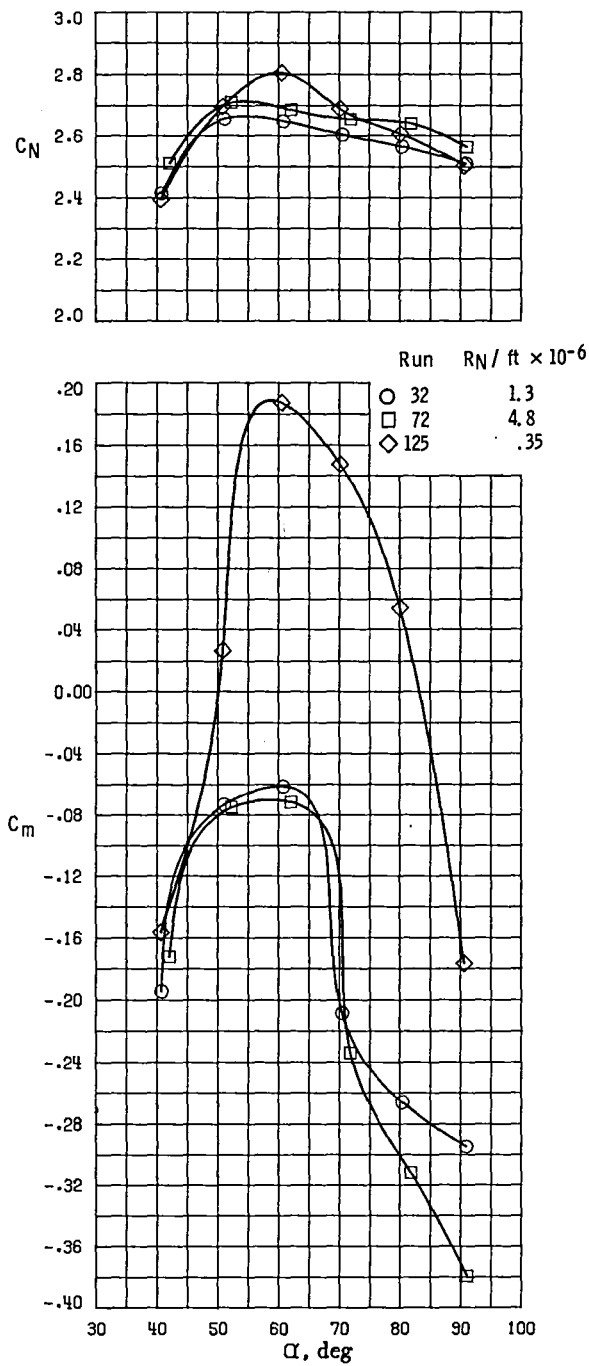


Figure 7.- Orientation of force and moment coefficients about body axes. Positive directions of force coefficients, moment coefficients, and angles are indicated by arrows.



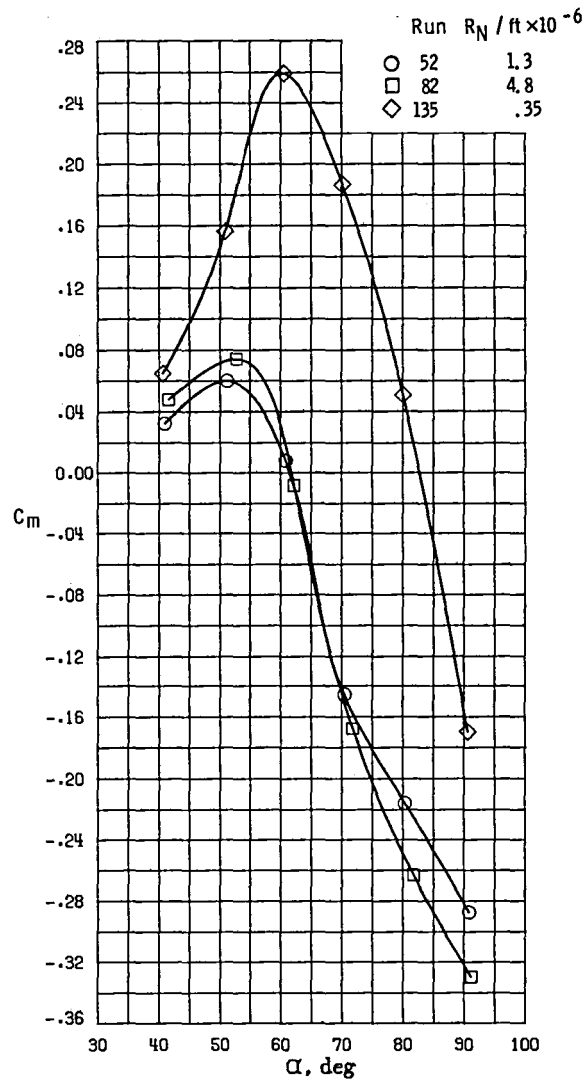
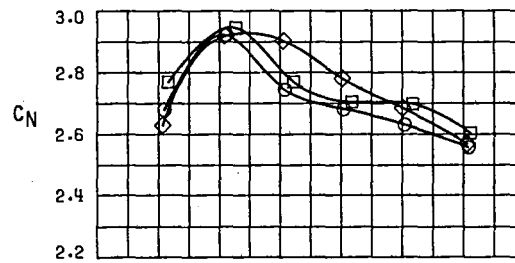
(a) $\delta_c = -60^\circ$; $\delta_a = 25^\circ$; $\delta_s = 30^\circ$.

Figure 8.- Longitudinal aerodynamic characteristics at various Reynolds numbers with $\beta = 0^\circ$.



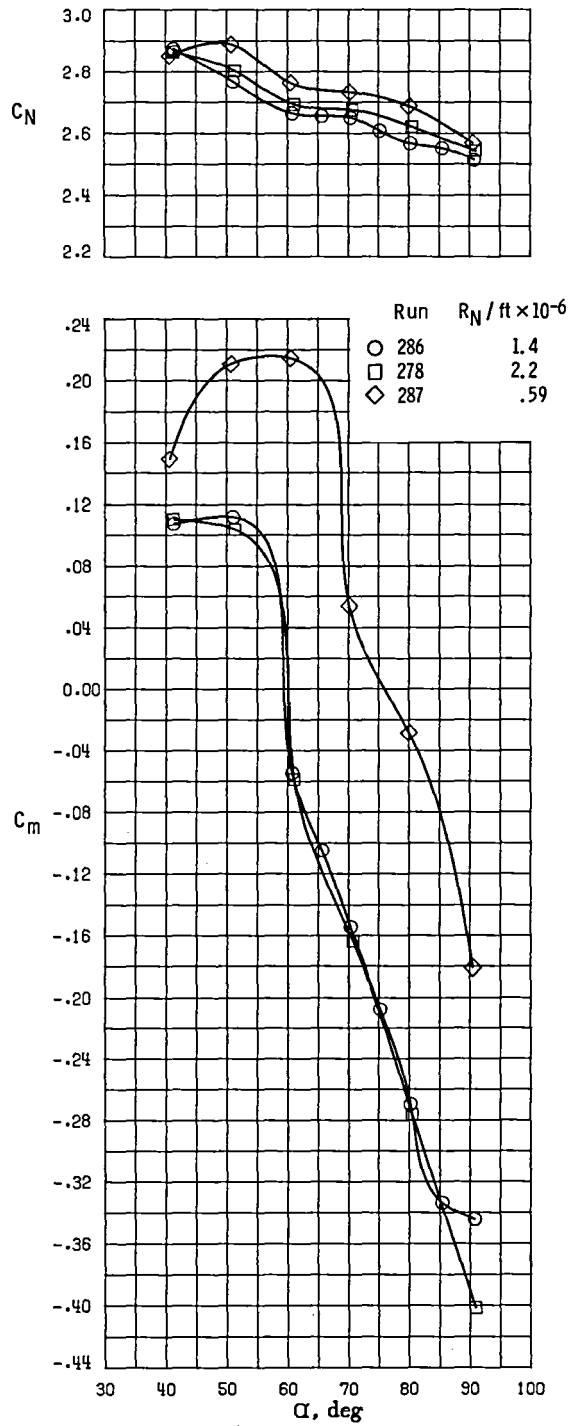
(b) $\delta_c = -40^\circ$; $\delta_a = 25^\circ$; $\delta_s = 30^\circ$.

Figure 8.- Continued.



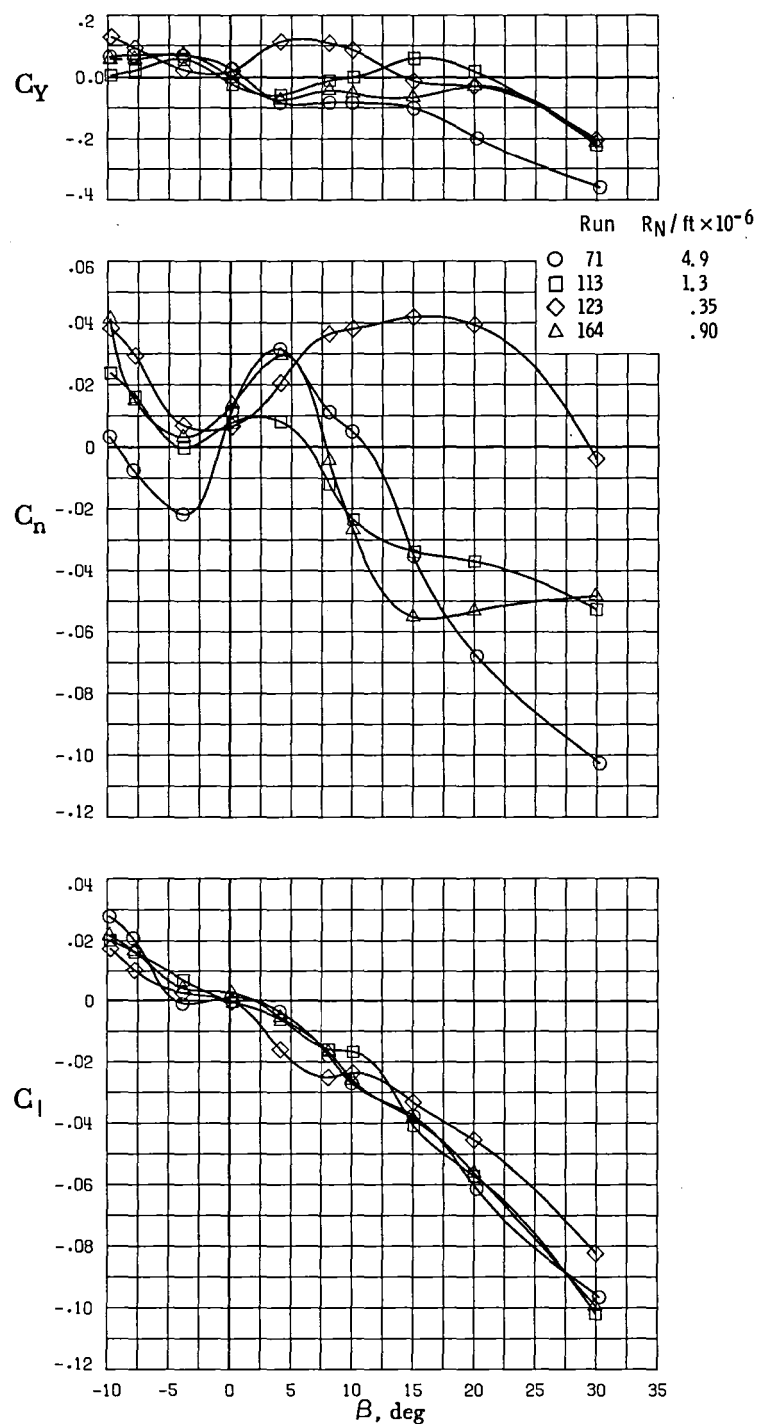
(c) $\delta_c = -20^\circ$; $\delta_a = 25^\circ$; $\delta_s = 30^\circ$.

Figure 8.- Continued.



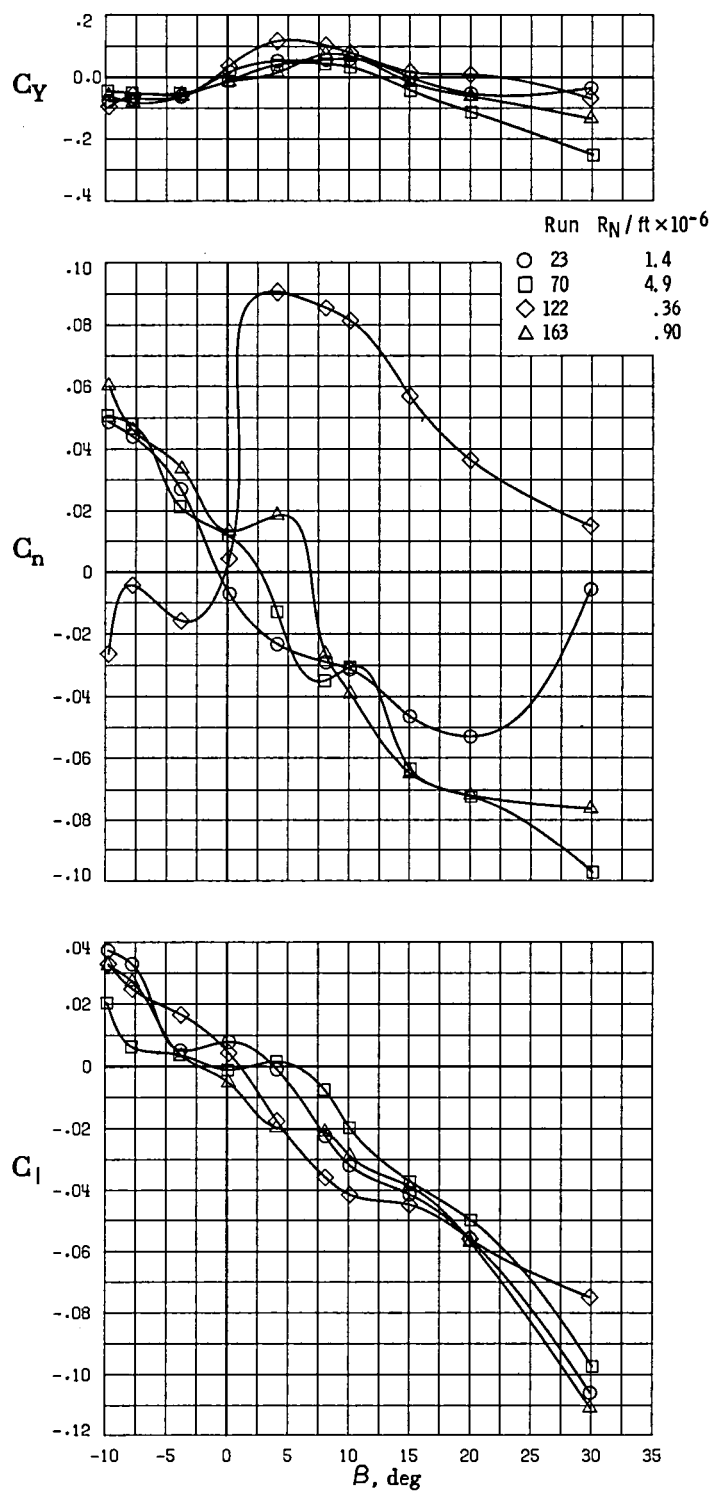
(d) $\delta_c = 0^\circ$; $\delta_a = 25^\circ$; $\delta_s = 30^\circ$.

Figure 8.- Concluded.



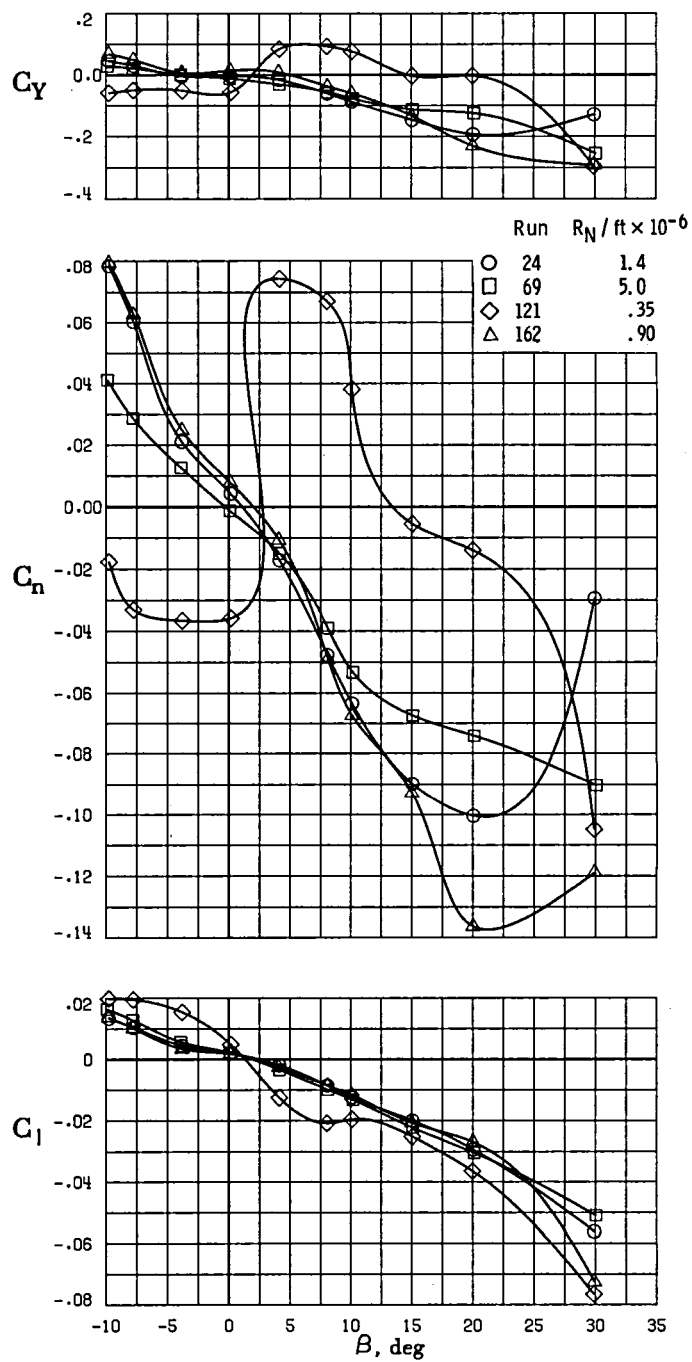
(a) $\alpha = 40^\circ$.

Figure 9.- Lateral-directional aerodynamic characteristics at various Reynolds numbers. $\delta_c = -60^\circ$; $\delta_a = 25^\circ$; $\delta_s = 30^\circ$.



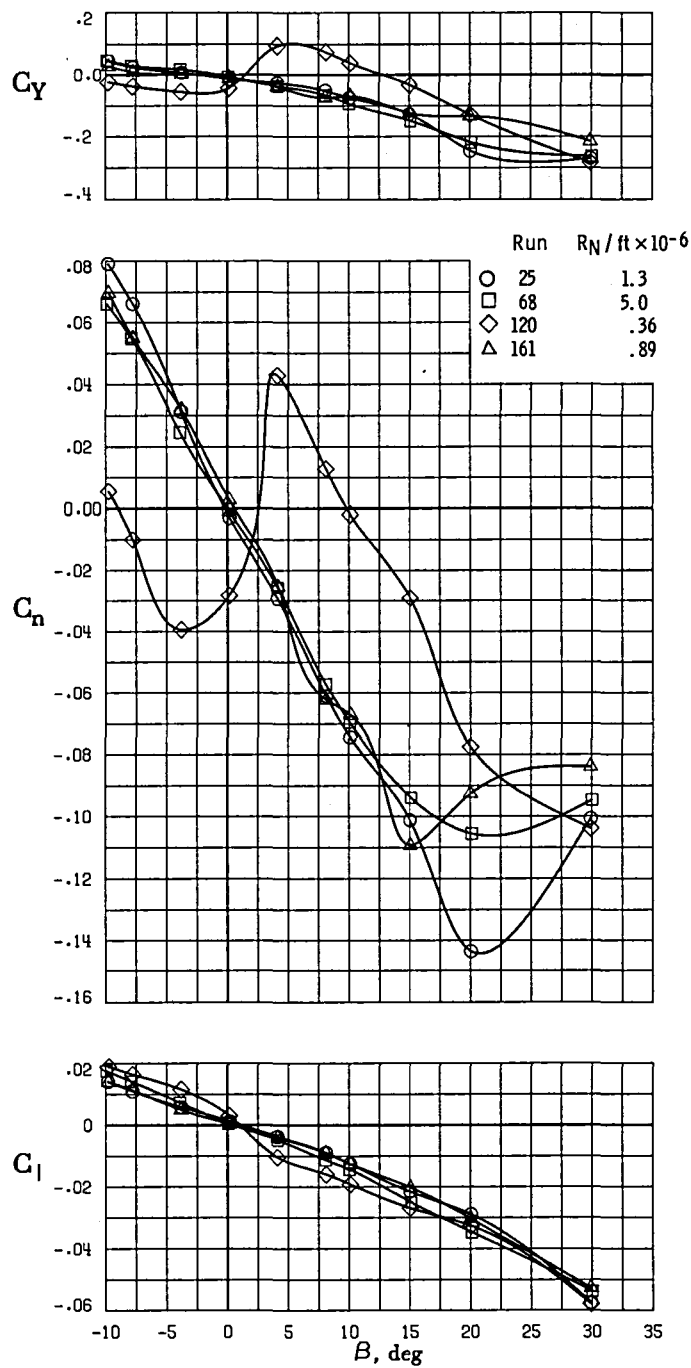
(b) $\alpha = 50^\circ$.

Figure 9.- Continued.



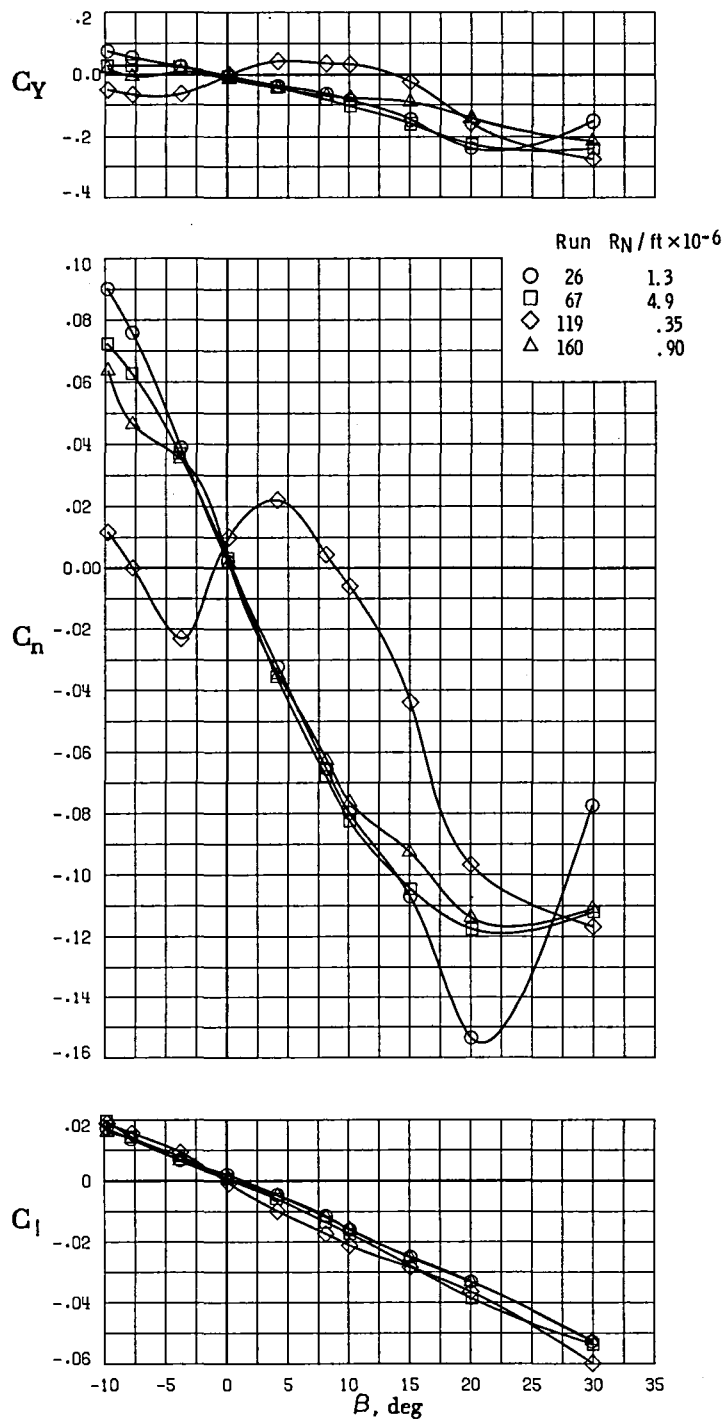
(c) $\alpha = 60^\circ$.

Figure 9.- Continued.



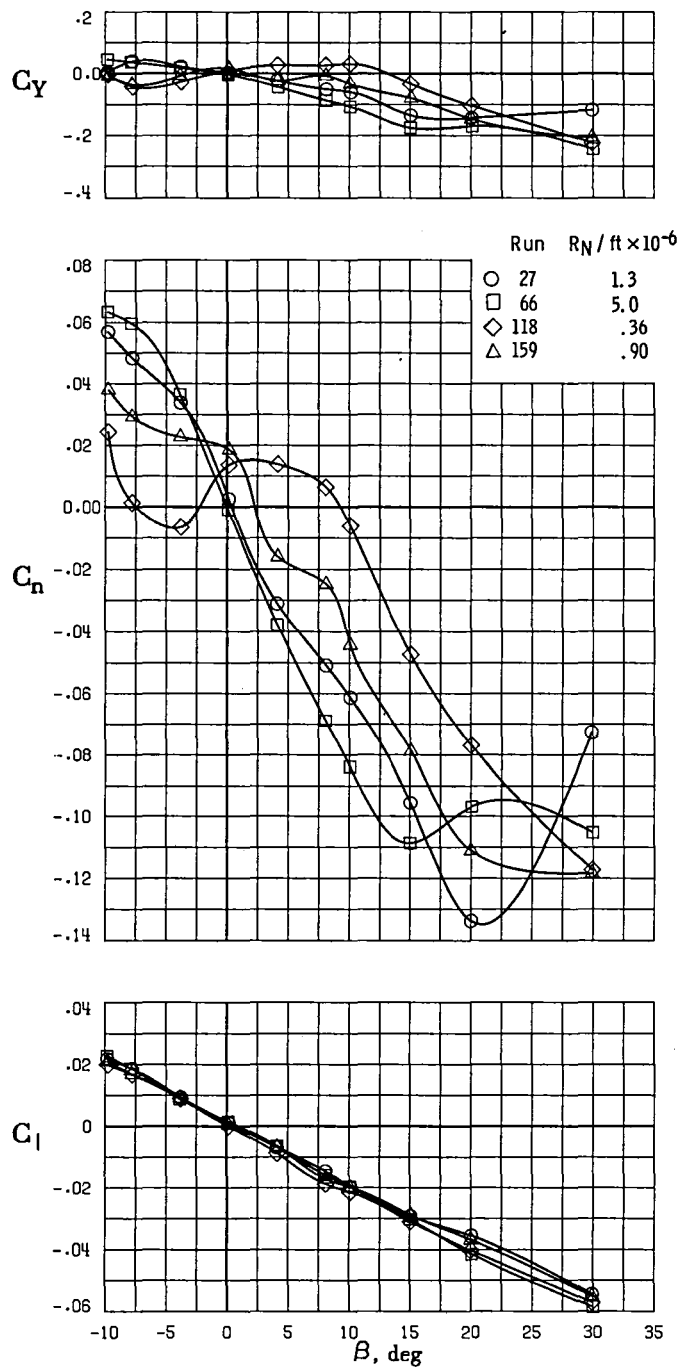
(d) $\alpha = 65^\circ$.

Figure 9.- Continued.



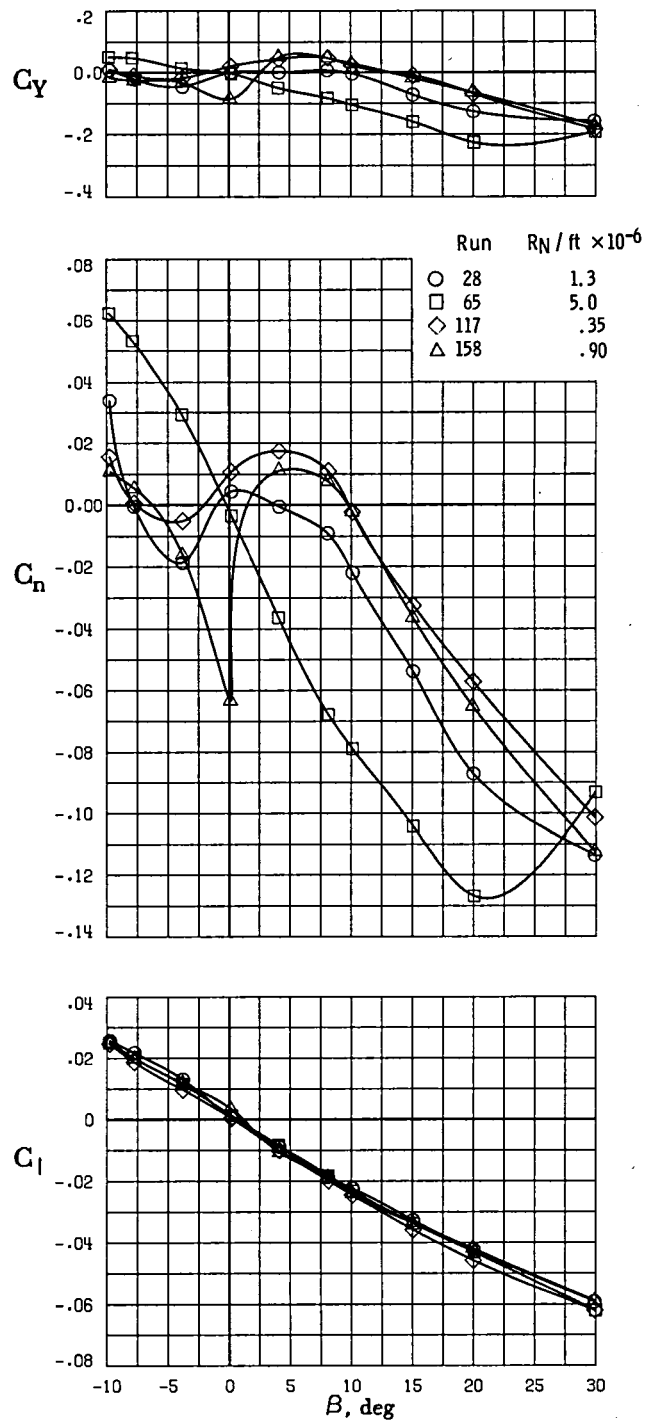
(e) $\alpha = 70^\circ$.

Figure 9.- Continued.



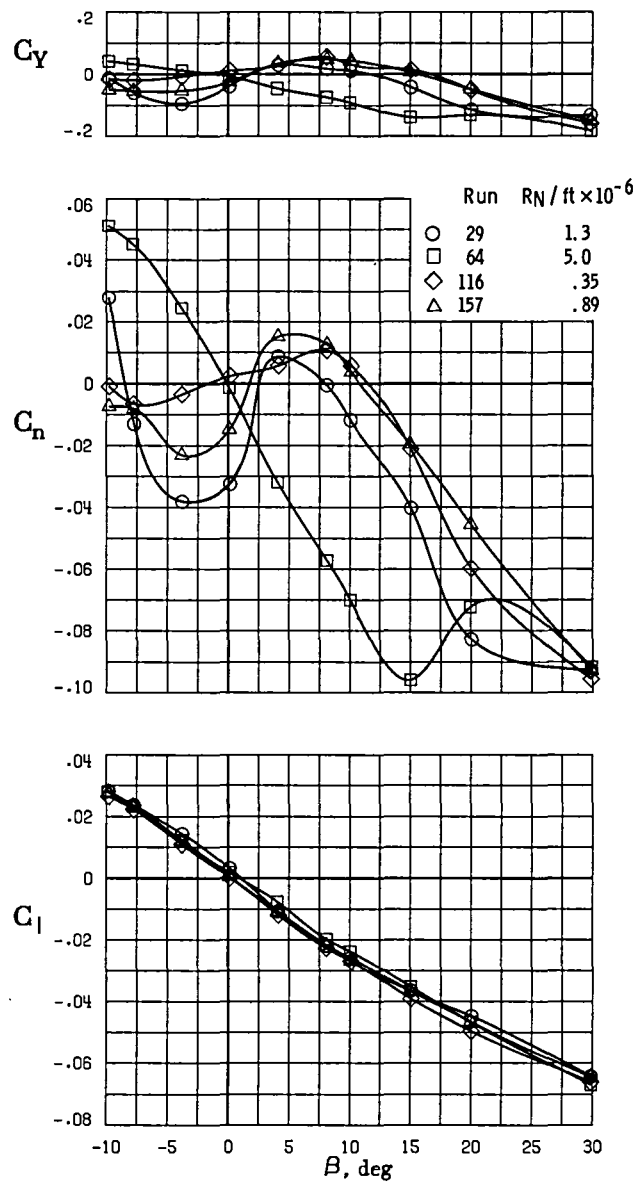
(f) $\alpha = 75^\circ$.

Figure 9.- Continued.



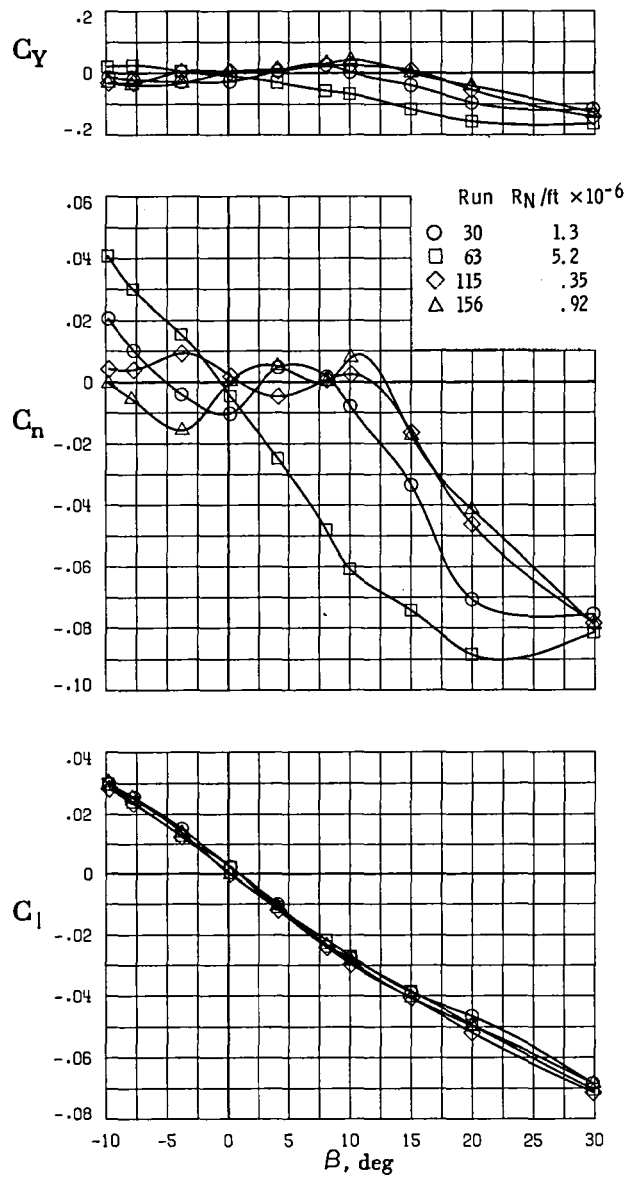
(g) $\alpha = 80^\circ$.

Figure 9.- Continued.



(h) $\alpha = 85^\circ$.

Figure 9.- Continued.



(i) $\alpha = 90^\circ$.

Figure 9.- Concluded.

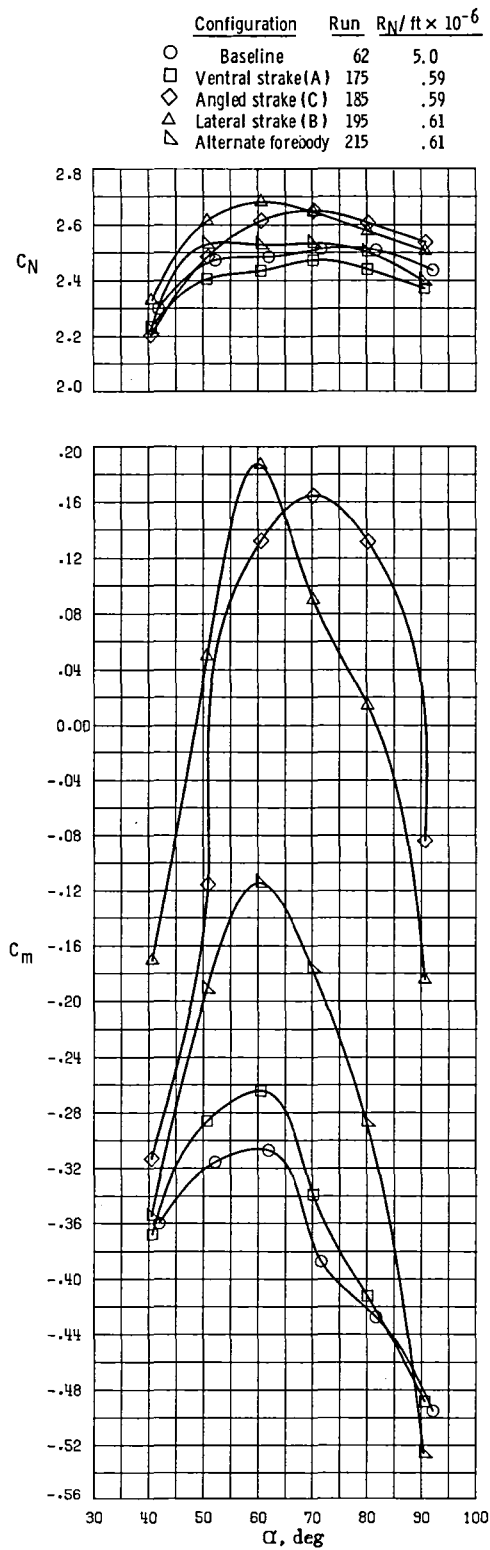
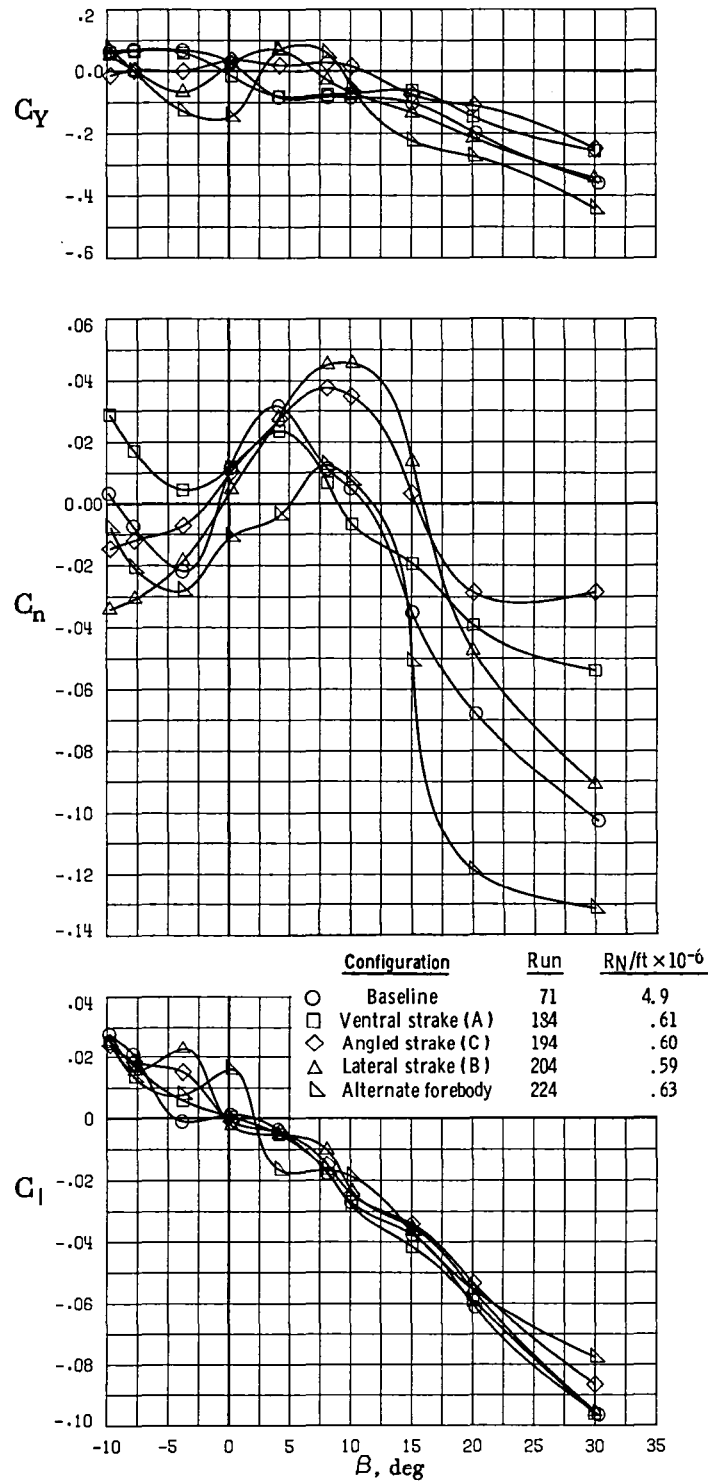
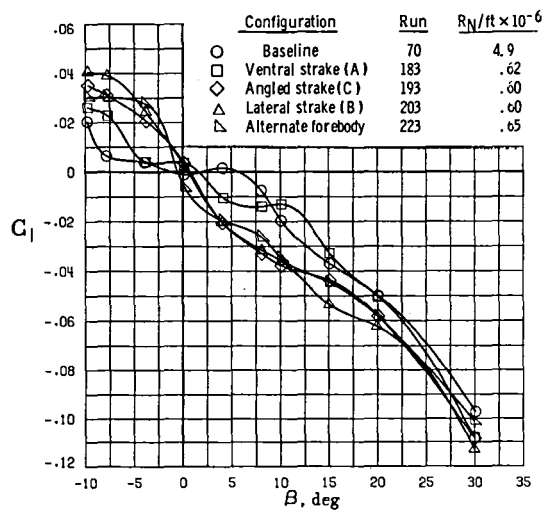
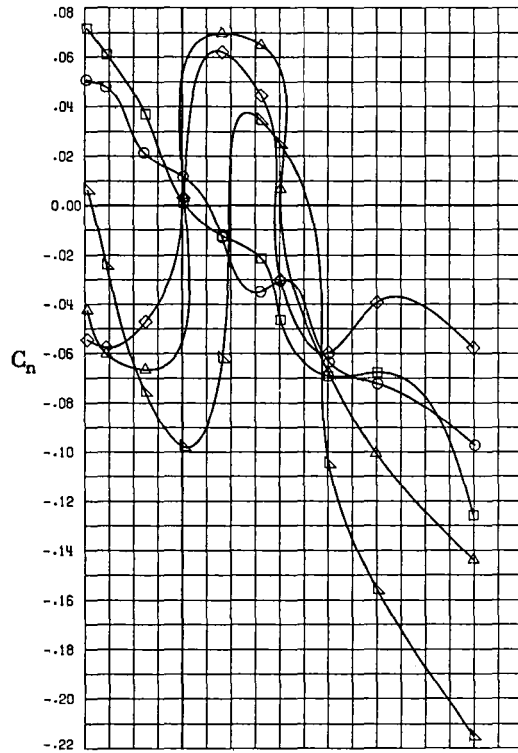
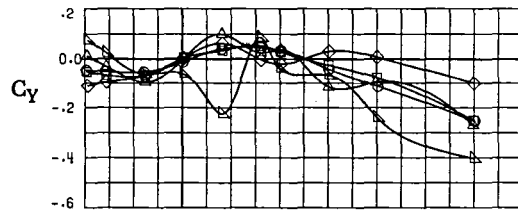


Figure 10.- Longitudinal aerodynamic characteristics of baseline configuration at high Reynolds number compared with various forebody modifications at low Reynolds number.



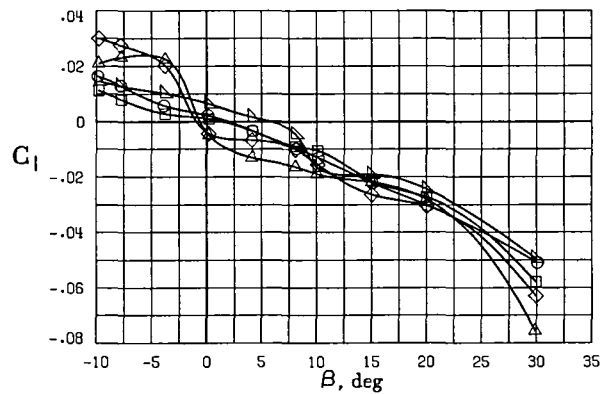
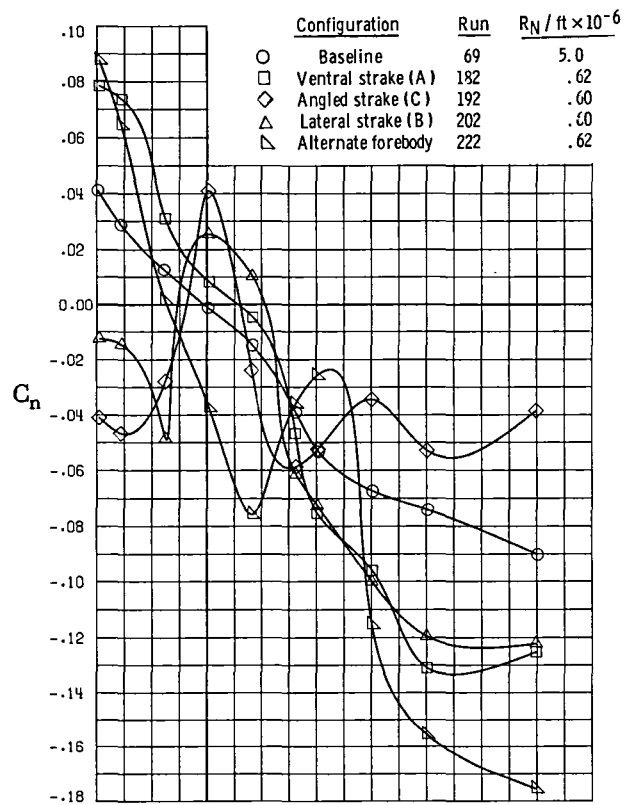
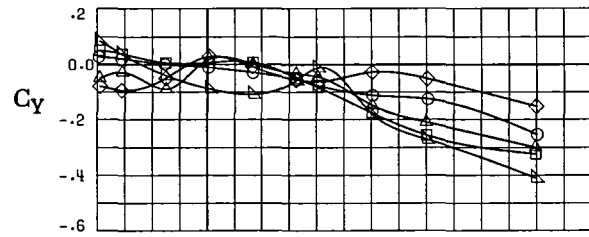
(a) $\alpha = 40^\circ$.

Figure 11.- Lateral-directional aerodynamic characteristics of baseline configuration at high Reynolds number compared with various forebody modifications at low Reynolds number.



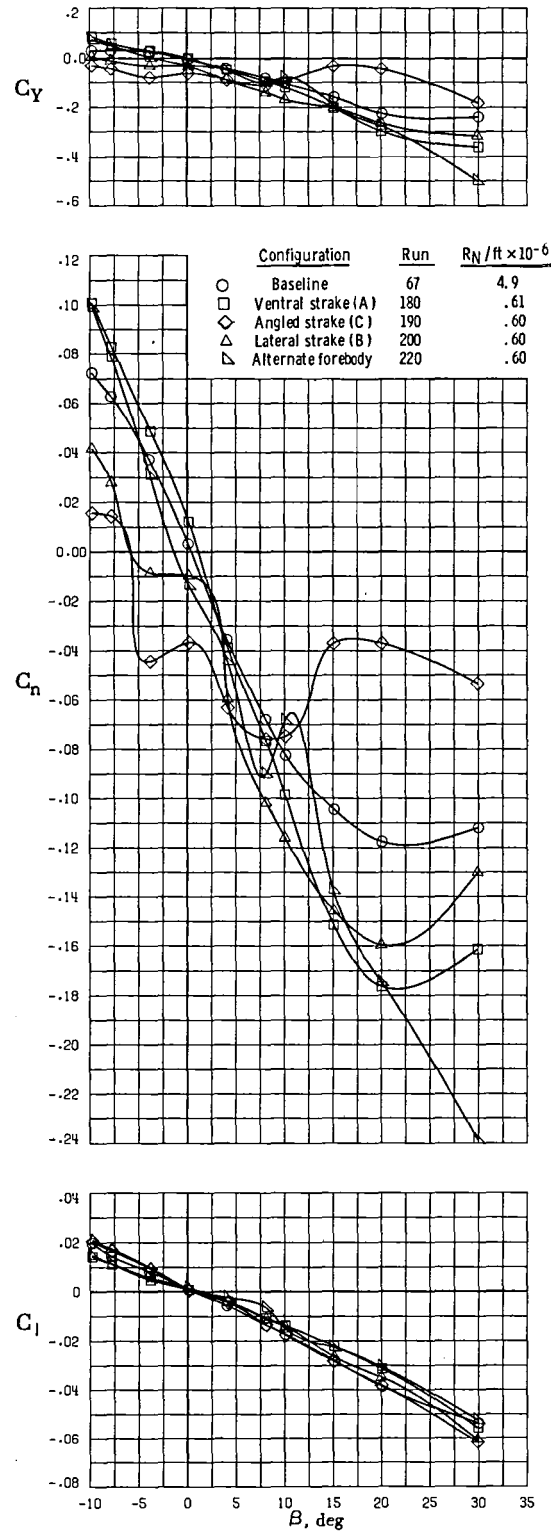
(b) $\alpha = 50^\circ$.

Figure 11.- Continued.



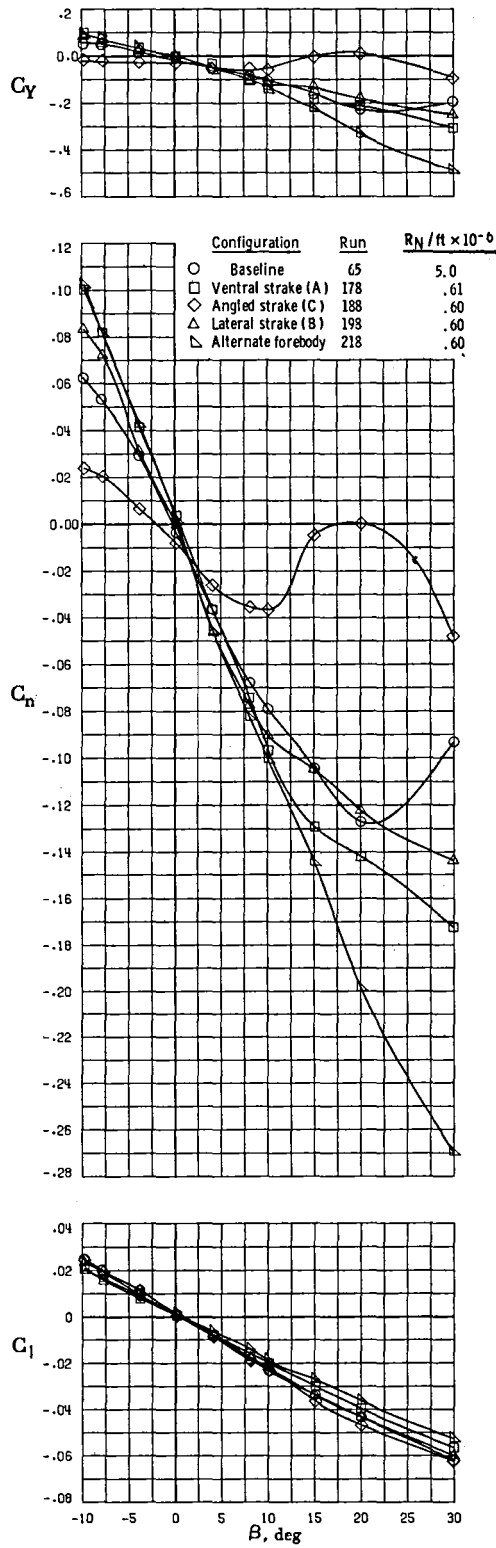
(c) $\alpha = 60^\circ$.

Figure 11.- Continued.



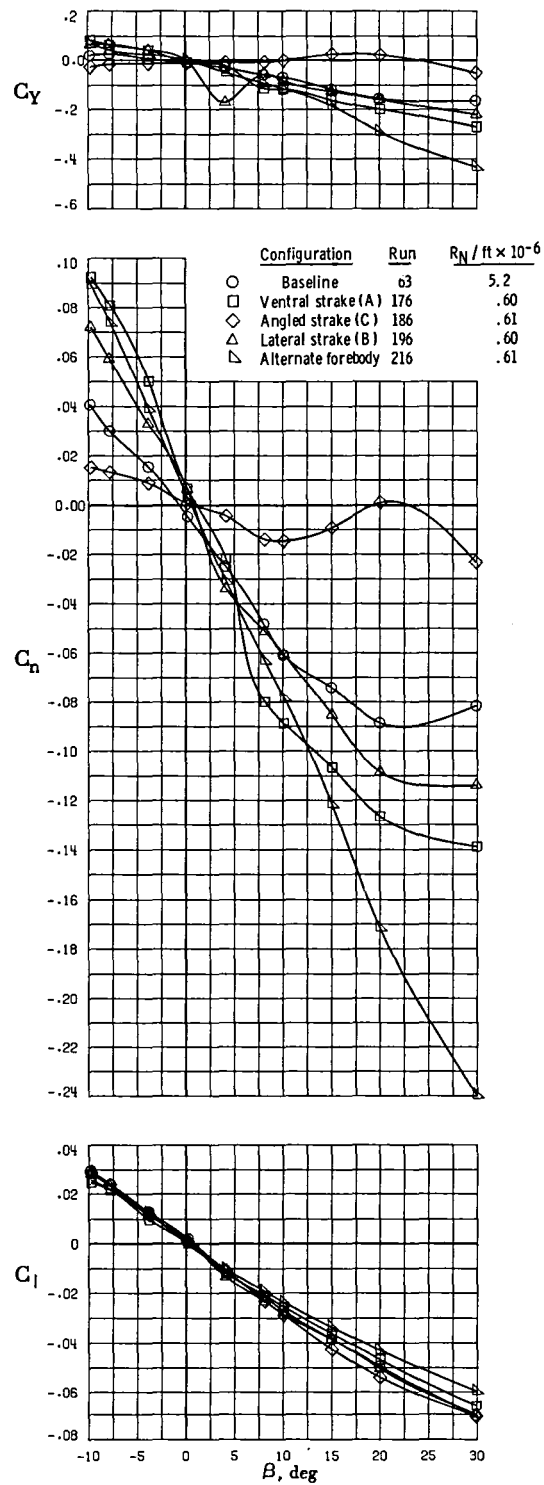
(d) $\alpha = 70^\circ$.

Figure 11.- Continued.



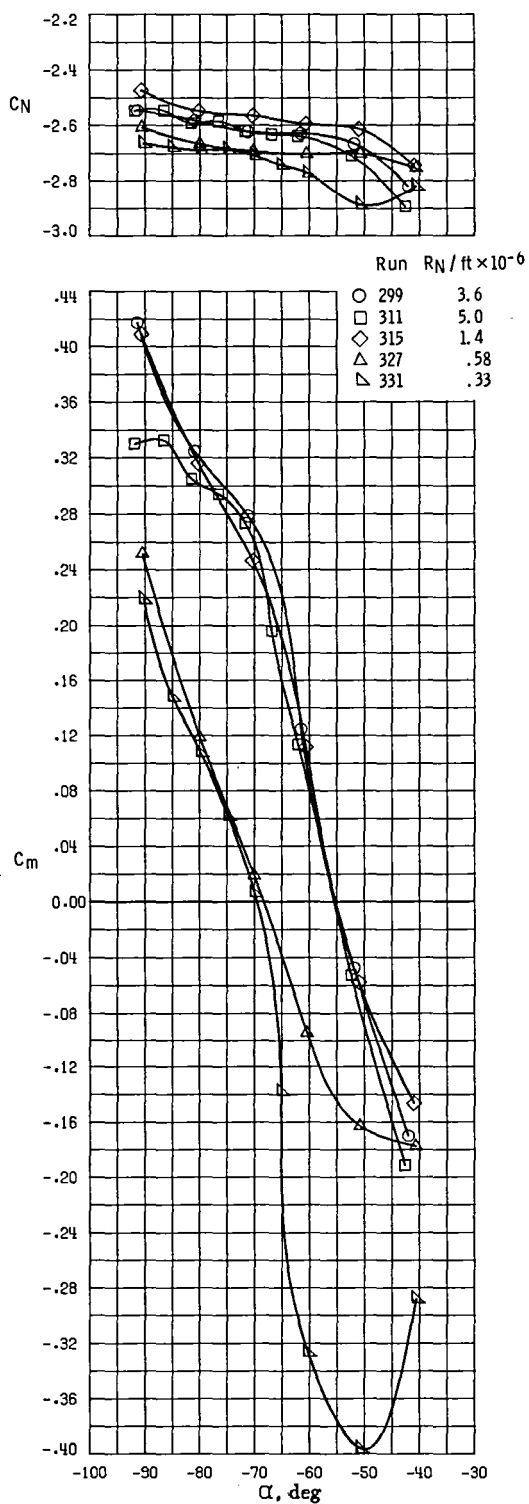
(e) $\alpha = 80^\circ$.

Figure 11.- Continued.



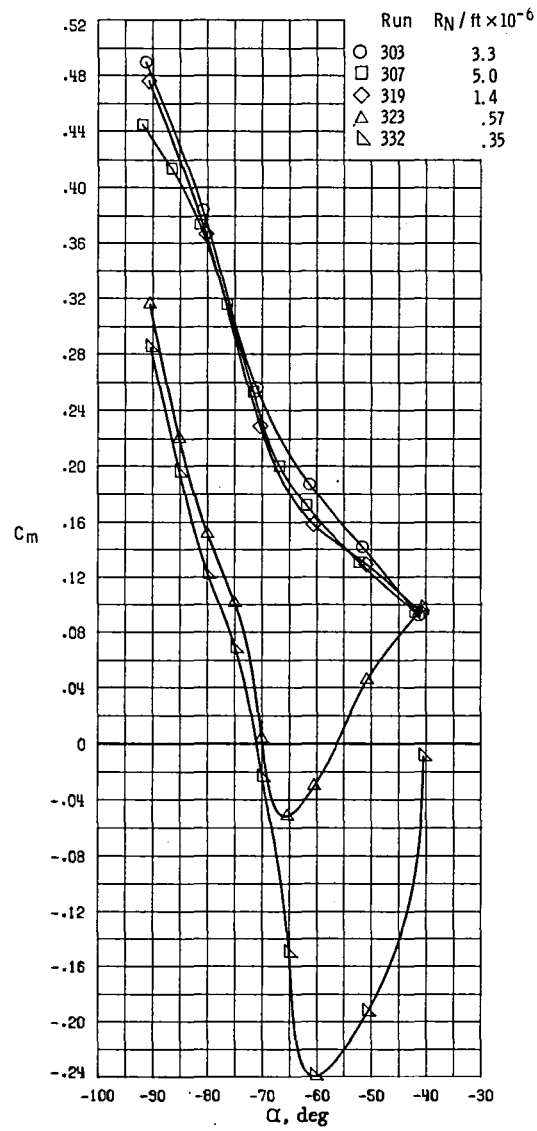
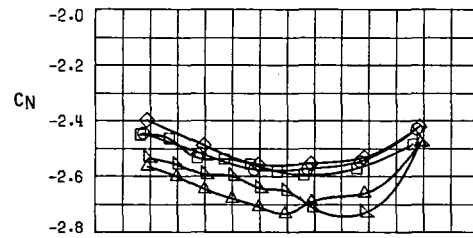
(f) $\alpha = 90^\circ$.

Figure 11.- Concluded.



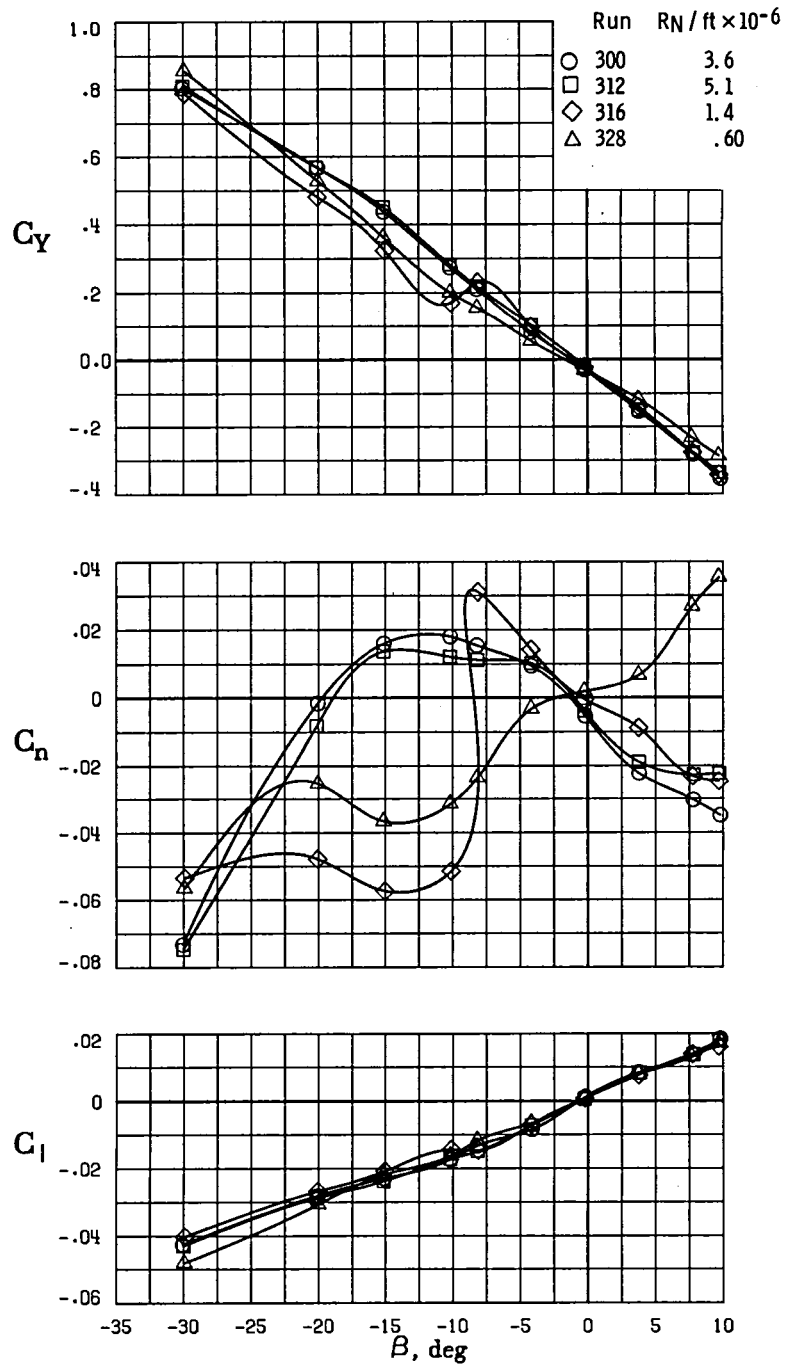
(a) $\delta_c = 0^\circ$; $\delta_f = -10^\circ$; $\delta_s = -30^\circ$.

Figure 12.- Longitudinal aerodynamic characteristics at negative high angles of attack for various Reynolds numbers with $\beta = 0^\circ$.



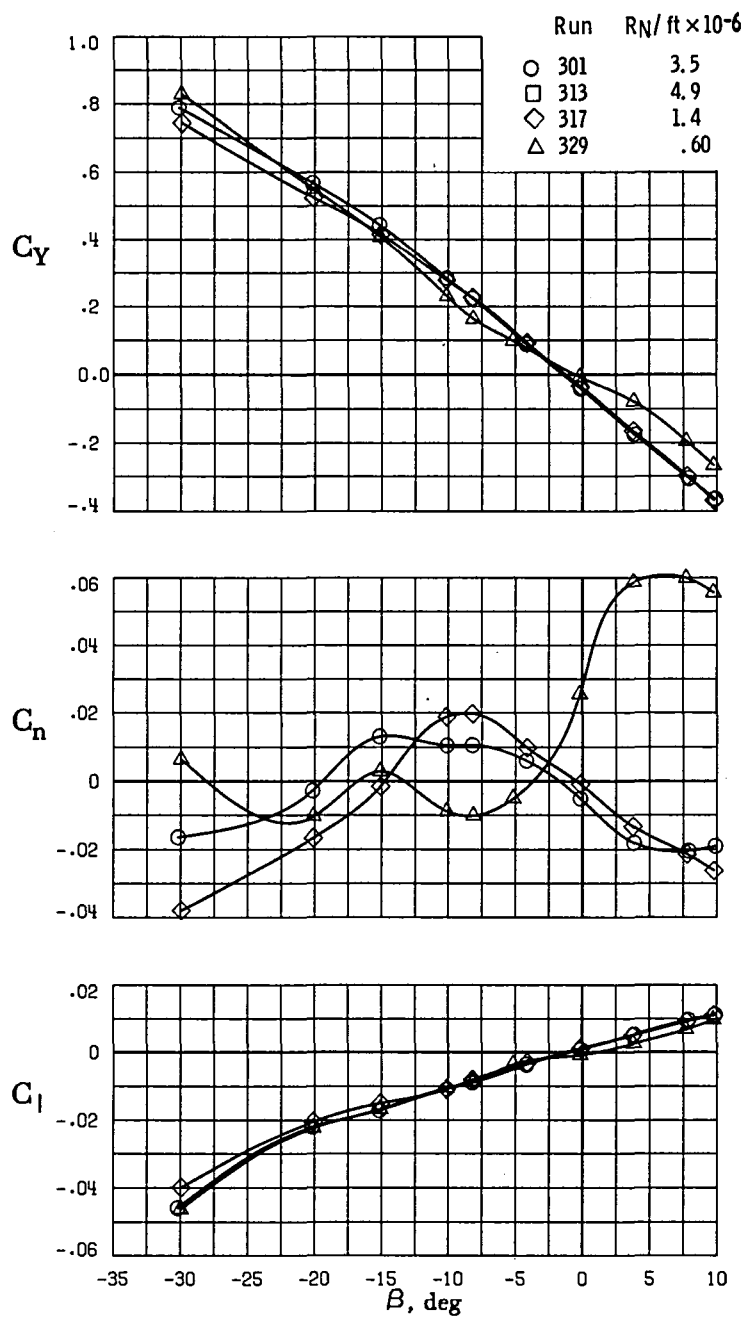
(b) $\delta_C = 30^\circ$; $\delta_F = -10^\circ$; $\delta_S = -30^\circ$.

Figure 12.- Concluded.



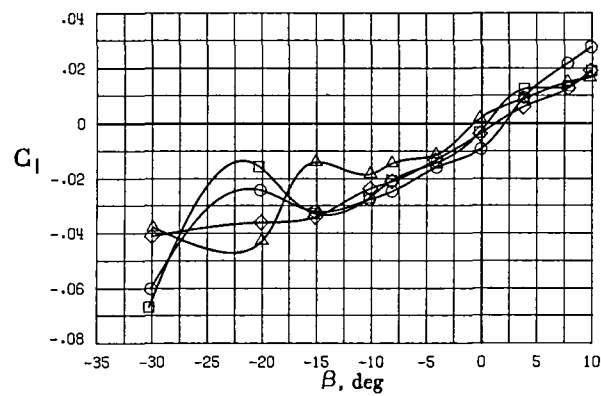
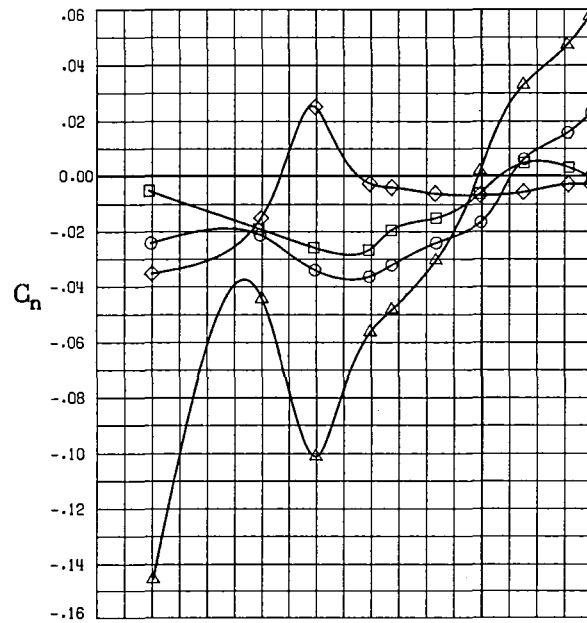
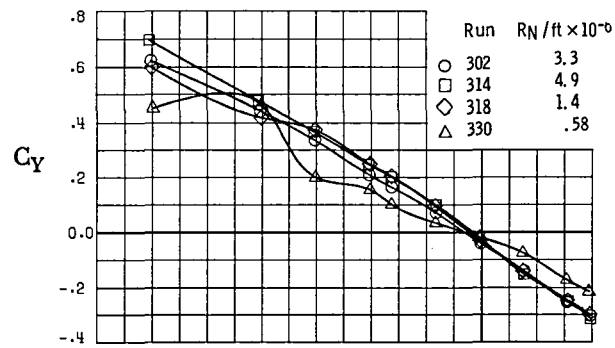
(a) $\alpha = -80^\circ$; $\delta_c = 0^\circ$; $\delta_f = -10^\circ$; $\delta_s = -30^\circ$.

Figure 13.- Lateral-directional aerodynamic characteristics at negative high angles of attack for various Reynolds numbers.



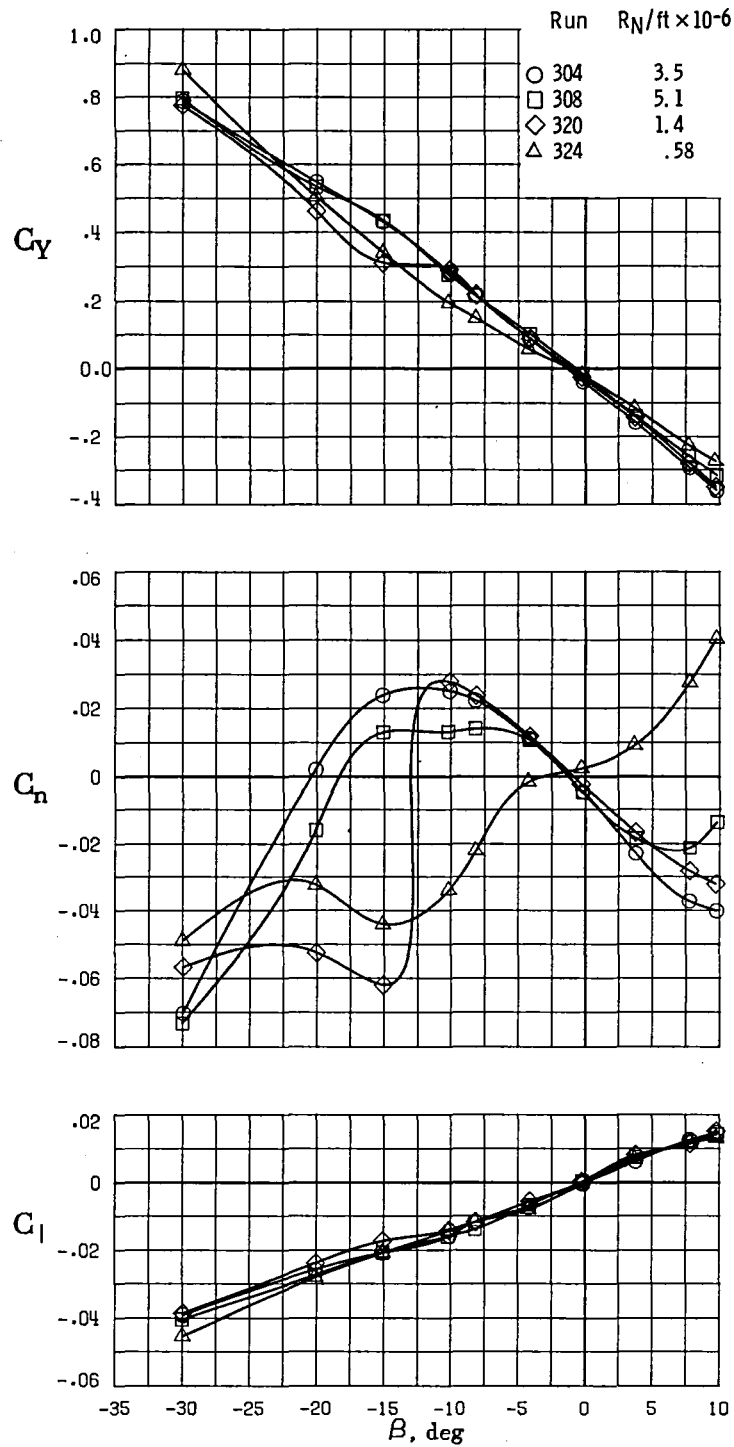
(b) $\alpha = -60^\circ$; $\delta_c = 0^\circ$; $\delta_f = -10^\circ$; $\delta_s = -30^\circ$.

Figure 13.- Continued.



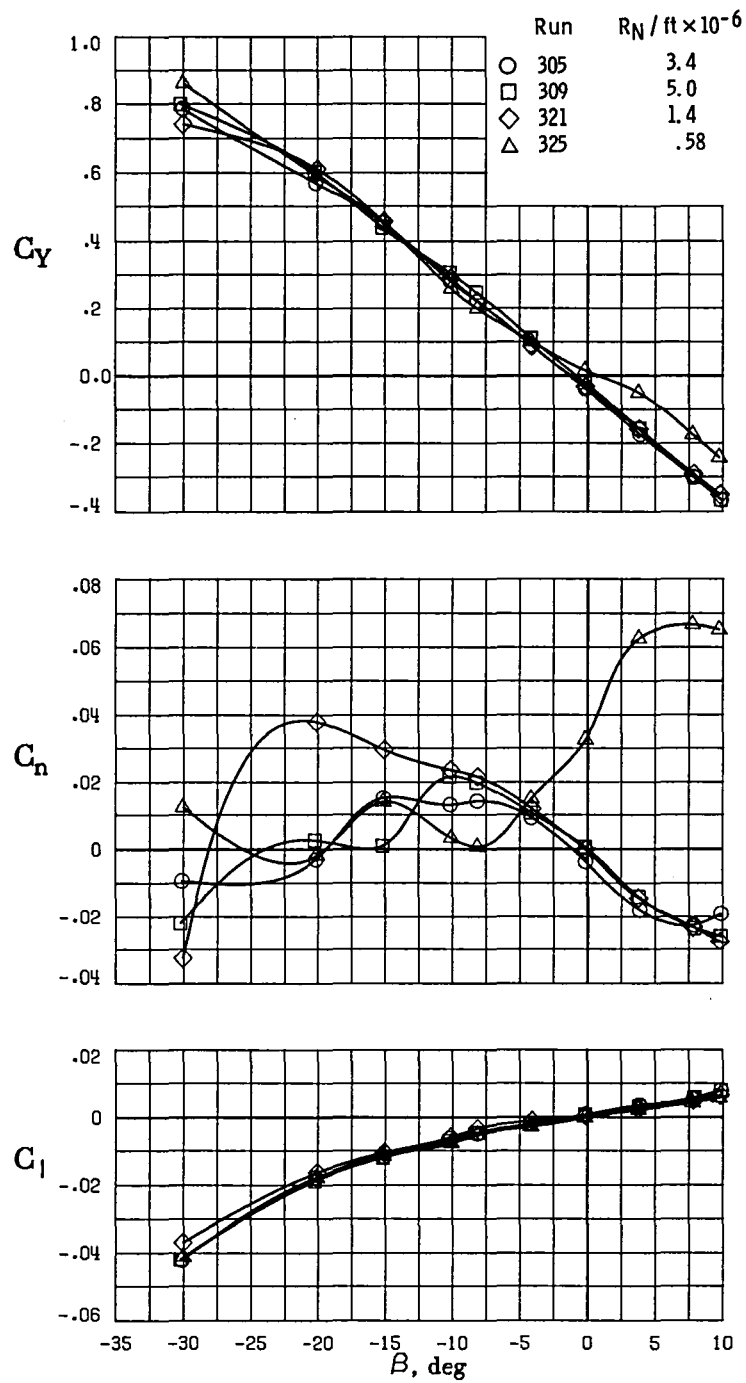
(c) $\alpha = -40^\circ$; $\delta_c = 0^\circ$; $\delta_f = -10^\circ$; $\delta_s = -30^\circ$.

Figure 13.- Continued.



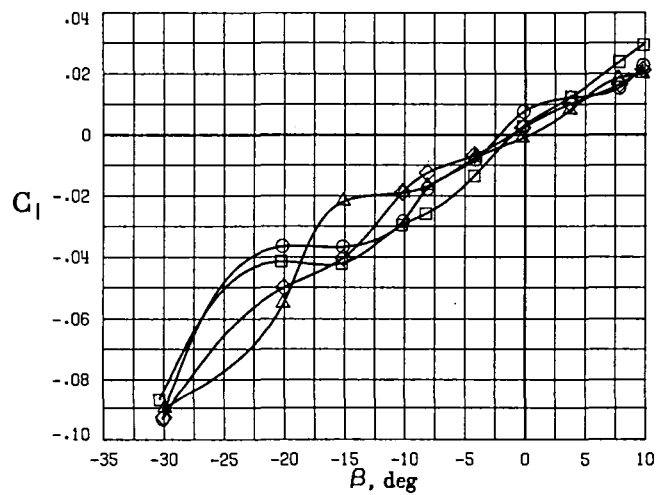
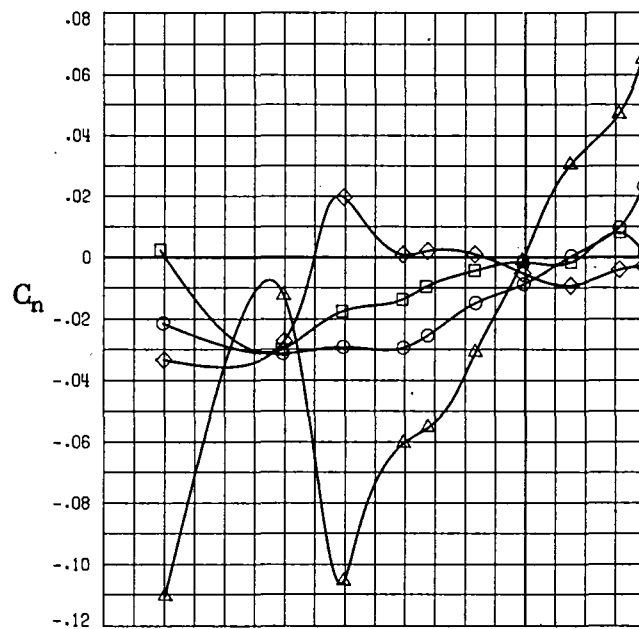
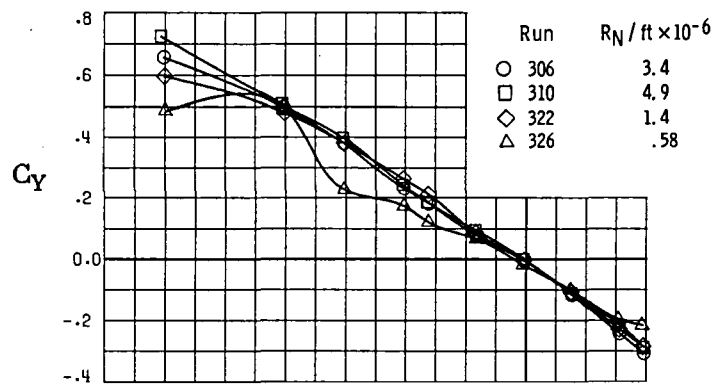
(d) $\alpha = -80^\circ$; $\delta_c = 30^\circ$; $\delta_f = -10^\circ$; $\delta_s = -30^\circ$.

Figure 13.- Continued.



(e) $\alpha = -60^\circ$; $\delta_C = 30^\circ$; $\delta_F = -10^\circ$; $\delta_S = -30^\circ$.

Figure 13.- Continued.



(f) $\alpha = -40^\circ$; $\delta_c = 30^\circ$; $\delta_f = -10^\circ$; $\delta_s = -30^\circ$.

Figure 13.- Concluded.

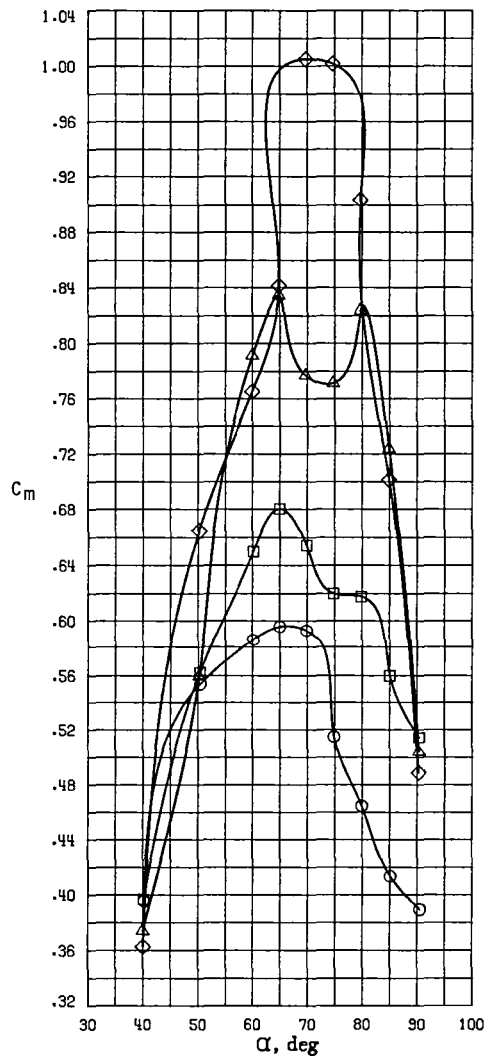
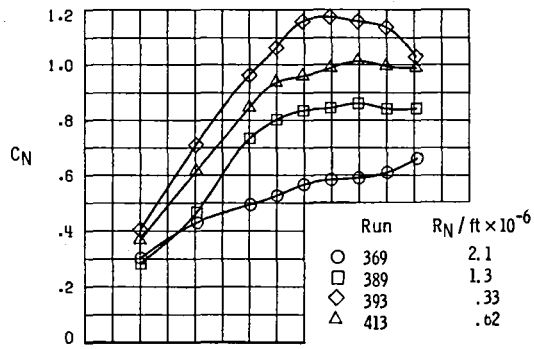
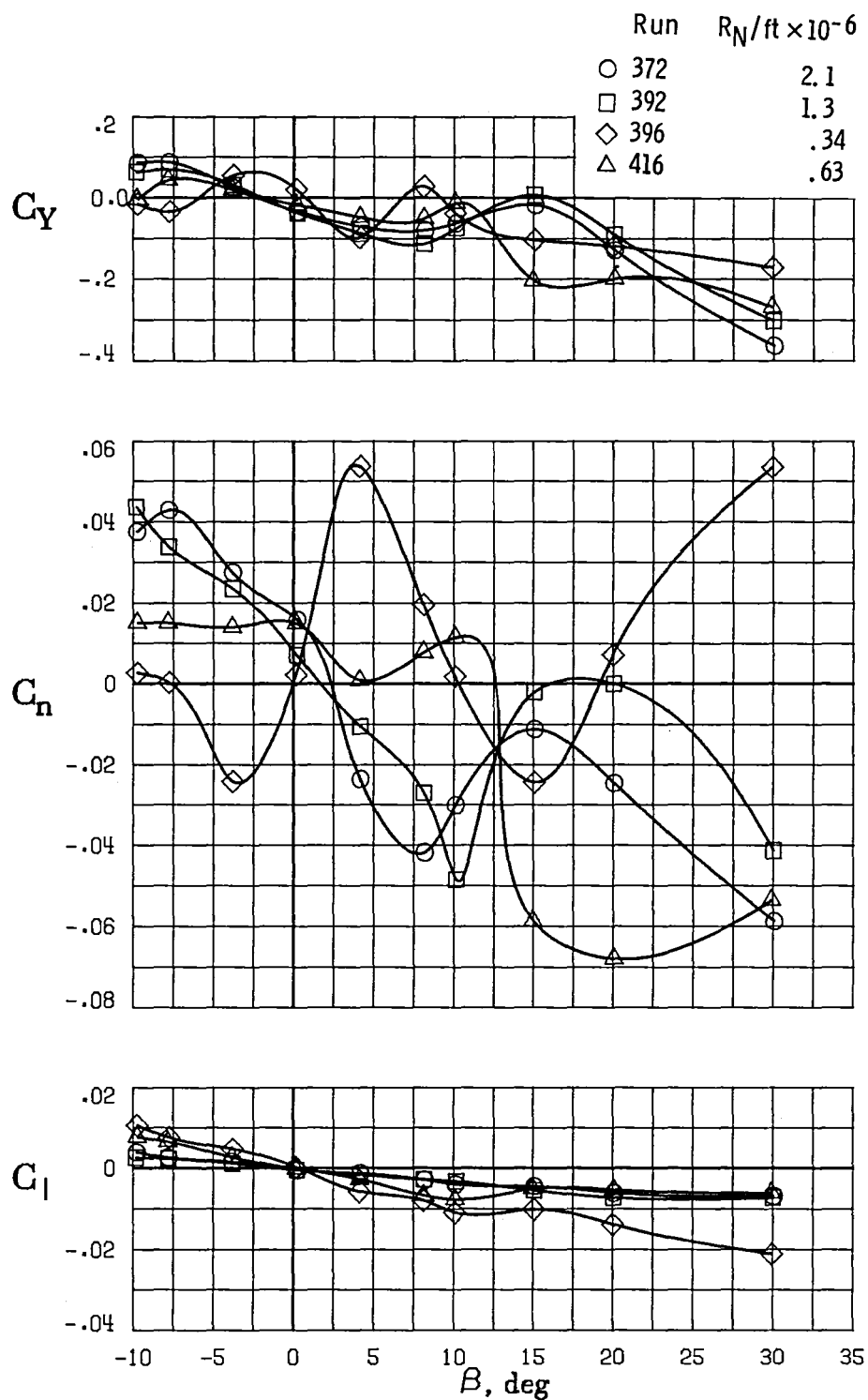
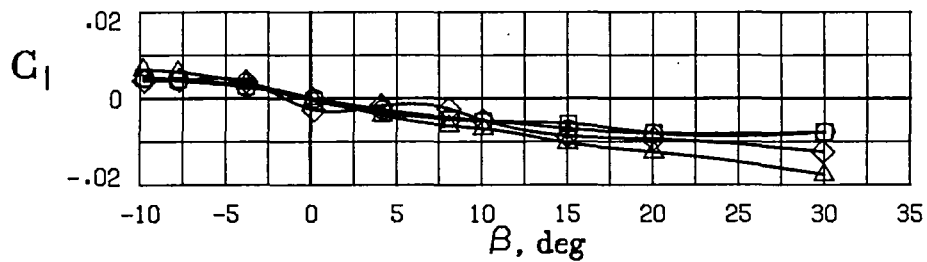
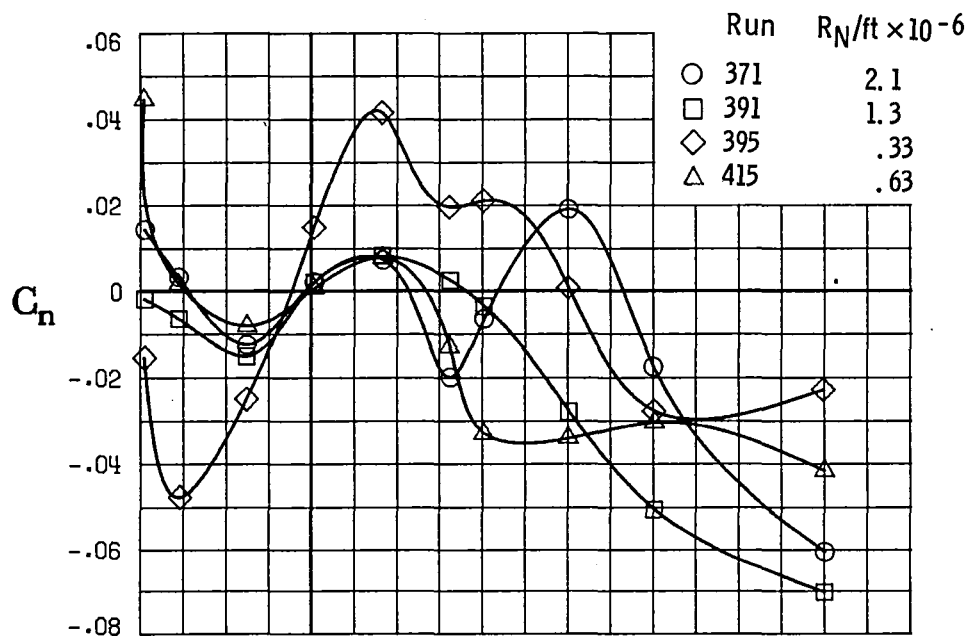
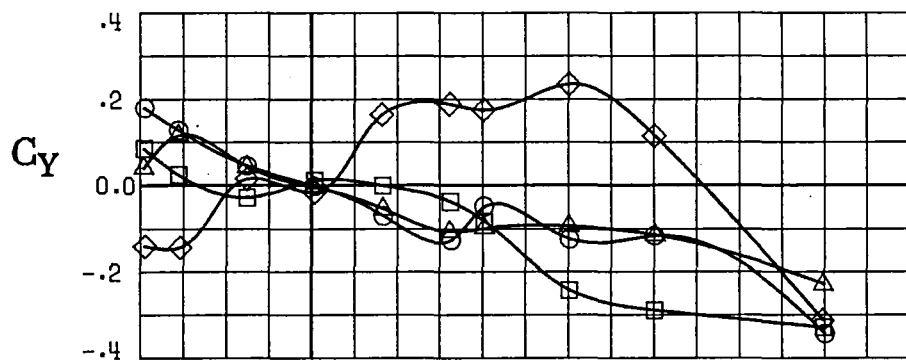


Figure 14.- Longitudinal aerodynamic characteristics of fuselage with canards. Wing off; tail off; strakes off for various Reynolds numbers; $\beta = 0^\circ$; $\delta_c = -60^\circ$.



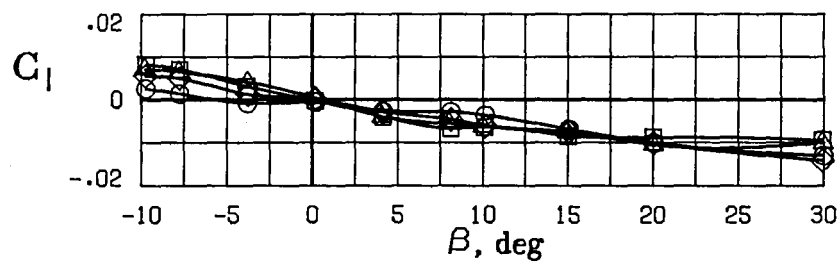
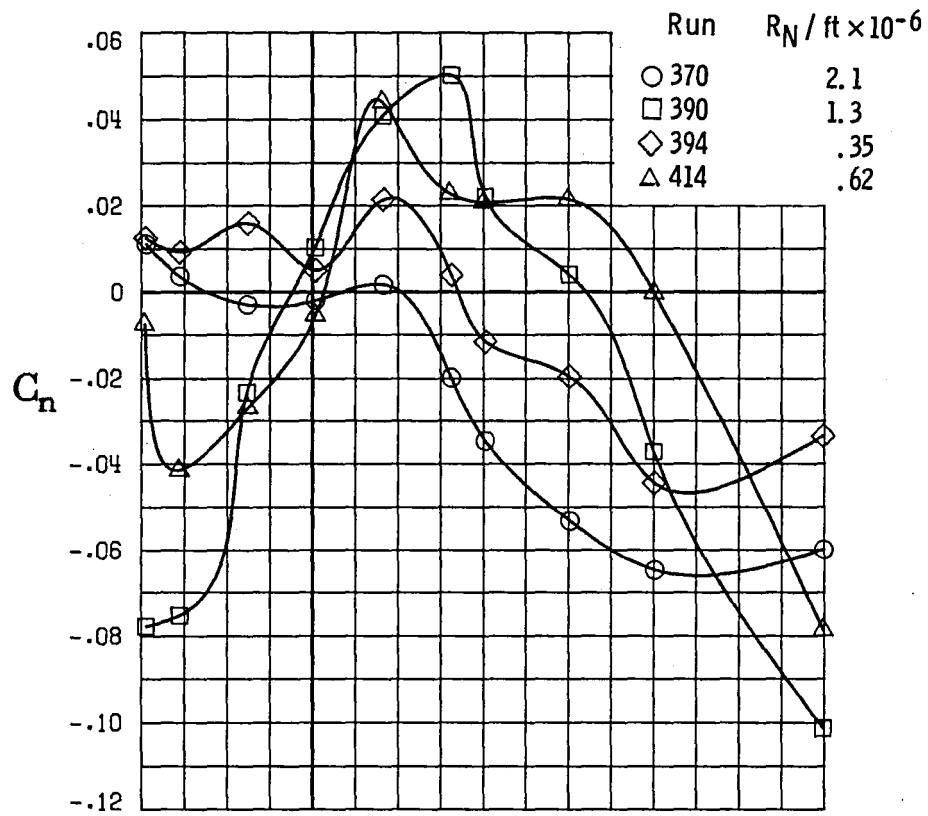
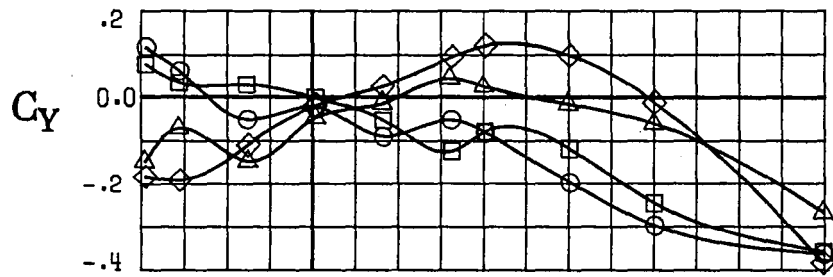
(a) $\alpha = 40^\circ$; $\delta_c = -60^\circ$.

Figure 15.- Lateral-directional aerodynamic characteristics of fuselage with canards. Wing off; tail off; strakes off for various Reynolds numbers.



(b) $\alpha = 60^\circ$; $\delta_c = -60^\circ$.

Figure 15.- Continued.



(c) $\alpha = 80^\circ$; $\delta_c = -60^\circ$.

Figure 15.- Concluded.

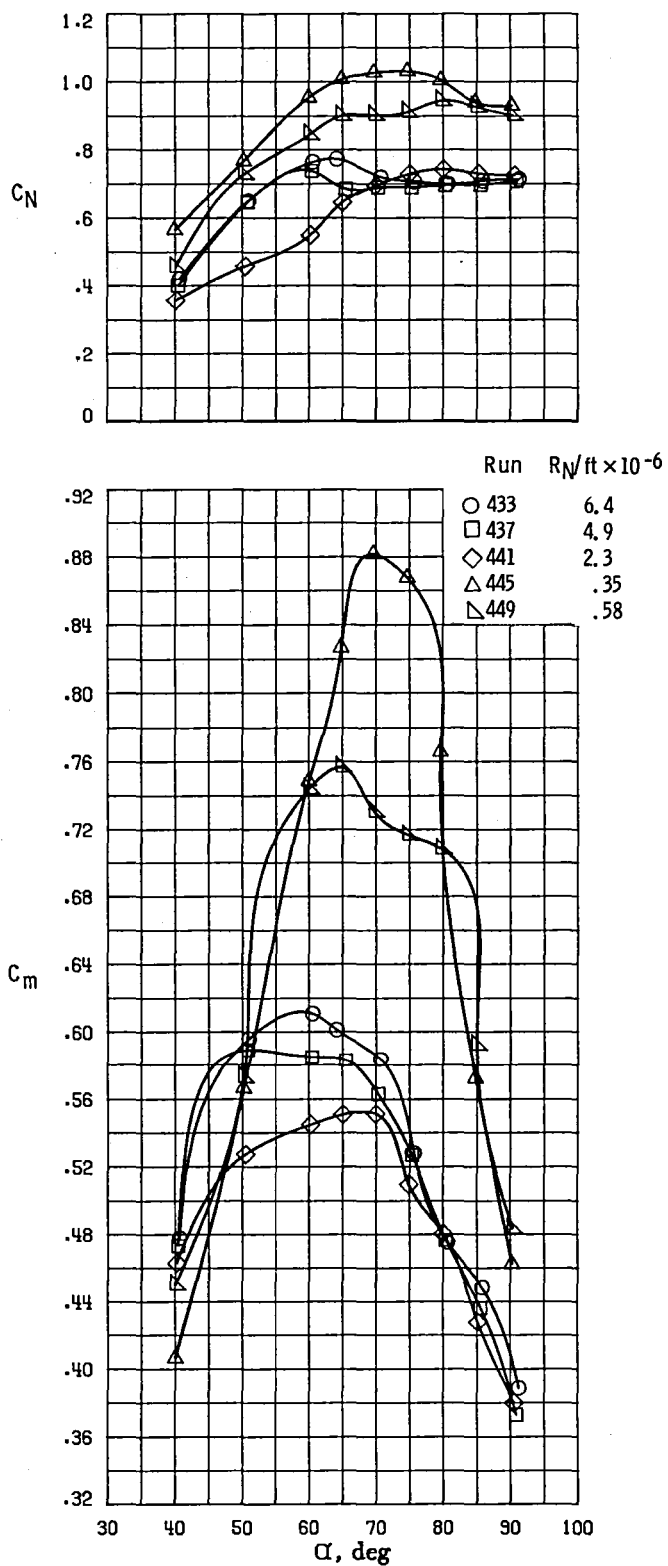
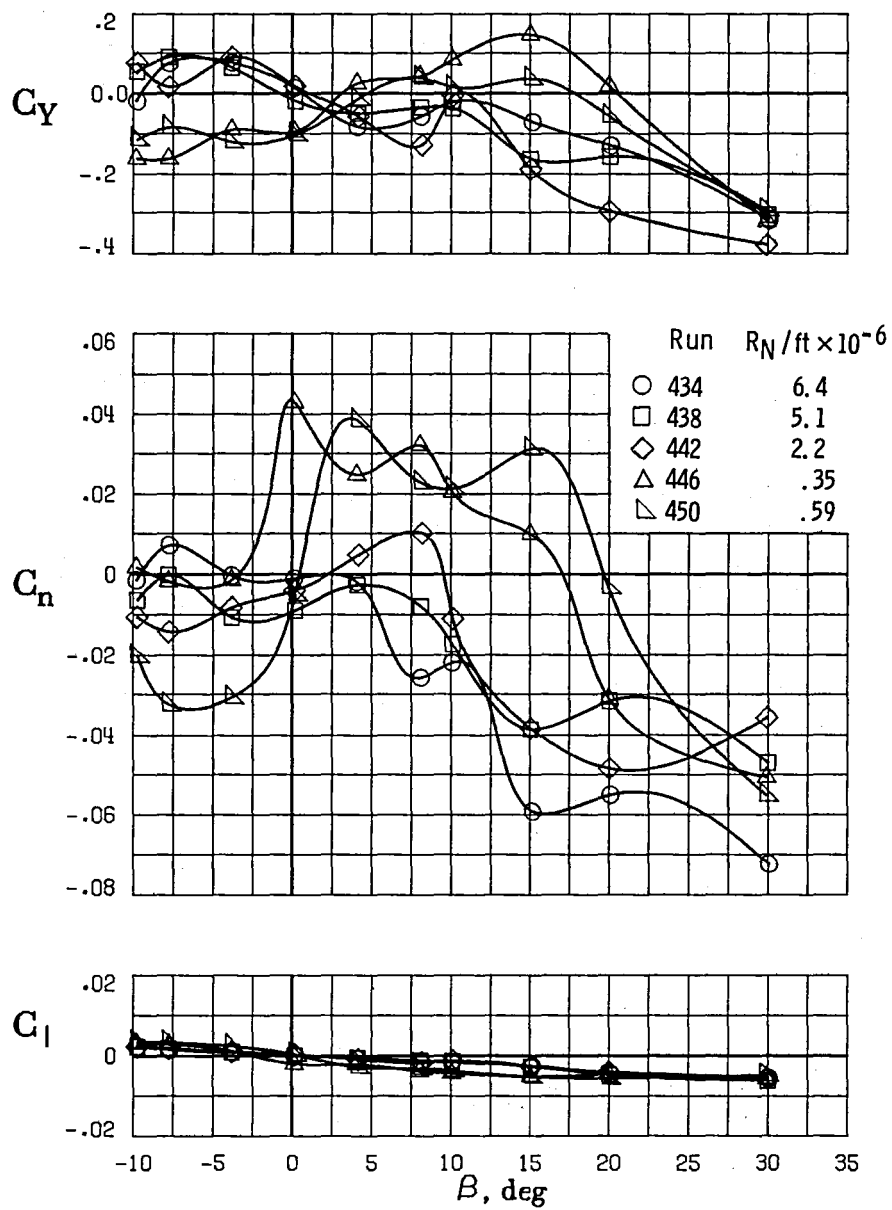
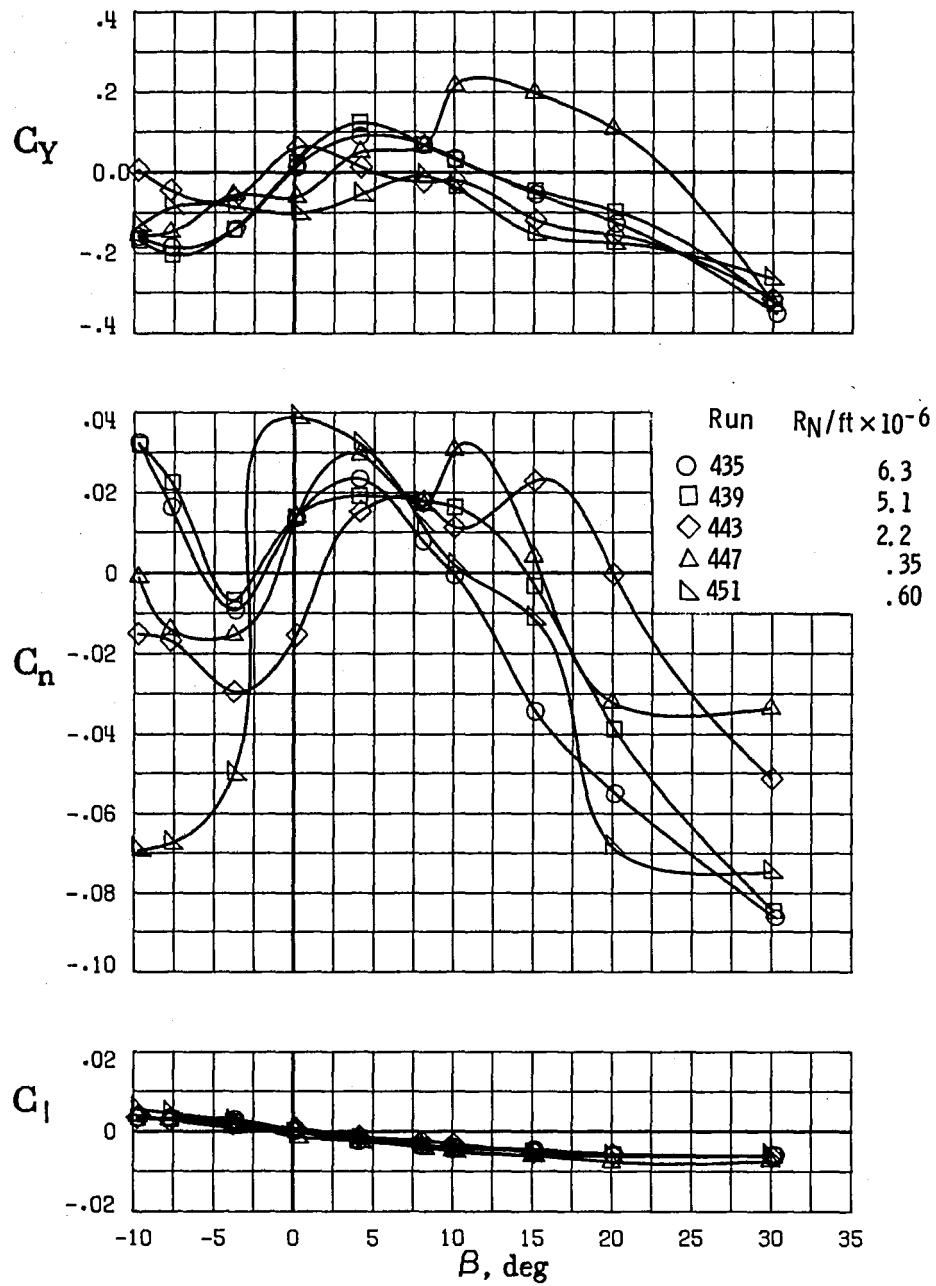


Figure 16.- Longitudinal aerodynamic characteristics of fuselage alone for various Reynolds numbers with $\beta = 0^\circ$.



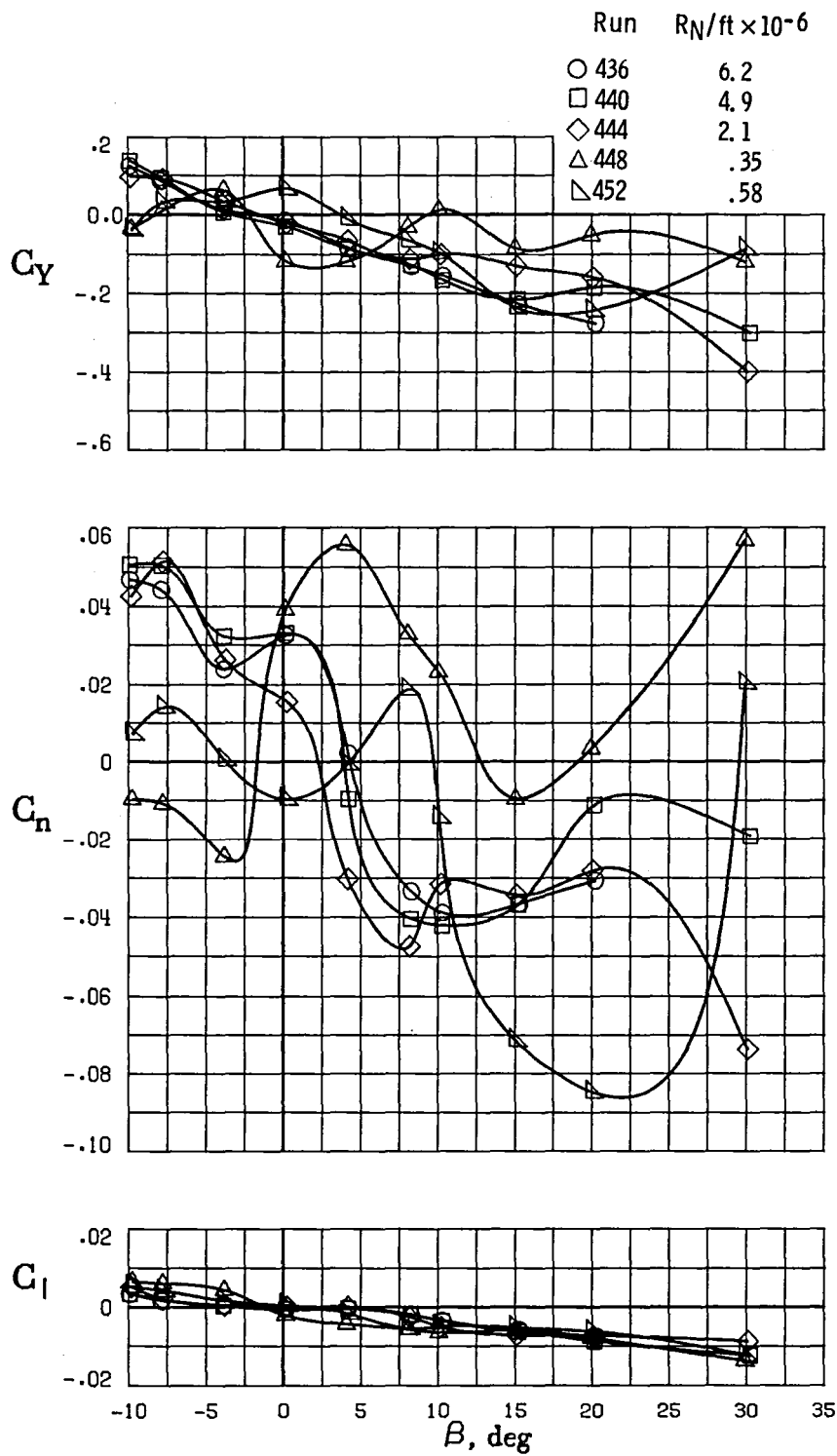
(a) $\alpha = 80^\circ$.

Figure 17.- Lateral-directional aerodynamic characteristics of fuselage alone for various Reynolds numbers.



(b) $\alpha = 60^\circ$.

Figure 17.- Continued.



(c) $\alpha = 40^\circ$.

Figure 17.- Concluded.

APPENDIX

TABULATED DATA

RUN	6	Q= 60.00 PSF	RN/FT= 1.407	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.83	-.01	1.9699	-.0631	-.2215	-.0218	.0111	-.0023
50.82	.17	2.1625	-.0870	-.2802	.0064	-.0059	.0045
60.63	.14	2.1925	-.1040	-.3651	-.0004	-.0036	.0001
70.27	.18	2.2171	-.1132	-.4683	-.0061	-.0069	-.0004
80.21	.13	2.2350	-.1199	-.5497	-.0210	-.0155	.0019
90.73	-.03	2.1470	-.1234	-.6171	-.0365	-.0347	.0007

RUN	7	Q= 52.50 PSF	RN/FT= 1.301	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.67	*****	2.0004	-.0704	-.1461	.0998	.0301	.0244
40.68	-5.08	1.9416	-.0662	-.1913	.0947	-.0012	.0131
40.66	.01	1.9631	-.0646	-.2180	-.0227	.0121	-.0019
40.66	5.13	1.9543	-.0645	-.1893	-.0733	.0073	-.0151
40.66	10.01	2.0118	-.0692	-.1285	-.0868	-.0320	-.0243
40.69	14.98	2.1140	-.0709	-.1393	-.0451	-.0408	-.0253
40.71	20.03	2.1112	-.0699	-.1258	-.0890	-.0485	-.0582

APPENDIX - Continued

RUN 8		Q= 58.40 PSF		RN/FT= 1.364		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
60.63	-9.95	2.2153	-.1041	-.2503	.0288	.0477	.0109
60.62	-4.92	2.2147	-.1041	-.2963	-.0095	.0048	.0035
60.58	-.03	2.1767	-.1041	-.3620	.0052	-.0029	-.0005
60.59	5.04	2.2191	-.1045	-.3045	.0194	-.0048	-.0038
60.60	10.10	2.2279	-.1015	-.2552	-.0288	-.0430	-.0118
60.63	15.06	2.2257	-.1028	-.2016	-.1161	-.0842	-.0191

RUN 9		Q=132.50 PSF		RN/FT= 3.033		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
41.02	.18	2.0212	-.0624	-.2183	.0001	.0147	-.0005
51.32	.23	2.2085	-.0845	-.2908	-.0033	-.0008	.0019
61.08	.19	2.2145	-.1005	-.3529	.0048	.0065	.0002
70.76	.20	2.2234	-.1143	-.4633	.0078	.0032	.0009
80.66	.13	2.2080	-.1150	-.6444	.0006	-.0015	.0009
91.12	.14	2.1383	-.1219	-.7766	-.0037	-.0047	.0022

APPENDIX - Continued

RUN 10	Q=133.40 PSF		RN/FT= 3.017		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.07	-9.81	2.0450	-.0702	-.1355	.0853	.0214	.0255
40.98	-4.81	1.9606	-.0635	-.1892	.0998	-.0153	.0148
40.98	.17	2.0081	-.0612	-.2153	-.0081	.0151	-.0010
40.96	5.13	1.9749	-.0613	-.1849	-.1073	.0224	-.0184
41.02	10.13	2.0606	-.0658	-.1090	-.0876	-.0138	-.0294
41.09	15.09	2.1650	-.0722	-.0997	-.0742	-.0382	-.0360
41.10	20.08	2.1687	-.0740	-.1104	-.1254	-.0510	-.0597

RUN 11	Q=139.60 PSF		RN/FT= 3.096		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
61.14	-9.71	2.2365	-.0982	-.3050	-.0048	.0346	.0114
61.10	-4.81	2.2325	-.0994	-.3409	-.0292	-.0031	.0053
61.08	.15	2.2232	-.1006	-.3563	.0018	.0048	-.0002
61.09	5.14	2.2481	-.0988	-.3155	.0241	.0044	-.0037
61.10	10.09	2.2368	-.0940	-.2984	-.0034	-.0260	-.0121
61.12	15.05	2.2594	-.0946	-.2926	-.0368	-.0532	-.0217
61.07	20.06	2.2196	-.0945	-.2781	-.0992	-.0608	-.0307

APPENDIX - Continued

RUN 12		Q=132.70 PSF		RN/FT= 3.004		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.65	-9.79	2.1788	-.1126	-.6598	.1064	.0635	.0226
80.62	-4.82	2.1926	-.1145	-.6523	.0617	.0368	.0123
80.62	.12	2.2018	-.1142	-.6498	.0047	-.0008	.0013
80.62	5.11	2.2125	-.1136	-.6358	-.0418	-.0343	-.0097
80.63	10.07	2.2075	-.1109	-.6379	-.0926	-.0615	-.0204
80.62	15.05	2.1918	-.1079	-.6769	-.1677	-.0899	-.0333
80.61	20.00	2.1421	-.1059	-.6925	-.2358	-.1088	-.0420

RUN 13		Q=218.40 PSF		RN/FT= 5.012		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.61	.12	2.0673	-.0641	-.1947	.0100	.0159	-.0015
51.90	.15	2.2399	-.0840	-.2612	.0037	.0143	-.0058
61.75	.14	2.2940	-.1026	-.3016	.0144	.0070	.0033
71.36	.12	2.3069	-.1052	-.4808	.0464	.0198	.0019
81.26	.16	2.2530	-.1118	-.5963	.0184	.0083	.0019
91.69	.15	2.1745	-.1208	-.7101	.0115	.0046	.0014

APPENDIX - Continued

RUN 14 Q=236.20 PSF RN/FT= 5.187 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
81.22	-9.78	2.2301	-.1117	-.6260	.0669	.0524	.0223
81.20	-4.80	2.2466	-.1113	-.6028	.0379	.0298	.0119
81.21	.15	2.2713	-.1121	-.6023	.0249	.0087	.0016
81.17	5.08	2.2456	-.1082	-.6079	-.0043	-.0205	-.0100
81.18	10.09	2.2251	-.1068	-.6223	-.0767	-.0506	-.0204
81.26	15.09	2.2060	-.1064	-.6147	-.1434	-.0717	-.0321
81.25	20.03	2.1733	-.1052	-.6342	-.2102	-.0923	-.0423

RUN 15 Q=228.90 PSF RN/FT= 5.091 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
61.74	-9.74	2.2543	-.0984	-.2963	-.0099	.0232	.0127
61.70	-4.78	2.2640	-.0990	-.3179	-.0342	-.0035	.0042
61.71	.19	2.2831	-.1021	-.3072	.0134	.0082	.0033
61.69	5.10	2.2646	-.0982	-.2951	.0304	.0030	-.0032
61.70	10.15	2.2630	-.0945	-.2889	-.0118	-.0317	-.0114
61.67	15.14	2.2105	-.0876	-.3228	-.0866	-.0705	-.0209
61.70	20.18	2.2114	-.0896	-.3435	-.1717	-.0947	-.0318

APPENDIX - Continued

RUN 16		Q=218.30 PSF		RN/FT= 4.958		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.67	-9.83	2.0599	-.0729	-.1070	.1099	.0032	.0311
41.60	-4.77	2.0156	-.0645	-.1658	.0893	-.0244	.0122
41.70	.11	2.0677	-.0633	-.1932	.0155	.0178	-.0017
41.58	5.12	2.0268	-.0630	-.1590	-.1015	.0334	-.0169
41.64	10.12	2.0696	-.0685	-.0842	-.1200	.0101	-.0329
41.76	15.18	2.1325	-.0750	-.0473	-.1512	-.0318	-.0427
41.78	20.26	2.0729	-.0757	-.0277	-.2879	-.0578	-.0658

RUN 17		Q= 56.70 PSF		RN/FT= 1.380		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.57	.18	1.9600	-.0497	-.2170	.0012	.0098	-.0015
50.77	.16	2.1797	-.0749	-.2860	.0236	-.0042	.0042
70.25	.18	2.2371	-.0980	-.4735	.0111	-.0035	.0008
60.54	.16	2.1884	-.0914	-.3634	.0167	.0002	.0006
80.20	.19	2.2136	-.1057	-.5408	-.0093	-.0279	.0014
90.74	.17	2.1615	-.1104	-.5956	.0009	-.0123	.0014

APPENDIX - Continued

RUN 18		Q= 60.50 PSF		RN/FT= 1.382		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.24	-9.80	2.2315	-.1036	-.4688	-.0002	-.0165	.0236
80.22	-4.80	2.2502	-.1060	-.4696	-.0291	-.0363	.0136
80.20	.16	2.2169	-.1079	-.5454	-.0341	-.0265	.0021
80.18	5.12	2.2377	-.1036	-.5246	.0181	.0109	-.0115
80.17	10.06	2.2146	-.0980	-.5201	.0185	-.0094	-.0225
80.16	15.03	2.1855	-.0943	-.5010	-.0678	-.0340	-.0328
80.16	20.00	2.1674	-.0915	-.4870	-.1586	-.0695	-.0415

RUN 19		Q= 58.30 PSF		RN/FT= 1.346		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.58	-9.74	2.1955	-.0932	-.2487	.0372	.0499	.0108
60.55	-4.82	2.1959	-.0937	-.2998	-.0022	.0057	.0037
60.52	.16	2.1580	-.0931	-.3566	.0125	.0008	-.0002
60.53	5.07	2.2036	-.0940	-.2918	.0334	-.0022	-.0038
60.54	10.09	2.2066	-.0921	-.2363	.0076	-.0318	-.0121
60.55	15.06	2.2316	-.0930	-.1512	-.0199	-.0437	-.0210
60.55	20.01	2.2048	-.0923	-.1824	-.1246	-.0880	-.0281

APPENDIX - Continued

RUN 20		Q= 56.70 PSF		RN/FT= 1.322		MACH=0.20	
ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.60	-9.74	1.9851	-.0586	-.1627	.0785	.0222	.0222
40.58	-4.78	1.9283	-.0571	-.1907	.0976	-.0046	.0142
40.55	.13	1.9388	-.0554	-.2159	-.0101	.0103	-.0020
40.55	5.13	1.9454	-.0554	-.1913	-.0653	.0073	-.0144
40.56	10.09	2.0029	-.0584	-.1555	-.0363	-.0220	-.0208
40.56	15.05	1.9571	-.0583	-.0575	-.0685	.0082	-.0466
40.58	20.02	1.9712	-.0689	.1644	-.0787	.0399	-.0532

RUN 21		Q= 56.60 PSF		RN/FT= 1.365		MACH=0.20	
ALPHA	BETA	C_N	C_A	C_m	C_Y	C_n	C_l
40.57	.16	2.1819	.0410	-.3885	-.0093	.0061	.0013
50.82	.15	2.3775	-.0666	-.3360	.0205	-.0087	.0085
60.65	.14	2.4048	-.1393	-.2927	-.0033	.0025	.0035
70.35	.15	2.4637	-.1790	-.3645	-.0073	-.0010	.0009
80.30	.17	2.4216	-.2164	-.3882	.0009	.0043	.0011
90.83	.14	2.4080	-.2551	-.3768	-.0135	-.0090	.0024

APPENDIX - Continued

RUN	22	Q= 58.20 PSF	RN/FT= 1.361	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.66	-9.74	2.2510	.0390	-.3624	.0209	.0269	.0205
40.64	-7.78	2.1924	.0405	-.3497	.0446	.0158	.0191
40.62	-3.82	2.1659	.0411	-.3702	.0727	-.0014	.0060
40.59	.14	2.1681	.0429	-.3861	-.0185	.0070	.0004
40.61	4.15	2.1737	.0410	-.3683	-.0560	.0067	-.0053
40.63	8.11	2.2273	.0408	-.3601	-.0215	-.0143	-.0142
40.66	10.08	2.2720	.0369	-.3523	-.0065	-.0254	-.0158
40.68	15.05	2.3308	.0427	-.3596	.0456	-.0333	-.0413
40.67	20.00	2.3282	.0409	-.3433	.0059	-.0367	-.0564
40.72	29.88	2.3032	.0575	.2625	.0112	.0594	-.0713

RUN	23	Q= 59.10 PSF	RN/FT= 1.364	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
50.94	29.92	2.5197	-.0426	.0202	-.0354	-.0056	-.1057
50.94	20.03	2.5213	-.0465	-.2414	-.0531	-.0529	-.0559
50.89	15.06	2.4991	-.0475	-.2322	.0004	-.0463	-.0413
50.88	10.09	2.4630	-.0483	-.2803	.0609	-.0312	-.0317
50.86	8.11	2.4261	-.0502	-.2957	.0572	-.0289	-.0223
50.85	4.11	2.3652	-.0578	-.3292	.0528	-.0232	-.0009
50.85	.18	2.3522	-.0696	-.3284	.0171	-.0071	.0080
50.86	-3.82	2.3771	-.0594	-.3366	-.0626	.0270	.0052
50.88	-7.78	2.5177	-.0571	-.2978	-.0701	.0441	.0329
50.91	-9.75	2.5478	-.0562	-.2993	-.0770	.0488	.0373

APPENDIX - Continued

RUN 24		Q= 59.30 PSF		RN/FT= 1.362		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.61	-9.76	2.3892	-.0927	-.3584	.0447	.0783	.0133
60.60	-7.76	2.3991	-.0985	-.3566	.0301	.0602	.0104
60.59	-3.83	2.4072	-.1282	-.3054	-.0042	.0211	.0045
60.60	.14	2.3957	-.1405	-.2888	-.0032	.0043	.0019
60.60	4.13	2.3952	-.1276	-.3049	-.0163	-.0171	-.0020
60.60	8.09	2.3841	-.1126	-.3274	-.0607	-.0477	-.0086
60.59	10.11	2.3924	-.1059	-.3364	-.0875	-.0634	-.0124
60.61	15.05	2.3449	-.1012	-.3176	-.1470	-.0898	-.0200
60.62	20.05	2.3345	-.1041	-.2778	-.1934	-.1004	-.0294
60.64	29.92	2.3428	-.0975	-.0295	-.1294	-.0295	-.0562

RUN 25		Q= 58.30 PSF		RN/FT= 1.347		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.46	29.92	2.2841	-.0993	-.1860	-.2689	-.1007	-.0574
65.47	20.05	2.3449	-.1209	-.3618	-.2447	-.1435	-.0290
65.45	15.03	2.3731	-.1302	-.3561	-.1275	-.1012	-.0216
65.46	10.09	2.4117	-.1345	-.3643	-.0735	-.0744	-.0126
65.45	8.12	2.4136	-.1339	-.3705	-.0514	-.0610	-.0089
65.45	4.12	2.4360	-.1386	-.3690	-.0269	-.0294	-.0037
65.45	.18	2.4344	-.1390	-.3632	-.0138	-.0028	.0012
65.47	-3.81	2.4315	-.1315	-.3689	.0071	.0313	.0059
65.46	-7.79	2.4279	-.1300	-.3706	.0246	.0662	.0110
65.46	-9.80	2.4127	-.1282	-.3659	.0454	.0791	.0141

APPENDIX - Continued

RUN 26		Q= 58.60 PSF		RN/FT= 1.346		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
70.33	-9.80	2.4287	-.1755	-.3838	.0752	.0902	.0171
70.32	-7.79	2.4334	-.1777	-.3828	.0552	.0759	.0136
70.31	-3.81	2.4480	-.1783	-.3643	.0266	.0390	.0068
70.32	.05	2.4644	-.1794	-.3610	-.0036	.0022	.0020
70.31	4.14	2.4681	-.1791	-.3715	-.0365	-.0322	-.0046
70.31	8.10	2.4472	-.1736	-.3835	-.0628	-.0653	-.0114
70.30	10.10	2.4260	-.1702	-.3786	-.0842	-.0798	-.0159
70.35	15.06	2.4055	-.1599	-.3889	-.1478	-.1070	-.0249
70.36	20.03	2.3496	-.1472	-.3507	-.2377	-.1534	-.0331
70.32	29.91	2.3305	-.1360	-.1432	-.1514	-.0773	-.0527
RUN 27		Q= 57.60 PSF		RN/FT= 1.332		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
75.29	29.90	2.3517	-.1624	-.1648	-.1173	-.0727	-.0545
75.31	20.03	2.4040	-.1817	-.3238	-.1436	-.1338	-.0357
75.27	15.06	2.3841	-.1882	-.3841	-.1350	-.0956	-.0293
75.28	10.10	2.4212	-.1985	-.3700	-.0597	-.0613	-.0197
75.29	8.11	2.4467	-.1999	-.3759	-.0505	-.0508	-.0146
75.26	4.12	2.4623	-.2104	-.3933	-.0235	-.0311	-.0069
75.27	.16	2.4501	-.2096	-.3880	.0021	.0025	.0011
75.28	-3.80	2.4569	-.2114	-.3828	.0228	.0338	.0093
75.27	-7.79	2.4498	-.2076	-.3494	.0407	.0484	.0186
75.29	-9.78	2.4613	-.2076	-.3087	.0043	.0569	.0218

APPENDIX - Continued

RUN 28		Q= 58.70 PSF		RN/FT= 1.340		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
80.33	-9.76	2.4492	-.2270	-.3449	.0085	.0338	.0257
80.32	-7.77	2.4688	-.2264	-.2969	-.0217	-.0005	.0217
80.30	-3.80	2.4573	-.2159	-.3204	-.0455	-.0187	.0130
80.27	.17	2.4390	-.2194	-.3827	.0000	.0044	.0006
80.26	4.14	2.4484	-.2152	-.3758	.0003	-.0006	-.0090
80.25	8.07	2.4453	-.2039	-.3443	.0068	-.0091	-.0187
80.25	10.11	2.4220	-.2146	-.3399	-.0043	-.0220	-.0224
80.24	15.06	2.4093	-.2113	-.3437	-.0721	-.0539	-.0327
80.23	20.00	2.3789	-.1973	-.3509	-.1265	-.0871	-.0423
80.23	29.88	2.3118	-.1825	-.2855	-.1591	-.1135	-.0592
RUN 29		Q= 57.70 PSF		RN/FT= 1.327		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
85.51	29.87	2.2982	-.2049	-.3169	-.1314	-.0928	-.0644
85.52	20.04	2.3611	-.2093	-.3815	-.1138	-.0828	-.0449
85.54	15.05	2.4050	-.2222	-.3629	-.0421	-.0403	-.0365
85.54	10.07	2.4222	-.2316	-.3722	.0112	-.0118	-.0259
85.53	8.11	2.4163	-.2305	-.3730	.0177	-.0005	-.0219
85.55	4.11	2.4234	-.2329	-.3891	.0307	.0086	-.0107
85.55	.12	2.4374	-.2352	-.3856	-.0388	-.0325	.0032
85.58	-3.79	2.4363	-.2340	-.3235	-.0939	-.0382	.0143
85.59	-7.73	2.4358	-.2369	-.3255	-.0591	-.0130	.0236
85.59	-9.78	2.4159	-.2365	-.3635	-.0144	.0279	.0281

APPENDIX - Continued

RUN 30		Q= 58.40 PSF		RN/FT= 1.332		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
90.85	-9.77	2.3974	-.2438	-.3857	-.0134	.0207	.0300
90.86	-7.74	2.4080	-.2466	-.3857	-.0217	.0102	.0255
90.85	-3.81	2.4194	-.2521	-.3733	-.0286	-.0040	.0152
90.84	.15	2.4206	-.2571	-.3666	-.0260	-.0103	.0022
90.84	4.11	2.4213	-.2513	-.3649	.0068	.0047	-.0100
90.81	8.08	2.4084	-.2418	-.3955	.0271	.0017	-.0237
90.81	10.04	2.4066	-.2398	-.4055	.0031	-.0080	-.0276
90.80	15.02	2.3897	-.2290	-.4012	-.0392	-.0334	-.0388
90.80	19.97	2.3560	-.2138	-.4064	-.0952	-.0706	-.0466
90.79	29.86	2.2864	-.2159	-.3390	-.1168	-.0754	-.0684
RUN 31		Q= 57.30 PSF		RN/FT= 1.318		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
90.89	24.93	2.3236	-.2067	-.3842	-.1186	-.0768	-.0571
85.53	24.92	2.3497	-.2050	-.3370	-.0975	-.0765	-.0552
80.30	24.93	2.3516	-.1858	-.3076	-.1532	-.1061	-.0509
75.29	24.95	2.3689	-.1718	-.2739	-.1685	-.1202	-.0451
70.35	24.96	2.3570	-.1447	-.2445	-.1849	-.1216	-.0411
65.50	24.95	2.3457	-.1196	-.1681	-.1806	-.0952	-.0388
60.64	24.95	2.4348	-.1174	-.1433	-.1464	-.0664	-.0512
50.93	24.92	2.4735	-.0398	-.0918	-.0031	-.0037	-.0694
40.69	24.95	2.1887	.0255	.0005	-.1334	.0027	-.0595

APPENDIX - Continued

RUN 32		Q= 57.70 PSF		RN/FT= 1.323		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.74	.17	2.4148	-.0863	-.1944	-.0014	.0011	.0040
51.04	.15	2.6562	-.1817	-.0733	.0215	-.0061	.0060
60.73	.16	2.6484	-.1945	-.0613	-.0091	-.0005	.0051
70.44	.16	2.6030	-.1697	-.2086	-.0101	.0014	.0011
80.38	.15	2.5638	-.1855	-.2662	-.0343	-.0230	.0035
90.87	.15	2.5085	-.1925	-.2946	-.0148	-.0096	.0007

RUN 33		Q= 58.10 PSF		RN/FT= 1.322		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
90.92	-9.69	2.5046	-.1885	-.3141	.0202	.0218	.0288
90.91	-7.77	2.5190	-.1922	-.3052	-.0051	.0123	.0250
90.90	-3.80	2.5217	-.1951	-.2842	-.0180	.0024	.0142
90.88	.16	2.5059	-.1944	-.3110	-.0432	-.0246	.0028
90.87	4.14	2.5149	-.1921	-.2770	-.0197	-.0029	-.0081
90.86	8.08	2.5152	-.1852	-.3105	-.0144	-.0116	-.0214
90.86	10.11	2.5076	-.1833	-.3217	-.0308	-.0163	-.0266
90.84	15.06	2.4605	-.1737	-.3279	-.0746	-.0373	-.0363
90.82	20.00	2.4242	-.1655	-.3359	-.1361	-.0682	-.0449
90.80	29.92	2.3473	-.1490	-.2642	-.1575	-.0676	-.0637

APPENDIX - Continued

RUN	34	Q= 56.70 PSF	RN/FT= 1.305	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.52	29.92	2.3742	-.1540	-.2201	-.1600	-.0868	-.0615
85.52	20.00	2.4633	-.1671	-.2922	-.1446	-.0771	-.0417
85.54	15.08	2.5076	-.1756	-.2784	-.0696	-.0398	-.0339
85.56	10.12	2.5387	-.1840	-.2777	-.0088	-.0105	-.0243
85.56	8.11	2.5424	-.1865	-.2787	.0063	.0014	-.0197
85.56	4.14	2.5585	-.1898	-.2619	.0197	.0058	-.0095
85.57	.13	2.5488	-.1898	-.2695	-.0371	-.0212	.0029
85.58	-3.79	2.5615	-.1936	-.2319	-.0779	-.0449	.0141
85.60	-7.78	2.5687	-.1902	-.2303	-.0551	-.0188	.0233
85.61	-9.76	2.5508	-.1879	-.2322	-.0386	-.0090	.0280

RUN	35	Q= 57.60 PSF	RN/FT= 1.311	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.35	-9.76	2.5715	-.1857	-.1816	-.0324	-.0086	.0262
80.34	-7.76	2.5812	-.1872	-.1869	-.0536	-.0207	.0218
80.33	-3.79	2.5923	-.1867	-.1939	-.0782	-.0414	.0125
80.30	.20	2.5740	-.1859	-.2596	-.0616	-.0310	.0036
80.29	4.11	2.5615	-.1829	-.2624	.0078	.0129	-.0089
80.28	8.11	2.5707	-.1808	-.2436	.0056	.0006	-.0189
80.27	10.07	2.5513	-.1781	-.2428	-.0089	-.0115	-.0229
80.27	15.05	2.5166	-.1690	-.2482	-.0753	-.0424	-.0323
80.26	20.00	2.4832	-.1673	-.2449	-.1531	-.0809	-.0394
80.26	29.91	2.3968	-.1714	-.1378	-.1794	-.1083	-.0598

APPENDIX - Continued

RUN 36		Q= 58.10 PSF	RN/FT= 1.315		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
75.35	29.93	2.4615	-.1850	.0065	-.0966	-.0761	-.0596
75.34	20.00	2.4798	-.1737	-.2118	-.1943	-.1226	-.0364
75.33	15.08	2.5062	-.1702	-.2602	-.1448	-.0835	-.0284
75.34	10.08	2.5475	-.1759	-.2412	-.0675	-.0417	-.0190
75.34	8.11	2.5536	-.1781	-.2385	-.0466	-.0389	-.0151
75.35	4.11	2.5562	-.1792	-.2554	-.0323	-.0188	-.0057
75.36	.16	2.5627	-.1792	-.2558	-.0041	.0028	.0018
75.38	-3.82	2.5634	-.1801	-.2335	.0023	.0186	.0087
75.41	-7.75	2.5867	-.1849	-.1630	.0035	.0168	.0176
75.42	-9.77	2.5749	-.1837	-.1610	.0126	.0285	.0224

RUN 37		Q= 56.70 PSF	RN/FT= 1.296		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.39	-9.78	2.5709	-.1735	-.2150	.0539	.0768	.0177
70.37	-7.81	2.5691	-.1718	-.2112	.0461	.0634	.0140
70.36	-3.80	2.5692	-.1694	-.2069	.0130	.0338	.0070
70.36	.18	2.5915	-.1700	-.2053	-.0144	.0014	.0012
70.35	4.15	2.5853	-.1684	-.2110	-.0395	-.0281	-.0047
70.35	8.12	2.5864	-.1705	-.2119	-.0704	-.0550	-.0123
70.35	10.13	2.5683	-.1691	-.2126	-.0930	-.0677	-.0167
70.35	15.09	2.5334	-.1681	-.2171	-.1588	-.0983	-.0269
70.36	20.05	2.5170	-.1733	-.1731	-.2434	-.1528	-.0359
70.34	29.92	2.4904	-.1865	.0318	-.1617	-.0871	-.0593

APPENDIX - Continued

RUN 38		Q= 57.40 PSF		RN/FT= 1.303		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
65.59	29.94	2.5704	-.1903	.0533	-.1919	-.0978	-.0721
65.56	20.06	2.5443	-.1784	-.1572	-.2206	-.1472	-.0373
65.55	15.05	2.5712	-.1692	-.1589	-.1295	-.0896	-.0264
65.56	10.07	2.6050	-.1677	-.1656	-.0728	-.0663	-.0159
65.56	8.08	2.5905	-.1663	-.1660	-.0625	-.0514	-.0122
65.58	4.11	2.5785	-.1651	-.1765	-.0307	-.0266	-.0043
65.58	.18	2.6064	-.1669	-.1845	-.0136	.0015	.0018
65.60	-3.78	2.5916	-.1664	-.1808	.0155	.0338	.0071
65.61	-7.77	2.5985	-.1686	-.1773	.0423	.0637	.0140
65.63	-9.75	2.5969	-.1695	-.1746	.0498	.0767	.0175

RUN 39		Q= 57.60 PSF		RN/FT= 1.301		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
60.75	-9.76	2.6381	-.1785	-.1098	.0634	.0713	.0204
60.75	-7.78	2.6351	-.1799	-.1069	.0398	.0586	.0156
60.74	-3.81	2.6380	-.1833	-.0916	.0067	.0262	.0090
60.72	.18	2.6290	-.1923	-.0620	-.0050	-.0010	.0051
60.72	4.12	2.6278	-.1825	-.0902	-.0226	-.0207	-.0052
60.72	8.13	2.6376	-.1790	-.0965	-.0589	-.0473	-.0128
60.72	10.10	2.6396	-.1784	-.0972	-.0726	-.0594	-.0178
60.72	15.07	2.6228	-.1777	-.0910	-.1261	-.0861	-.0305
60.70	20.06	2.5949	-.1797	-.0769	-.1682	-.1030	-.0450
60.67	29.91	2.5529	-.1712	.0820	-.1176	-.0347	-.0792

APPENDIX - Continued

RUN 40		Q= 56.40 PSF		RN/FT= 1.286		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
50.95	29.91	2.5948	-.1203	.0747	-.0453	-.0054	-.1171
51.00	20.05	2.7278	-.1456	-.0996	-.0844	-.0699	-.0660
50.99	15.06	2.6480	-.1436	-.0798	-.0581	-.0467	-.0425
50.98	10.10	2.6457	-.1558	-.0701	.0246	-.0301	-.0324
50.99	8.13	2.6582	-.1606	-.0764	.0419	-.0315	-.0254
50.99	4.13	2.6456	-.1690	-.0819	.0501	-.0249	-.0089
51.02	.17	2.6401	-.1816	-.0732	.0242	-.0079	.0061
51.02	-3.78	2.6519	-.1700	-.0820	-.0495	.0280	.0140
51.05	-7.76	2.7004	-.1685	-.0566	-.0283	.0493	.0380
51.07	-9.76	2.7280	-.1661	-.0506	.0076	.0550	.0405

RUN 41		Q= 58.50 PSF		RN/FT= 1.307		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.76	-9.74	2.4221	-.0782	-.1676	.0354	.0126	.0276
40.74	-7.78	2.4012	-.0798	-.1520	.0472	.0091	.0161
40.73	-3.84	2.3851	-.0821	-.1748	.0495	.0016	.0037
40.74	.18	2.4022	-.0839	-.1943	-.0078	.0011	.0041
40.71	4.12	2.3658	-.0816	-.1754	-.0498	.0059	-.0004
40.71	8.14	2.3981	-.0779	-.1661	-.0285	-.0072	-.0165
40.72	10.08	2.4306	-.0727	-.1793	-.0082	-.0096	-.0269
40.71	15.04	2.4524	-.0639	-.1974	.0042	-.0246	-.0514
40.67	20.03	2.4012	-.0539	-.2014	-.0432	-.0274	-.0639
40.73	29.91	2.4121	-.0577	.2196	-.1555	.0179	-.0866

APPENDIX - Continued

RUN 42		Q= 57.40 PSF		RN/FT= 1.300		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.85	.18	2.6474	-.1173	.0335	.0044	-.0014	0.0000
51.07	.15	2.8534	-.1400	.0380	.0018	-.0051	.0060
60.75	.17	2.7163	-.1339	-.0128	-.0209	-.0043	.0059
70.39	.15	2.6605	-.1245	-.1481	-.0166	.0014	.0018
80.32	.16	2.6253	-.1292	-.2214	-.0590	-.0333	.0031
90.84	.17	2.5551	-.1344	-.2569	-.0243	-.0044	.0035

RUN 43		Q= 58.10 PSF		RN/FT= 1.302		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
90.88	-9.73	2.5486	-.1312	-.2781	.0191	.0287	.0275
90.87	-7.77	2.5588	-.1339	-.2780	.0061	.0156	.0241
90.86	-3.80	2.5606	-.1349	-.2494	-.0210	.0084	.0141
90.85	.17	2.5610	-.1370	-.2522	-.0435	-.0136	.0022
90.84	4.13	2.5684	-.1309	-.2548	-.0240	-.0111	-.0116
90.83	8.09	2.5620	-.1263	-.2851	-.0160	-.0206	-.0233
90.82	10.09	2.5524	-.1253	-.2903	-.0510	-.0211	-.0253
90.80	15.06	2.5094	-.1197	-.3085	-.0891	-.0439	-.0354
90.80	20.01	2.4840	-.1126	-.3241	-.1567	-.0683	-.0448
90.78	29.92	2.3569	-.0995	-.2568	-.1777	-.0698	-.0647

APPENDIX - Continued

RUN 44		Q= 57.80 PSF		RN/FT= 1.298		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.47	-9.72	2.5874	-.1283	-.1925	-.0309	-.0024	.0272
85.47	-7.76	2.6054	-.1300	-.1897	-.0422	-.0142	.0235
85.47	-3.78	2.6275	-.1343	-.1944	-.0776	-.0344	.0146
85.45	.19	2.6081	-.1329	-.2092	-.0422	-.0186	.0023
85.45	4.11	2.6062	-.1303	-.2151	-.0001	.0041	-.0094
85.44	8.11	2.5883	-.1265	-.2324	-.0108	-.0061	-.0195
85.43	10.10	2.5765	-.1220	-.2544	-.0355	-.0170	-.0235
85.50	15.02	2.5613	-.1181	-.2464	-.0869	-.0436	-.0333
85.49	19.99	2.4975	-.1136	-.2636	-.1535	-.0769	-.0405
85.47	29.87	2.3993	-.1022	-.2092	-.1824	-.0795	-.0598

RUN 45		Q= 57.40 PSF		RN/FT= 1.292		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.33	-9.75	2.6095	-.1277	-.1473	-.0189	-.0086	.0252
80.33	-7.76	2.6225	-.1277	-.1484	-.0372	-.0186	.0217
80.31	-3.81	2.6250	-.1296	-.1596	-.0695	-.0394	.0127
80.29	.15	2.6286	-.1307	-.2168	-.0667	-.0340	.0033
80.28	4.14	2.6176	-.1269	-.2137	.0103	.0162	-.0091
80.28	8.09	2.6221	-.1222	-.2052	-.0163	-.0021	-.0179
80.27	10.09	2.6145	-.1198	-.2107	-.0240	-.0152	-.0222
80.27	15.06	2.5614	-.1156	-.2034	-.0903	-.0418	-.0308
80.26	20.00	2.5418	-.1147	-.1489	-.1178	-.0586	-.0390
80.25	29.91	2.4288	-.1064	-.1546	-.2078	-.1088	-.0558

APPENDIX - Continued

RUN 46		Q= 56.40 PSF		RN/FT= 1.279		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
75.32	-9.73	2.6419	-.1294	-.1012	.0230	.0173	.0228
75.31	-7.76	2.6537	-.1301	-.1031	-.0023	.0084	.0190
75.30	-3.81	2.6406	-.1287	-.1576	-.0028	.0009	.0106
75.28	.18	2.6418	-.1266	-.2066	-.0231	.0015	.0019
75.28	4.15	2.6288	-.1226	-.1949	-.0124	-.0086	-.0075
75.27	8.08	2.6297	-.1201	-.1683	-.0227	-.0147	-.0160
75.26	10.12	2.6245	-.1190	-.1661	-.0400	-.0244	-.0201
75.25	15.07	2.5775	-.1159	-.1927	-.1246	-.0736	-.0276
75.27	20.05	2.5545	-.1186	-.1074	-.1609	-.0947	-.0360
75.33	29.94	2.4912	-.1136	.0090	-.1508	-.0698	-.0541

RUN 47		Q= 57.20 PSF		RN/FT= 1.287		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.39	-9.72	2.6175	-.1215	-.1642	.0892	.0711	.0194
70.38	-7.76	2.6353	-.1230	-.1656	.0646	.0623	.0155
70.36	-3.80	2.6475	-.1230	-.1524	.0263	.0348	.0073
70.36	.16	2.6524	-.1228	-.1501	-.0168	.0008	.0015
70.35	4.15	2.6420	-.1214	-.1563	-.0528	-.0285	-.0058
70.34	8.13	2.6312	-.1194	-.1690	-.0888	-.0554	-.0130
70.34	10.09	2.6195	-.1172	-.1704	-.1085	-.0662	-.0170
70.34	15.07	2.5758	-.1138	-.1800	-.1741	-.0986	-.0258
70.34	20.06	2.5460	-.1152	-.1195	-.2465	-.1479	-.0316
70.33	29.89	2.5111	-.1134	.0382	-.1826	-.0766	-.0528

APPENDIX - Continued

RUN 48		Q= 56.00 PSF		RN/FT= 1.272		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.52	-9.74	2.6324	-.1154	-.1174	.0710	.0729	.0162
65.52	-7.76	2.6406	-.1170	-.1228	.0489	.0598	.0130
65.51	-3.80	2.6553	-.1159	-.1224	.0157	.0315	.0068
65.50	.15	2.6588	-.1161	-.1235	-.0099	.0001	.0010
65.50	4.15	2.6479	-.1145	-.1202	-.0427	-.0266	-.0041
65.50	8.14	2.6580	-.1132	-.1188	-.0809	-.0509	-.0111
65.49	10.14	2.6487	-.1125	-.1193	-.0958	-.0666	-.0148
65.49	15.07	2.6140	-.1098	-.1161	-.1547	-.0939	-.0230
65.49	20.07	2.5789	-.1129	-.1072	-.2412	-.1457	-.0314
65.56	29.93	2.5399	-.1088	.0463	-.2159	-.0884	-.0672

RUN 49		Q= 54.40 PSF		RN/FT= 1.252		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.74	-9.76	2.6692	-.1172	-.0569	.0869	.0728	.0164
60.72	-7.79	2.6654	-.1170	-.0675	.0581	.0633	.0122
60.75	-3.82	2.6999	-.1239	-.0502	.0226	.0306	.0052
60.76	.19	2.7514	-.1353	-.0086	-.0143	-.0055	.0062
60.73	4.13	2.7039	-.1213	-.0568	-.0416	-.0285	-.0026
60.72	8.14	2.6821	-.1172	-.0573	-.0602	-.0535	-.0102
60.72	10.10	2.6663	-.1151	-.0526	-.0869	-.0613	-.0135
60.72	15.07	2.6452	-.1124	-.0420	-.1560	-.0925	-.0236
60.71	20.01	2.6319	-.1193	-.0020	-.1804	-.0952	-.0335
60.71	29.91	2.6545	-.1281	.1401	-.0917	-.0248	-.0688

APPENDIX - Continued

RUN 50		Q= 55.10 PSF		RN/FT= 1.259		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
51.08	-9.77	2.9053	-.1455	.1649	.0332	.0394	.0410
51.10	-7.79	2.8990	-.1424	.1292	-.0197	.0413	.0357
51.07	-3.81	2.8496	-.1353	.0705	-.0253	.0247	.0132
51.07	.15	2.8557	-.1416	.0412	.0029	-.0050	.0069
51.06	4.12	2.8401	-.1309	.0717	.0216	-.0211	-.0132
51.06	8.13	2.8974	-.1305	.0960	.0555	-.0311	-.0301
51.07	10.08	2.9316	-.1327	.1104	.0571	-.0308	-.0378
51.07	15.06	2.9119	-.1404	.1389	-.0260	-.0473	-.0456
51.06	20.04	2.8933	-.1450	.1197	-.0863	-.0566	-.0672
51.00	29.90	2.7690	-.1305	.1824	-.0552	-.0055	-.1244

RUN 51		Q= 57.30 PSF		RN/FT= 1.283		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.84	-9.75	2.5716	-.1078	.0557	.0827	.0085	.0325
40.85	-7.78	2.5747	-.1110	.0715	.0768	.0101	.0206
40.85	.19	2.6418	-.1165	.0303	.0054	.0003	-.0011
40.83	4.14	2.5952	-.1111	.0509	-.0278	-.0037	-.0051
40.81	8.12	2.5701	-.1055	.0620	-.0513	-.0044	-.0200
40.81	10.12	2.5849	-.1035	.0543	-.0500	-.0024	-.0323
40.80	15.04	2.6040	-.0992	.0111	-.0478	-.0087	-.0549
40.77	20.02	2.5746	-.0917	-.0331	-.0562	-.0199	-.0692
40.82	29.91	2.5819	-.1024	.3840	-.1391	.0172	-.0937

APPENDIX - Continued

RUN	52	Q= 56.30 PSF	RN/FT= 1.278	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.96	.17	2.6796	-.0920	.0326	.0146	-.0034	-.0001
51.14	.12	2.9221	-.1240	.0599	-.0062	-.0061	.0086
60.78	.13	2.7446	-.1129	.0081	-.0070	-.0051	.0067
70.40	.14	2.6819	-.1073	-.1457	-.0141	.0019	.0024
80.33	.16	2.6307	-.1106	-.2158	-.0585	-.0338	.0041
90.82	.15	2.5574	-.1171	-.2874	-.0492	-.0341	.0017

RUN	53	Q= 58.30 PSF	RN/FT= 1.296	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
90.86	-9.80	2.5868	-.1102	-.2531	-.0059	-.0027	.0285
90.85	-7.82	2.5824	-.1134	-.2429	-.0300	-.0026	.0257
90.83	-3.85	2.6055	-.1166	-.2253	-.0540	-.0188	.0152
90.82	.17	2.5609	-.1179	-.2755	-.0496	-.0244	.0027
90.81	4.08	2.5863	-.1116	-.2550	-.0108	-.0132	-.0109
90.80	8.05	2.5937	-.1066	-.2934	-.0295	-.0196	-.0229
90.79	11.03	2.5640	-.1043	-.3048	-.0485	-.0304	-.0279
90.79	14.99	2.5520	-.0993	-.3143	-.0847	-.0440	-.0360
90.77	19.93	2.4935	-.0941	-.3244	-.1418	-.0696	-.0443
90.75	29.81	2.3874	-.0830	-.2533	-.1722	-.0682	-.0641

APPENDIX - Continued

RUN 54		Q= 58.10 PSF		RN/FT= 1.294		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
85.52	-9.77	2.6148	-.1103	-.1912	-.0274	-.0043	.0271
85.51	-7.81	2.6137	-.1127	-.1813	-.0317	-.0188	.0226
85.50	-3.84	2.6287	-.1140	-.1882	-.0688	-.0352	.0138
85.49	.14	2.6181	-.1126	-.2068	-.0438	-.0174	.0022
85.47	4.13	2.6061	-.1101	-.2053	-.0012	.0009	-.0110
85.46	8.06	2.6279	-.1086	-.2358	-.0025	-.0085	-.0194
85.46	10.00	2.5781	-.1051	-.2433	-.0313	-.0167	-.0238
85.45	15.01	2.5572	-.1020	-.2429	-.0812	-.0428	-.0319
85.44	19.96	2.5067	-.0963	-.2592	-.1630	-.0775	-.0408
85.47	29.84	2.4011	-.0865	-.1863	-.1765	-.0732	-.0598

RUN 55		Q= 57.90 PSF		RN/FT= 1.291		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
80.35	-9.80	2.6207	-.1068	-.1516	-.0197	-.0052	.0260
80.35	-7.85	2.6394	-.1108	-.1457	-.0375	-.0204	.0212
80.33	-3.85	2.6384	-.1099	-.1566	-.0752	-.0394	.0138
80.32	.14	2.6259	-.1113	-.2103	-.0601	-.0326	.0037
80.31	4.13	2.6421	-.1087	-.2011	.0221	.0159	-.0101
80.30	8.03	2.6113	-.1037	-.1974	-.0108	-.0031	-.0184
80.30	10.05	2.6072	-.1016	-.2067	-.0298	-.0139	-.0217
80.29	15.00	2.5843	-.0986	-.1994	-.0892	-.0429	-.0307
80.30	19.96	2.5013	-.0944	-.2089	-.1653	-.0798	-.0381
80.29	29.89	2.4223	-.0903	-.1392	-.1995	-.1015	-.0557

APPENDIX - Continued

RUN 56		Q= 57.10 PSF		RN/FT= 1.282		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
75.32	-9.77	2.6604	-.1125	-.0900	.0145	.0132	.0232
75.32	-7.81	2.6535	-.1117	-.0930	-.0101	.0026	.0176
75.30	-3.86	2.6557	-.1118	-.1342	-.0244	-.0027	.0100
75.27	.16	2.6460	-.1093	-.2016	-.0032	.0015	.0019
75.28	4.08	2.6518	-.1056	-.1806	-.0078	-.0084	-.0086
75.28	8.04	2.6408	-.1016	-.1523	-.0208	-.0098	-.0162
75.27	10.07	2.6305	-.1018	-.1489	-.0395	-.0228	-.0196
75.26	14.97	2.5785	-.0986	-.1691	-.1299	-.0651	-.0273
75.27	19.95	2.5605	-.1017	-.1050	-.1662	-.0939	-.0353
75.29	29.85	2.4877	-.0989	.0051	-.1358	-.0700	-.0533

RUN 57		Q= 56.60 PSF		RN/FT= 1.275		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.36	-9.78	2.6224	-.1053	-.1446	.0698	.0694	.0182
70.35	-7.76	2.6297	-.1050	-.1562	.0602	.0592	.0154
70.35	-3.85	2.6529	-.1070	-.1465	.0306	.0320	.0080
70.34	.11	2.6547	-.1060	-.1405	-.0132	.0016	.0025
70.33	4.06	2.6520	-.1057	-.1467	-.0580	-.0283	-.0049
70.32	8.11	2.6238	-.1012	-.1587	-.0890	-.0540	-.0132
70.32	10.07	2.6340	-.1011	-.1640	-.1180	-.0652	-.0166
70.31	15.04	2.5817	-.0968	-.1644	-.1739	-.0961	-.0254
70.33	19.97	2.5592	-.0977	-.1221	-.2431	-.1482	-.0317
70.30	29.89	2.5034	-.1003	-.0046	-.2042	-.1013	-.0505

APPENDIX - Continued

RUN	58	Q= 55.70 PSF	RN/FT= 1.265	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
65.55	29.90	2.5523	-.1008	.0920	-.1742	-.0847	-.0566
65.55	20.04	2.5630	-.0968	-.0931	-.2621	-.1467	-.0301
65.54	15.02	2.6024	-.0930	-.1081	-.1626	-.0966	-.0230
65.55	10.09	2.6426	-.0955	-.1064	-.0944	-.0650	-.0148
65.56	8.06	2.6663	-.0978	-.1100	-.0740	-.0508	-.0108
65.56	4.11	2.6534	-.0979	-.1148	-.0390	-.0267	-.0044
65.60	.11	2.6815	-.0999	-.1172	-.0127	.0000	.0017
65.62	-3.80	2.6522	-.0987	-.1191	.0144	.0313	.0064
65.63	-7.79	2.6472	-.0990	-.1171	.0517	.0605	.0134
65.64	-9.85	2.6502	-.0993	-.1156	.0709	.0744	.0162

RUN	59	Q= 58.50 PSF	RN/FT= 1.294	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
60.73	-9.85	2.6700	-.0959	-.0663	.0856	.0729	.0159
60.72	-7.82	2.6760	-.0965	-.0723	.0621	.0639	.0118
60.71	-3.84	2.6987	-.1015	-.0537	.0272	.0323	.0048
60.71	.14	2.7293	-.1123	.0025	-.0168	-.0033	.0043
60.68	4.11	2.6885	-.0975	-.0672	-.0423	-.0302	-.0029
60.68	8.10	2.6716	-.0952	-.0613	-.0709	-.0525	-.0096
60.68	10.04	2.6674	-.0937	-.0630	-.0914	-.0630	-.0131
60.69	15.03	2.6377	-.0918	-.0474	-.1640	-.0971	-.0226
60.68	20.02	2.6143	-.0957	-.0299	-.1892	-.1035	-.0310
60.67	29.88	2.6285	-.1004	.1226	-.0995	-.0264	-.0660

APPENDIX - Continued

RUN	60	Q= 57.40 PSF	RN/FT= 1.282	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
51.04	29.86	2.7712	-.1072	.2083	-.0369	.0041	-.1200
51.09	20.00	2.8927	-.1210	.1333	-.0810	-.0588	-.0627
51.09	15.08	2.8919	-.1174	.1357	-.0310	-.0500	-.0381
51.11	10.02	2.9523	-.1162	.1187	.0474	-.0302	-.0295
51.11	8.08	2.9434	-.1164	.1102	.0412	-.0299	-.0219
51.11	4.13	2.8823	-.1164	.0908	.0172	-.0218	-.0065
51.12	.14	2.8829	-.1227	.0602	-.0036	-.0068	.0085
51.12	-3.86	2.8783	-.1164	.0880	-.0195	.0263	.0099
51.16	-7.87	2.9542	-.1233	.1391	-.0303	.0455	.0284
51.18	-9.83	2.9575	-.1257	.1645	-.0014	.0445	.0364

RUN	61	Q= 57.20 PSF	RN/FT= 1.280	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.87	-9.86	2.5805	-.0945	.0848	.0736	.0084	.0316
40.86	-7.85	2.6267	-.0943	.0889	.0566	.0098	.0210
40.85	-3.84	2.6026	-.0864	.0476	-.0082	.0079	.0149
40.87	.12	2.6621	-.0921	.0316	.0113	-.0031	-.0002
40.83	4.09	2.6135	-.0873	.0540	-.0044	-.0071	-.0091
40.83	8.10	2.5935	-.0855	.0723	-.0481	-.0050	-.0200
40.84	10.04	2.6018	-.0884	.0764	-.0585	-.0037	-.0320
40.82	14.98	2.6392	-.0909	.0607	-.0604	-.0085	-.0563
40.80	19.96	2.6317	-.0865	.0125	-.0599	-.0200	-.0690
40.74	29.89	2.4383	-.0785	.1734	-.1836	-.0133	-.1155

APPENDIX - Continued

RUN 62		Q=225.90 PSF		RN/FT= 5.013		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.89	.12	2.3000	.0346	-.3601	.0225	.0100	.0019
52.19	.10	2.4723	-.0691	-.3156	-.0112	.0130	-.0047
61.95	.12	2.4846	-.1413	-.3070	-.0101	.0000	.0026
71.64	.11	2.5131	-.1747	-.3871	-.0007	.0023	.0009
81.69	.10	2.5085	-.2384	-.4275	-.0100	-.0008	.0013
92.10	.08	2.4364	-.2702	-.4951	-.0103	-.0024	.0018

RUN 63		Q=244.60 PSF		RN/FT= 5.189		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
92.18	-9.84	2.4378	-.2630	-.4905	.0206	.0408	.0298
92.15	-7.81	2.4420	-.2669	-.4818	.0251	.0300	.0241
92.12	-3.85	2.4416	-.2679	-.4931	.0055	.0155	.0129
92.07	.18	2.4521	-.2722	-.5023	-.0105	-.0046	.0021
92.08	4.07	2.4353	-.2626	-.5058	-.0300	-.0248	-.0110
91.97	8.04	2.4399	-.2616	-.5212	-.0567	-.0481	-.0216
91.99	10.01	2.4227	-.2614	-.5244	-.0671	-.0608	-.0270
91.95	15.00	2.3919	-.2520	-.5381	-.1163	-.0742	-.0384
91.93	19.96	2.3828	-.2406	-.5569	-.1560	-.0885	-.0494
91.95	29.87	2.2905	-.2393	-.5203	-.1642	-.0816	-.0704

APPENDIX - Continued

RUN 64		Q=226.10 PSF		RN/FT= 4.983		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
86.61	29.90	2.3214	-.2213	-.5049	-.1830	-.0916	-.0670
86.68	19.97	2.4003	-.2350	-.4560	-.1303	-.0723	-.0467
86.66	15.03	2.4229	-.2433	-.5029	-.1378	-.0959	-.0352
86.69	10.05	2.4545	-.2529	-.4716	-.0904	-.0700	-.0238
86.68	8.11	2.4649	-.2544	-.4608	-.0733	-.0571	-.0198
86.68	4.04	2.4731	-.2557	-.4511	-.0458	-.0319	-.0076
86.69	.08	2.4705	-.2599	-.4424	-.0074	-.0014	.0019
86.71	-3.80	2.4850	-.2583	-.4447	.0123	.0244	.0122
86.72	-7.82	2.4777	-.2581	-.4623	.0334	.0452	.0233
86.73	-9.82	2.4618	-.2546	-.4682	.0424	.0513	.0279

RUN 65		Q=227.30 PSF		RN/FT= 4.985		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
81.50	-9.81	2.4710	-.2381	-.4438	.0514	.0624	.0249
81.49	-7.89	2.4845	-.2384	-.4419	.0482	.0532	.0202
81.47	-3.87	2.4836	-.2384	-.4341	.0134	.0293	.0115
81.47	.17	2.5019	-.2413	-.4287	-.0047	-.0035	.0012
81.46	4.06	2.4926	-.2369	-.4372	-.0508	-.0364	-.0085
81.46	8.11	2.4769	-.2320	-.4553	-.0837	-.0678	-.0183
81.46	10.10	2.4668	-.2304	-.4593	-.1051	-.0790	-.0232
81.45	15.07	2.4369	-.2251	-.4841	-.1607	-.1043	-.0337
81.45	20.05	2.3850	-.2120	-.5435	-.2261	-.1269	-.0432
81.42	29.97	2.3100	-.1943	-.4662	-.1925	-.0933	-.0621

APPENDIX - Continued

RUN 66		Q=228.30 PSF		RN/FT= 4.986		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
76.44	30.01	2.2919	-.1619	-.4875	-.2440	-.1052	-.0586
76.48	20.10	2.4092	-.1826	-.4517	-.1698	-.0969	-.0415
76.46	15.05	2.4323	-.1948	-.4867	-.1757	-.1087	-.0303
76.47	10.06	2.4750	-.2043	-.4500	-.1064	-.0838	-.0196
76.49	8.10	2.4899	-.2078	-.4357	-.0863	-.0688	-.0158
76.47	4.15	2.4930	-.2111	-.4156	-.0433	-.0379	-.0065
76.50	.12	2.5090	-.2129	-.4022	-.0037	-.0009	.0015
76.50	-3.85	2.5109	-.2165	-.4119	.0180	.0365	.0087
76.52	-7.87	2.4939	-.2164	-.4327	.0373	.0597	.0187
76.53	-9.81	2.4844	-.2154	-.4305	.0462	.0635	.0228

RUN 67		Q=224.40 PSF		RN/FT= 4.930		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
71.52	-9.81	2.4770	-.1821	-.4238	.0290	.0723	.0197
71.52	-7.82	2.4936	-.1842	-.4153	.0299	.0628	.0145
71.50	-3.91	2.5065	-.1819	-.3989	.0245	.0371	.0081
71.51	.07	2.5322	-.1800	-.3996	-.0052	.0033	.0007
71.54	4.05	2.5146	-.1773	-.4023	-.0415	-.0355	-.0058
71.55	8.08	2.4955	-.1748	-.4108	-.0822	-.0678	-.0134
71.55	10.12	2.4897	-.1724	-.4243	-.1046	-.0824	-.0173
71.53	15.10	2.4298	-.1615	-.4646	-.1597	-.1045	-.0280
71.50	20.11	2.3647	-.1410	-.5196	-.2246	-.1176	-.0387
71.51	30.01	2.2690	-.1342	-.4733	-.2387	-.1120	-.0537

APPENDIX - Continued

RUN 68		Q=233.90 PSF	RN/FT= 5.022		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
66.76	30.04	2.2704	-.1080	-.3791	-.2621	-.0947	-.0537
66.72	20.12	2.3512	-.1137	-.4692	-.2184	-.1056	-.0346
66.71	15.12	2.4111	-.1256	-.4360	-.1496	-.0939	-.0251
66.81	10.05	2.4726	-.1388	-.4145	-.0928	-.0695	-.0144
66.79	8.09	2.4654	-.1384	-.4016	-.0650	-.0572	-.0113
66.79	4.12	2.4898	-.1498	-.3784	-.0365	-.0257	-.0048
66.79	.06	2.4967	-.1589	-.3616	-.0069	-.0003	.0005
66.81	-3.89	2.4785	-.1571	-.3800	.0177	.0246	.0073
66.82	-7.89	2.4705	-.1496	-.4088	.0299	.0548	.0141
66.83	-9.91	2.4680	-.1476	-.4196	.0467	.0661	.0175

RUN 69		Q=230.70 PSF	RN/FT= 4.975		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
61.88	-9.87	2.4294	-.1231	-.3581	.0289	.0412	.0163
61.87	-7.80	2.4381	-.1270	-.3480	.0214	.0287	.0128
61.87	-3.89	2.4571	-.1309	-.3338	.0010	.0127	.0057
61.87	.09	2.4679	-.1418	-.3107	-.0111	-.0012	.0022
61.86	4.14	2.4634	-.1258	-.3334	-.0305	-.0149	-.0034
61.86	8.14	2.4528	-.1141	-.3656	-.0558	-.0390	-.0099
61.85	10.19	2.4260	-.1078	-.3799	-.0769	-.0533	-.0132
61.85	15.09	2.4070	-.0959	-.3887	-.1121	-.0674	-.0223
61.95	20.12	2.4478	-.1302	-.2930	-.1256	-.0742	-.0304
61.95	30.07	2.3329	-.1111	-.2588	-.2545	-.0902	-.0510

APPENDIX - Continued

RUN 70		Q=227.20 PSF	RN/FT= 4.941		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
52.27	30.10	2.4927	-.0343	-.2868	-.2527	-.0973	-.0973
52.25	20.09	2.5884	-.0439	-.2796	-.1128	-.0723	-.0499
52.25	15.10	2.6051	-.0511	-.2762	-.0427	-.0634	-.0370
52.20	10.10	2.5214	-.0580	-.2712	.0335	-.0306	-.0196
52.08	8.03	2.4976	-.0536	-.3013	.0441	-.0350	-.0075
52.04	4.09	2.4553	-.0547	-.3259	.0407	-.0129	.0016
52.07	.08	2.4394	-.0663	-.3155	-.0122	.0118	-.0011
52.08	-3.90	2.4686	-.0669	-.3126	-.0530	.0214	.0038
52.08	-7.83	2.4889	-.0589	-.3187	-.0517	.0480	.0064
52.21	-9.83	2.5492	-.0661	-.3041	-.0457	.0508	.0204

RUN 71		Q=223.70 PSF	RN/FT= 4.920		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.83	-9.83	2.2951	.0269	-.2689	.0647	.0033	.0278
41.79	-7.87	2.2663	.0326	-.2897	.0695	-.0074	.0209
41.79	-3.86	2.2677	.0391	-.3363	.0672	-.0218	-.0010
42.03	.12	2.2985	.0413	-.3659	.0269	.0115	.0011
41.91	4.06	2.2573	.0384	-.3421	-.0838	.0315	-.0037
41.73	8.13	2.2662	.0403	-.2971	-.0830	.0112	-.0180
41.85	10.03	2.2802	.0386	-.2674	-.0841	.0049	-.0271
42.03	15.05	2.4123	.0256	-.2329	-.1011	-.0351	-.0377
41.99	20.23	2.4142	.0356	-.2665	-.1990	-.0680	-.0614
42.07	30.25	2.4594	.0419	-.4074	-.3592	-.1026	-.0965

APPENDIX - Continued

RUN 72		Q=208.90 PSF	RN/FT= 4.849		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
42.04	.09	2.5096	-.0977	-.1722	.0435	.0081	-.0024
52.23	.11	2.7098	-.1898	-.0751	.0006	.0095	.0002
62.06	.12	2.6855	-.2028	-.0717	-.0089	.0002	.0034
71.80	.10	2.6542	-.1753	-.2339	-.0035	.0008	.0014
81.80	.08	2.6394	-.2095	-.3121	-.0024	-.0008	.0013
91.07	.09	2.5624	-.2200	-.3794	-.0090	-.0008	.0017

RUN 73		Q=233.20 PSF	RN/FT= 5.127		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
91.09	-9.79	2.5394	-.2118	-.3925	.0364	.0419	.0286
91.05	-7.76	2.5552	-.2124	-.3898	.0326	.0361	.0251
91.04	-3.82	2.5542	-.2176	-.3762	.0080	.0133	.0149
91.04	.15	2.5555	-.2173	-.3837	-.0010	-.0008	.0029
91.03	4.06	2.5570	-.2164	-.3789	-.0373	-.0224	-.0086
91.02	8.09	2.5489	-.2116	-.4081	-.0657	-.0453	-.0213
90.99	10.08	2.5380	-.2086	-.4192	-.0797	-.0568	-.0259
90.94	15.01	2.4890	-.2026	-.4336	-.1290	-.0717	-.0360
90.95	19.94	2.4544	-.1938	-.4659	-.1877	-.0853	-.0460
90.86	29.82	2.3263	-.1809	-.4620	-.2138	-.0761	-.0655

APPENDIX - Continued

RUN 74		Q=223.60 PSF		RN/FT= 5.022		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
86.70	29.87	2.3618	-.1808	-.4282	-.1989	-.0875	-.0634
86.77	19.97	2.4845	-.1952	-.3763	-.1623	-.0736	-.0436
86.75	15.04	2.5061	-.1965	-.4178	-.1450	-.0818	-.0335
86.79	9.93	2.5555	-.2060	-.3904	-.0951	-.0608	-.0232
86.83	8.05	2.5887	-.2114	-.3730	-.0801	-.0482	-.0193
86.83	4.03	2.5946	-.2133	-.3584	-.0371	-.0220	-.0080
86.85	.10	2.5949	-.2163	-.3549	-.0033	-.0001	.0024
86.85	-3.87	2.5909	-.2143	-.3660	.0121	.0235	.0129
86.87	-7.82	2.5723	-.2111	-.3510	.0427	.0317	.0226
86.88	-9.83	2.5747	-.2068	-.3657	.0538	.0435	.0267

RUN 75		Q=224.50 PSF		RN/FT= 5.024		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
81.61	-9.84	2.5946	-.2002	-.3364	.0592	.0519	.0250
81.61	-7.84	2.5987	-.2036	-.3293	.0493	.0422	.0202
81.58	-3.87	2.6207	-.2072	-.3182	.0204	.0201	.0111
81.59	.14	2.6252	-.2091	-.3183	-.0079	-.0010	.0012
81.59	4.10	2.6248	-.2061	-.3208	-.0305	-.0276	-.0090
81.59	8.10	2.6167	-.2010	-.3366	-.0754	-.0526	-.0172
81.64	10.05	2.5911	-.1973	-.3421	-.0925	-.0639	-.0212
81.62	15.00	2.5434	-.1908	-.3817	-.1584	-.0889	-.0316
81.60	20.00	2.4651	-.1871	-.4210	-.2142	-.1081	-.0404
81.57	29.97	2.3898	-.1813	-.3658	-.1993	-.0904	-.0611

APPENDIX - Continued

RUN	76	Q=228.50 PSF	RN/FT= 5.060	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
76.66	29.95	2.3874	-.1876	-.3261	-.2221	-.1004	-.0609
76.68	20.05	2.5048	-.1851	-.3036	-.1654	-.0810	-.0405
76.67	15.07	2.5459	-.1831	-.3532	-.1617	-.0940	-.0307
76.70	10.08	2.5851	-.1845	-.3157	-.1082	-.0711	-.0197
76.69	8.04	2.5874	-.1853	-.2988	-.0833	-.0580	-.0147
76.71	4.13	2.6232	-.1892	-.2777	-.0453	-.0309	-.0069
76.72	.11	2.6365	-.1921	-.2650	-.0063	.0004	.0027
76.63	-3.90	2.6147	-.1903	-.2823	.0219	.0303	.0105
76.63	-7.86	2.6044	-.1903	-.3058	.0506	.0478	.0189
76.65	-9.86	2.5992	-.1904	-.3105	.0477	.0545	.0232

RUN	77	Q=222.30 PSF	RN/FT= 4.980	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
71.67	-9.86	2.5920	-.1816	-.2539	.0402	.0573	.0212
71.67	-7.79	2.6220	-.1818	-.2448	.0252	.0501	.0165
71.65	-3.85	2.6321	-.1795	-.2357	.0034	.0288	.0091
71.64	.10	2.6398	-.1765	-.2330	-.0058	.0008	.0015
71.65	4.10	2.6374	-.1743	-.2317	-.0256	-.0269	-.0058
71.65	8.12	2.6301	-.1762	-.2379	-.0654	-.0531	-.0142
71.64	10.09	2.6105	-.1771	-.2427	-.0862	-.0653	-.0177
71.63	15.10	2.5710	-.1793	-.2905	-.1468	-.0894	-.0297
71.64	20.11	2.5009	-.1791	-.3437	-.1954	-.1060	-.0404
71.75	29.99	2.4175	-.1945	-.2977	-.2313	-.1095	-.0623

APPENDIX - Continued

RUN 78		Q=218.20 PSF		RN/FT= 4.929		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
66.88	30.01	2.4800	-.1895	-.1946	-.2095	-.0984	-.0709
66.83	20.08	2.5506	-.1834	-.2488	-.1569	-.0912	-.0407
66.83	15.11	2.5981	-.1791	-.2238	-.1084	-.0821	-.0292
66.82	10.11	2.6305	-.1743	-.2033	-.0611	-.0586	-.0177
66.81	8.11	2.6291	-.1719	-.2005	-.0513	-.0483	-.0137
66.81	4.07	2.6451	-.1713	-.2002	-.0292	-.0244	-.0051
66.79	.14	2.6418	-.1739	-.2034	-.0045	.0028	.0018
66.82	-3.85	2.6356	-.1762	-.2023	.0118	.0256	.0077
66.84	-7.84	2.6372	-.1788	-.2131	.0206	.0475	.0168
66.93	-9.85	2.6367	-.1796	-.2183	.0302	.0555	.0215

RUN 79		Q=215.70 PSF		RN/FT= 4.908		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
62.05	-9.82	2.6811	-.1946	-.1531	.0341	.0406	.0228
62.06	-7.84	2.7005	-.1958	-.1386	.0191	.0334	.0181
62.08	-3.85	2.6895	-.1970	-.1121	-.0093	.0134	.0086
62.09	.16	2.6962	-.2034	-.0739	-.0095	-.0003	.0032
62.03	4.14	2.6854	-.1926	-.1103	-.0197	-.0167	-.0058
62.05	8.14	2.6686	-.1868	-.1416	-.0565	-.0430	-.0145
62.04	10.12	2.6644	-.1831	-.1634	-.0618	-.0529	-.0197
62.03	15.13	2.6496	-.1872	-.1720	-.0974	-.0682	-.0320
62.06	20.05	2.6360	-.1897	-.1619	-.1319	-.0688	-.0455
61.95	30.05	2.4861	-.1678	-.1843	-.2174	-.1029	-.0705

APPENDIX - Continued

RUN 80		Q=211.80 PSF		RN/FT= 4.869		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
52.33	30.09	2.5580	-.1206	-.1709	-.2459	-.0938	-.1053
52.35	20.07	2.6516	-.1433	-.1200	-.1505	-.0654	-.0578
52.38	15.09	2.6574	-.1492	-.1311	-.0876	-.0508	-.0408
52.35	10.04	2.6825	-.1613	-.1184	-.0135	-.0254	-.0284
52.41	8.08	2.6899	-.1646	-.1131	.0175	-.0248	-.0208
52.42	4.09	2.6758	-.1762	-.0889	.0380	-.0108	-.0057
52.42	.12	2.7019	-.1894	-.0727	-.0009	.0059	.0027
52.41	-3.83	2.6904	-.1859	-.0720	-.0399	.0160	.0109
52.37	-7.85	2.6818	-.1714	-.1063	-.0410	.0302	.0237
52.41	-9.86	2.6679	-.1692	-.1105	-.0109	.0325	.0310

RUN 81		Q=206.50 PSF		RN/FT= 4.811		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.90	-9.85	2.3999	-.0876	-.1031	.0713	-.0028	.0312
41.88	-7.77	2.4021	-.0883	-.1194	.0652	-.0093	.0221
41.87	-3.79	2.3980	-.0896	-.1413	.0242	-.0209	.0045
41.91	.10	2.4977	-.0938	-.1776	.0425	.0079	-.0025
41.86	4.08	2.4159	-.0880	-.1387	-.0567	.0274	-.0012
41.89	8.10	2.4094	-.0808	-.1168	-.0758	.0147	-.0194
41.85	10.09	2.4193	-.0788	-.0912	-.0787	.0095	-.0294
41.94	15.07	2.5021	-.0820	-.0899	-.1291	-.0263	-.0432
41.96	20.11	2.5251	-.0710	-.1379	-.1704	-.0540	-.0657
41.90	30.18	2.3803	-.0366	-.2884	-.3179	-.0990	-.1160

APPENDIX - Continued

RUN 82		Q=208.40 PSF		RN/FT= 4.839		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
41.55	.11	2.7697	-.1102	.0477	.0292	.0119	-.0007
52.66	.11	2.9453	-.1364	.0743	.0105	.0055	.0041
62.19	.14	2.7699	-.1278	-.0082	-.0068	-.0046	.0049
71.79	.12	2.7034	-.1199	-.1678	-.0064	.0010	.0025
81.75	.13	2.6970	-.1357	-.2631	-.0083	-.0015	.0020
91.11	.12	2.6045	-.1411	-.3298	-.0080	-.0005	.0027

RUN 83		Q=231.10 PSF		RN/FT= 5.087		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
91.07	-9.78	2.5841	-.1415	-.3483	.0419	.0501	.0294
91.08	-7.82	2.5985	-.1407	-.3447	.0393	.0391	.0246
91.04	-3.86	2.6147	-.1426	-.3321	.0087	.0179	.0151
91.03	.10	2.6162	-.1417	-.3313	-.0123	-.0022	.0022
91.04	4.07	2.6020	-.1376	-.3430	-.0402	-.0301	-.0106
91.02	8.04	2.5980	-.1352	-.3762	-.0979	-.0480	-.0194
90.99	10.00	2.5869	-.1330	-.3883	-.1070	-.0598	-.0244
90.97	14.99	2.5594	-.1306	-.4113	-.1426	-.0706	-.0349
90.94	19.96	2.5071	-.1287	-.4190	-.1833	-.0763	-.0437
90.91	29.85	2.3875	-.1215	-.4048	-.1994	-.0684	-.0659

APPENDIX - Continued

RUN 84		Q=230.60 PSF		RN/FT= 5.073		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
86.86	29.88	2.4182	-.1195	-.3523	-.1970	-.0713	-.0627
86.93	19.99	2.5307	-.1255	-.3746	-.2092	-.0849	-.0427
86.86	14.98	2.5801	-.1260	-.3765	-.1580	-.0717	-.0337
86.88	10.04	2.5950	-.1293	-.3641	-.1126	-.0599	-.0229
86.89	8.03	2.6097	-.1314	-.3448	-.0760	-.0524	-.0191
86.86	4.11	2.6296	-.1355	-.3323	-.0550	-.0267	-.0085
86.80	.09	2.6187	-.1397	-.3107	-.0041	-.0021	.0020
86.83	-3.83	2.6443	-.1403	-.3191	.0293	.0205	.0120
86.84	-7.84	2.6136	-.1359	-.3242	.0483	.0356	.0219
86.86	-9.80	2.5955	-.1364	-.3226	.0526	.0414	.0265

RUN 85		Q=221.40 PSF		RN/FT= 4.965		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
81.57	-9.79	2.6177	-.1311	-.2942	.0820	.0521	.0231
81.55	-7.85	2.6460	-.1337	-.2890	.0681	.0461	.0187
81.57	-3.86	2.6732	-.1352	-.2771	.0235	.0252	.0115
81.57	.12	2.6691	-.1355	-.2634	-.0012	-.0027	.0007
81.59	4.09	2.6686	-.1322	-.2807	-.0511	-.0308	-.0078
81.60	8.09	2.6515	-.1274	-.2967	-.0843	-.0557	-.0172
81.59	10.10	2.6256	-.1253	-.3031	-.1176	-.0628	-.0210
81.59	15.04	2.5948	-.1240	-.3263	-.1637	-.0867	-.0303
81.56	20.00	2.5202	-.1218	-.3643	-.2158	-.1056	-.0402
81.58	29.88	2.4437	-.1170	-.2992	-.1876	-.0756	-.0596

APPENDIX - Continued

RUN 86		Q=217.10 PSF		RN/FT= 4.916		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
76.55	29.91	2.4379	-.1135	-.2689	-.2074	-.0838	-.0569
76.61	20.04	2.5635	-.1185	-.2429	-.1640	-.0728	-.0393
76.60	15.09	2.5948	-.1185	-.2950	-.1637	-.0884	-.0293
76.62	10.09	2.6423	-.1206	-.2613	-.1076	-.0670	-.0197
76.62	8.11	2.6560	-.1220	-.2573	-.0922	-.0561	-.0152
76.60	4.09	2.6875	-.1258	-.2373	-.0535	-.0299	-.0075
76.64	.10	2.6946	-.1295	-.2289	-.0101	-.0007	.0019
76.65	-3.86	2.6877	-.1287	-.2401	.0186	.0258	.0102
76.64	-7.86	2.6522	-.1269	-.2520	.0547	.0448	.0186
76.62	-9.86	2.6361	-.1260	-.2494	.0697	.0512	.0215

RUN 87		Q=217.30 PSF		RN/FT= 4.917		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
71.68	-9.87	2.6656	-.1207	-.2025	.0596	.0549	.0219
71.67	-7.86	2.6717	-.1216	-.1931	.0464	.0479	.0180
71.67	-3.89	2.6890	-.1225	-.1720	.0167	.0303	.0099
71.66	.12	2.7068	-.1228	-.1666	-.0054	.0022	.0028
71.67	4.11	2.7106	-.1210	-.1681	-.0449	-.0286	-.0054
71.65	8.09	2.6760	-.1175	-.1848	-.0801	-.0547	-.0142
71.68	10.11	2.6855	-.1177	-.1923	-.1042	-.0642	-.0180
71.72	15.07	2.6207	-.1129	-.2368	-.1502	-.0839	-.0278
71.66	20.07	2.5498	-.1084	-.2826	-.2003	-.0954	-.0368
71.65	29.97	2.4410	-.1098	-.2646	-.2330	-.0975	-.0551

APPENDIX - Continued

RUN 88		Q=218.60 PSF	RN/FT= 4.931		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
66.87	29.97	2.5137	-.1125	-.1753	-.1995	-.0923	-.0537
66.84	20.06	2.5903	-.1047	-.1964	-.1621	-.0819	-.0354
66.86	15.06	2.6344	-.1066	-.1668	-.1109	-.0708	-.0259
66.89	10.09	2.6969	-.1104	-.1467	-.0678	-.0547	-.0155
66.95	8.12	2.7165	-.1114	-.1407	-.0652	-.0486	-.0117
66.93	4.09	2.7267	-.1142	-.1317	-.0300	-.0234	-.0046
66.93	.09	2.7220	-.1160	-.1338	-.0042	.0033	.0031
66.95	-3.89	2.7136	-.1159	-.1430	.0169	.0269	.0090
66.94	-7.87	2.6964	-.1146	-.1537	.0367	.0458	.0161
66.96	-9.88	2.6812	-.1144	-.1579	.0379	.0536	.0201

RUN 89		Q=220.10 PSF	RN/FT= 4.943		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
62.09	-9.87	2.6904	-.1131	-.0960	.0409	.0397	.0189
62.08	-7.89	2.7074	-.1141	-.0930	.0332	.0361	.0151
62.15	-3.90	2.7309	-.1166	-.0845	.0223	.0226	.0078
62.21	.12	2.7857	-.1309	-.0098	-.0023	-.0072	.0061
62.14	4.11	2.7298	-.1133	-.0825	-.0317	-.0242	-.0031
62.13	8.10	2.7294	-.1081	-.1042	-.0478	-.0451	-.0115
62.14	10.10	2.7099	-.1055	-.1159	-.0494	-.0525	-.0152
62.14	15.07	2.6842	-.1043	-.1174	-.1023	-.0638	-.0249
62.12	20.07	2.6405	-.1060	-.1213	-.1467	-.0707	-.0347
62.19	30.00	2.5578	-.1133	-.1261	-.2147	-.0879	-.0624

APPENDIX - Continued

RUN 90		Q=218.80 PSF		RN/FT= 4.924		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
52.58	30.07	2.7169	-.1323	.0010	-.2479	-.0827	-.1076
52.63	20.06	2.8649	-.1268	.0450	-.1103	-.0543	-.0549
52.66	15.07	2.9387	-.1341	.0790	-.0563	-.0487	-.0426
52.68	10.09	2.9776	-.1333	.0652	.0002	-.0269	-.0306
52.69	8.06	2.9539	-.1293	.0730	.0067	-.0146	-.0241
52.66	4.07	2.9329	-.1294	.0802	.0205	-.0066	-.0063
52.68	.08	2.9440	-.1372	.0757	.0043	.0054	.0023
52.66	-3.85	2.9366	-.1347	.0851	-.0092	.0060	.0152
52.68	-7.80	2.9567	-.1310	.0730	-.0329	.0249	.0216
52.72	-9.85	2.9611	-.1331	.0735	-.0405	.0314	.0285

RUN 91		Q=213.90 PSF		RN/FT= 4.866		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
42.45	-9.86	2.6633	-.1170	.1413	.0581	.0010	.0352
42.26	-7.83	2.6591	-.1130	.1269	.0264	-.0032	.0284
42.34	-3.78	2.6781	-.1066	.0867	-.0463	-.0198	.0197
41.93	.05	2.7639	-.1117	.0489	.0326	.0145	-.0012
42.28	4.04	2.6685	-.1033	.1021	.0139	.0211	-.0135
42.25	8.10	2.6762	-.1105	.1358	-.0468	.0044	-.0250
42.27	10.04	2.6544	-.1106	.1536	-.0676	.0045	-.0307
42.30	15.07	2.6644	-.1081	.1449	-.1510	-.0122	-.0517
42.24	20.12	2.6594	-.1012	.0800	-.2044	-.0432	-.0712
42.25	30.17	2.5622	-.0855	-.0880	-.3238	-.0977	-.1188

APPENDIX - Continued

RUN 92		Q=139.50 PSF	RN/FT= 3.321		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.21	.15	2.2506	.0471	-.3821	.0062	.0090	.0008
51.49	.15	2.4081	-.0623	-.3409	-.0044	-.0008	.0049
61.31	.16	2.4173	-.1419	-.3122	-.0150	-.0046	.0005
71.02	.14	2.5047	-.1787	-.4091	-.0032	.0037	.0015
81.00	.15	2.4866	-.2409	-.4390	-.0078	-.0014	.0021
91.49	.14	2.4303	-.2709	-.5083	-.0056	.0028	.0014

RUN 93		Q=151.50 PSF	RN/FT= 3.431		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
91.50	-9.79	2.4310	-.2717	-.5345	.0429	.0613	.0286
91.48	-7.80	2.4135	-.2706	-.5363	.0460	.0561	.0232
91.44	-3.82	2.4210	-.2690	-.5166	.0287	.0301	.0137
91.42	.13	2.4177	-.2695	-.5117	-.0048	.0019	.0021
91.42	4.09	2.4196	-.2663	-.5128	-.0496	-.0301	-.0093
91.41	8.04	2.4050	-.2672	-.5311	-.0619	-.0544	-.0209
91.40	10.08	2.4090	-.2675	-.5431	-.0831	-.0650	-.0263
91.40	15.00	2.3944	-.2626	-.5585	-.1169	-.0780	-.0372
91.37	19.94	2.3422	-.2418	-.5889	-.1581	-.1027	-.0477
91.37	29.83	2.2725	-.2419	-.5204	-.1463	-.0706	-.0700

APPENDIX - Continued

RUN 94		Q=145.30 PSF		RN/FT= 3.353		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
86.07	29.86	2.2957	-.2232	-.5264	-.1534	-.0861	-.0646
86.10	19.99	2.3542	-.2295	-.5783	-.2128	-.1249	-.0450
86.12	15.00	2.4127	-.2476	-.5260	-.1464	-.1046	-.0348
86.15	10.01	2.4408	-.2543	-.4822	-.0985	-.0683	-.0237
86.16	8.05	2.4619	-.2589	-.4691	-.0758	-.0582	-.0183
86.16	4.08	2.4612	-.2587	-.4588	-.0345	-.0324	-.0077
86.17	.08	2.4732	-.2591	-.4533	-.0112	.0002	.0022
86.17	-3.85	2.4596	-.2586	-.4581	.0178	.0314	.0127
86.19	-7.87	2.4371	-.2598	-.4708	.0507	.0617	.0215
86.20	-9.84	2.4412	-.2587	-.4806	.0625	.0763	.0270

RUN 95		Q=147.00 PSF		RN/FT= 3.365		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.91	-9.84	2.4426	-.2383	-.4580	.0610	.0749	.0252
80.92	-7.83	2.4717	-.2415	-.4482	.0579	.0605	.0206
80.89	-3.86	2.4907	-.2443	-.4376	.0122	.0306	.0115
80.88	.17	2.4801	-.2415	-.4387	-.0018	-.0021	.0011
80.88	4.15	2.4761	-.2391	-.4445	-.0478	-.0331	-.0077
80.86	8.06	2.4634	-.2339	-.4495	-.0659	-.0599	-.0184
80.86	10.10	2.4522	-.2313	-.4582	-.0902	-.0746	-.0216
80.84	15.02	2.4179	-.2223	-.5046	-.1583	-.1017	-.0320
80.81	20.06	2.3531	-.2095	-.5518	-.2219	-.1272	-.0426
80.78	29.92	2.3132	-.1921	-.5149	-.1596	-.0838	-.0610

APPENDIX - Continued

RUN	96	Q=143.10 PSF	RN/FT= 3.316	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
75.83	29.95	2.2872	-.1613	-.5066	-.1739	-.0890	-.0565
75.87	20.06	2.3520	-.1762	-.5597	-.2219	-.1245	-.0388
75.90	15.03	2.4154	-.1914	-.5020	-.1509	-.1026	-.0305
75.93	10.08	2.4566	-.2055	-.4544	-.0886	-.0709	-.0197
75.92	8.08	2.4682	-.2085	-.4441	-.0661	-.0594	-.0158
75.89	4.10	2.4859	-.2121	-.4404	-.0467	-.0345	-.0064
75.91	.10	2.5015	-.2153	-.4294	-.0061	-.0009	.0013
75.93	-3.87	2.4920	-.2170	-.4383	.0175	.0318	.0091
75.93	-7.77	2.4678	-.2154	-.4452	.0342	.0601	.0177
75.94	-9.86	2.4582	-.2130	-.4578	.0605	.0732	.0217

RUN	97	Q=144.60 PSF	RN/FT= 3.326	MACH=0.20			
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.91	-9.86	2.4608	-.1810	-.4472	.0486	.0734	.0188
70.91	-7.84	2.4698	-.1823	-.4329	.0253	.0615	.0144
70.89	-3.86	2.4829	-.1807	-.4106	.0102	.0345	.0074
70.89	.12	2.4843	-.1780	-.4058	-.0032	.0012	.0014
70.90	4.14	2.5010	-.1766	-.4140	-.0395	-.0353	-.0052
70.89	8.05	2.4780	-.1753	-.4304	-.0661	-.0607	-.0124
70.88	10.12	2.4589	-.1704	-.4391	-.0802	-.0712	-.0174
70.85	15.02	2.4106	-.1573	-.4791	-.1348	-.0967	-.0263
70.80	20.07	2.3355	-.1404	-.5388	-.2006	-.1150	-.0367
70.89	29.95	2.2534	-.1316	-.4804	-.2045	-.0933	-.0525

APPENDIX - Continued

RUN 98		Q=141.00 PSF		RN/FT= 3.278		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
66.06	29.96	2.2538	-.1081	-.4130	-.2489	-.0888	-.0528
66.06	20.02	2.3235	-.1138	-.4723	-.1681	-.0885	-.0330
66.12	15.11	2.3931	-.1230	-.4479	-.1342	-.0872	-.0243
66.16	10.07	2.4420	-.1399	-.4133	-.0744	-.0597	-.0142
66.17	8.08	2.4550	-.1445	-.4012	-.0619	-.0471	-.0110
66.17	4.09	2.4419	-.1592	-.3626	-.0367	-.0204	-.0045
66.17	.11	2.4506	-.1712	-.3472	-.0084	-.0019	.0008
66.18	-3.85	2.4598	-.1641	-.3632	.0151	.0187	.0068
66.17	-7.83	2.4533	-.1507	-.4112	.0319	.0506	.0133
66.18	-9.89	2.4297	-.1472	-.4179	.0381	.0650	.0170

RUN 99		Q=146.30 PSF		RN/FT= 3.331		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
61.27	-9.87	2.4125	-.1219	-.3695	.0229	.0449	.0157
61.26	-7.81	2.4137	-.1262	-.3579	.0130	.0326	.0117
61.26	-3.89	2.4361	-.1356	-.3403	-.0134	.0077	.0058
61.26	.15	2.4421	-.1455	-.3163	-.0175	-.0034	.0011
61.25	4.13	2.4351	-.1281	-.3338	-.0085	-.0096	-.0040
61.24	8.11	2.4175	-.1134	-.3569	-.0271	-.0265	-.0098
61.22	10.11	2.4145	-.1061	-.3707	-.0501	-.0404	-.0135
61.21	15.05	2.3955	-.1000	-.3727	-.0885	-.0474	-.0235
61.19	20.06	2.3308	-.0976	-.3492	-.1362	-.0535	-.0310
61.27	29.97	2.3389	-.1073	-.2930	-.2274	-.0865	-.0513

APPENDIX - Continued

RUN 100 Q=143.00 PSF RN/FT= 3.288 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
51.62	30.00	2.4899	-.0412	-.3513	-.2023	-.0848	-.0986
51.65	20.04	2.5883	-.0417	-.2971	-.0623	-.0552	-.0517
51.65	15.04	2.5682	-.0592	-.2731	-.0072	-.0396	-.0372
51.64	10.00	2.5399	-.0697	-.2899	.0291	-.0337	-.0190
51.61	8.09	2.4814	-.0681	-.3021	.0410	-.0270	-.0060
51.54	4.08	2.4023	-.0522	-.3485	.0568	-.0101	.0016
51.56	.11	2.4151	-.0648	-.3395	-.0031	.0014	.0030
51.58	-3.82	2.4277	-.0633	-.3510	-.0672	.0188	.0027
51.65	-7.83	2.5122	-.0707	-.3177	-.0714	.0267	.0212
51.70	-9.81	2.5641	-.0774	-.3015	-.0563	.0383	.0237

RUN 101 Q=144.00 PSF RN/FT= 3.292 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
41.33	-9.83	2.3294	.0294	-.3072	.0380	.0228	.0272
41.26	-7.76	2.2442	.0366	-.3217	.0713	-.0006	.0252
41.22	-3.86	2.2157	.0425	-.3626	.0773	-.0168	.0051
41.24	.13	2.2583	.0468	-.3804	.0045	.0090	.0017
41.18	4.11	2.2063	.0467	-.3614	-.0856	.0242	-.0090
41.21	8.09	2.2580	.0441	-.3157	-.0725	.0040	-.0226
41.27	10.12	2.3110	.0371	-.2931	-.0486	-.0123	-.0282
41.33	15.00	2.4398	.0296	-.3020	-.0154	-.0367	-.0354
41.33	20.06	2.4338	.0337	-.3254	-.0828	-.0532	-.0557
41.38	30.05	2.3931	.0337	-.3788	-.2994	-.0750	-.0997

APPENDIX - Continued

RUN 102		Q= 92.10 PSF	RN/FT= 2.211		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.00	.19	2.2142	.0496	-.4012	-.0196	.0069	-.0008
51.20	.19	2.3808	-.0612	-.3553	.0111	-.0081	.0081
60.99	.18	2.4074	-.1453	-.3107	-.0223	-.0047	.0003
70.72	.17	2.4942	-.1758	-.3776	-.0133	-.0022	.0015
80.58	.16	2.4748	-.2435	-.4285	-.0081	-.0018	.0014
90.00	.17	2.4079	-.2662	-.4792	-.0059	.0004	.0004

RUN 103		Q= 93.20 PSF	RN/FT= 2.210		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
90.02	-9.75	2.4051	-.2640	-.5192	.0611	.0742	.0270
90.02	-7.75	2.4125	-.2638	-.5103	.0586	.0579	.0221
90.00	-3.77	2.4145	-.2646	-.5018	.0168	.0295	.0126
90.00	.17	2.4327	-.2688	-.4842	-.0058	.0016	.0012
90.01	4.10	2.4334	-.2624	-.4801	-.0417	-.0283	-.0097
89.99	8.13	2.4064	-.2530	-.4880	-.0592	-.0548	-.0211
89.99	10.11	2.3978	-.2522	-.5030	-.0746	-.0678	-.0260
89.98	15.02	2.3713	-.2498	-.5447	-.1314	-.0985	-.0372
89.96	20.01	2.3438	-.2393	-.5627	-.1405	-.0951	-.0474
89.96	29.90	2.2392	-.2400	-.6220	-.2471	-.1448	-.0675

APPENDIX - Continued

RUN 104		Q= 92.40 PSF	RN/FT= 2.195		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
85.78	29.94	2.2301	-.2193	-.6670	-.3021	-.1736	-.0627
85.79	20.05	2.3430	-.2293	-.5600	-.1980	-.1220	-.0461
85.81	15.07	2.3986	-.2408	-.5119	-.1397	-.1086	-.0353
85.82	10.12	2.4302	-.2480	-.4807	-.0904	-.0746	-.0233
85.76	8.10	2.4522	-.2510	-.4623	-.0725	-.0577	-.0197
85.77	4.16	2.4604	-.2553	-.4439	-.0438	-.0285	-.0081
85.78	.16	2.4451	-.2574	-.4377	-.0012	-.0005	.0012
85.79	-3.82	2.4432	-.2575	-.4535	.0269	.0297	.0117
85.80	-7.81	2.4383	-.2579	-.4598	.0489	.0646	.0213
85.80	-9.76	2.4181	-.2550	-.4715	.0799	.0767	.0255

RUN 105		Q= 93.60 PSF	RN/FT= 2.202		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
80.67	-9.76	2.4324	-.2306	-.4595	.0693	.0812	.0235
80.66	-7.77	2.4580	-.2352	-.4472	.0482	.0644	.0201
80.65	-3.79	2.4749	-.2395	-.4260	.0159	.0323	.0109
80.63	.15	2.4602	-.2410	-.4290	-.0065	.0006	.0007
80.62	4.13	2.4690	-.2397	-.4263	-.0294	-.0314	-.0089
80.62	8.10	2.4559	-.2316	-.4459	-.0727	-.0604	-.0172
80.61	10.14	2.4375	-.2288	-.4633	-.0984	-.0783	-.0223
80.59	15.06	2.4022	-.2191	-.5126	-.1614	-.1090	-.0324
80.57	20.06	2.3513	-.2069	-.5608	-.2103	-.1290	-.0420
80.56	29.96	2.2446	-.1899	-.6546	-.3162	-.1751	-.0583

APPENDIX - Continued

RUN 106		Q= 92.20 PSF		RN/FT= 2.181		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
75.53	29.99	2.2165	-.1516	-.6476	-.3245	-.1790	-.0549
75.54	20.09	2.3330	-.1754	-.5481	-.1999	-.1148	-.0394
75.58	15.06	2.4040	-.1876	-.5013	-.1629	-.1094	-.0298
75.59	10.14	2.4439	-.2010	-.4606	-.0934	-.0800	-.0190
75.59	8.15	2.4627	-.2052	-.4527	-.0684	-.0633	-.0148
75.61	4.15	2.4799	-.2084	-.4314	-.0389	-.0344	-.0070
75.62	.18	2.4658	-.2091	-.4213	-.0051	-.0013	.0011
75.63	-3.80	2.4745	-.2128	-.4292	.0149	.0307	.0091
75.65	-7.77	2.4658	-.2100	-.4514	.0557	.0678	.0164
75.64	-9.76	2.4469	-.2078	-.4639	.0736	.0857	.0201

RUN 107		Q= 93.50 PSF		RN/FT= 2.190		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.67	-9.79	2.4501	-.1771	-.4217	.0607	.0855	.0160
70.66	-7.80	2.4648	-.1772	-.4104	.0389	.0699	.0126
70.66	-3.78	2.4894	-.1780	-.3917	.0133	.0337	.0066
70.66	.19	2.4798	-.1744	-.3791	-.0066	.0012	.0005
70.65	4.16	2.4907	-.1743	-.3881	-.0353	-.0351	-.0058
70.64	8.13	2.4705	-.1723	-.4167	-.0627	-.0663	-.0123
70.64	10.11	2.4481	-.1673	-.4225	-.0840	-.0809	-.0169
70.62	15.11	2.3979	-.1559	-.4466	-.1352	-.1000	-.0267
70.58	20.04	2.3284	-.1399	-.5045	-.1831	-.1062	-.0364
70.56	30.02	2.2038	-.1162	-.6042	-.3286	-.1567	-.0551

APPENDIX - Continued

RUN 108		Q= 92.40 PSF		RN/FT= 2.172		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.76	30.02	2.2468	-.1019	-.4168	-.2593	-.0980	-.0528
65.78	20.07	2.3277	-.1169	-.4392	-.1471	-.0817	-.0326
65.82	15.09	2.3937	-.1210	-.4239	-.1332	-.0917	-.0236
65.84	10.17	2.4387	-.1311	-.4035	-.0751	-.0722	-.0133
65.84	8.17	2.4464	-.1330	-.4002	-.0584	-.0572	-.0104
65.86	4.15	2.4768	-.1295	-.3947	-.0382	-.0324	-.0043
65.86	.15	2.4486	-.1339	-.3823	-.0228	-.0068	.0004
65.87	-3.78	2.4596	-.1293	-.3916	-.0118	.0221	.0060
65.90	-7.77	2.4708	-.1338	-.4128	.0182	.0627	.0115
65.90	-9.77	2.4372	-.1325	-.4099	.0401	.0798	.0139

RUN 109		Q= 92.90 PSF		RN/FT= 2.171		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.98	-9.79	2.4118	-.1102	-.3800	.0527	.0693	.0139
60.97	-7.78	2.4136	-.1180	-.3572	.0316	.0493	.0107
60.96	-3.81	2.4219	-.1313	-.3383	-.0161	.0082	.0050
60.96	.19	2.4225	-.1465	-.3118	-.0115	-.0045	.0004
60.95	4.13	2.4243	-.1273	-.3341	-.0099	-.0101	-.0040
60.94	8.12	2.4151	-.1169	-.3450	-.0482	-.0424	-.0091
60.93	10.12	2.4083	-.1111	-.3553	-.0721	-.0577	-.0127
60.92	15.12	2.3819	-.0995	-.3795	-.1165	-.0672	-.0228
60.88	20.04	2.3048	-.0857	-.3799	-.1430	-.0601	-.0302
60.92	30.00	2.2953	-.0988	-.3112	-.2814	-.0970	-.0597

APPENDIX - Continued

RUN 110		Q= 91.40 PSF		RN/FT= 2.148		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
51.29	30.01	2.4933	-.0331	-.3347	-.1826	-.0887	-.1080
51.29	20.02	2.5240	-.0384	-.2743	-.0120	-.0357	-.0535
51.29	15.07	2.4938	-.0432	-.2752	.0372	-.0277	-.0391
51.28	10.10	2.4390	-.0403	-.3044	.0437	-.0221	-.0269
51.26	8.13	2.4317	-.0431	-.3178	.0485	-.0287	-.0175
51.25	4.17	2.3718	-.0468	-.3494	.0520	-.0158	-.0004
51.26	.17	2.3707	-.0619	-.3550	.0108	-.0094	.0096
51.26	-3.78	2.3753	-.0534	-.3611	-.0713	.0170	.0028
51.32	-7.73	2.4710	-.0434	-.3263	-.0596	.0250	.0240
51.34	-9.75	2.4665	-.0450	-.3141	-.0430	.0259	.0329

RUN 111		Q= 92.00 PSF		RN/FT= 2.150		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.06	-9.77	2.2957	.0407	-.3592	.0180	.0330	.0201
41.02	-7.79	2.2430	.0460	-.3565	.0530	.0155	.0226
40.97	-3.80	2.1695	.0503	-.3860	.0831	-.0118	.0093
40.97	.17	2.2123	.0537	-.4045	-.0255	.0090	-.0018
40.96	4.16	2.1921	.0523	-.3888	-.0826	.0097	-.0098
40.99	8.17	2.2454	.0510	-.3647	-.0404	-.0179	-.0177
41.00	10.11	2.2752	.0477	-.3643	-.0048	-.0240	-.0180
41.05	15.07	2.4023	.0410	-.3559	.0114	-.0409	-.0322
41.06	20.09	2.4298	.0487	-.3982	-.0423	-.0554	-.0558
41.13	30.04	2.3677	.0383	-.3930	-.2650	-.0641	-.0983

APPENDIX - Continued

RUN 112 Q= 54.90 PSF RN/FT= 1.325 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.77	.21	2.1772	.0536	-.3932	-.0198	.0072	.0005
51.00	.19	2.3835	-.0554	-.3351	.0016	-.0020	.0015
60.74	.18	2.4023	-.1272	-.2983	.0049	.0034	.0018
65.53	.20	2.4467	-.1138	-.3805	-.0082	-.0019	.0010
70.40	.19	2.4607	-.1579	-.3693	-.0098	-.0017	.0015
75.31	.18	2.4653	-.2021	-.4118	.0061	.0035	.0008
80.31	.18	2.4370	-.2213	-.3966	.0234	.0087	-.0001
85.50	.21	2.4299	-.2321	-.3988	-.0359	-.0291	.0020
90.83	.19	2.4273	-.2490	-.3880	-.0259	-.0129	.0025

RUN 113 Q= 57.40 PSF RN/FT= 1.338 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.83	-9.74	2.2436	.0515	-.3638	.0071	.0237	.0202
40.84	-7.76	2.2207	.0531	-.3615	.0237	.0162	.0163
40.80	-3.78	2.1747	.0546	-.3771	.0572	-.0003	.0070
40.78	.20	2.1850	.0543	-.3977	-.0232	.0079	-.0004
40.76	4.15	2.1642	.0549	-.3788	-.0580	.0081	-.0062
40.78	8.14	2.2071	.0551	-.3659	-.0099	-.0121	-.0159
40.79	10.12	2.2548	.0527	-.3678	.0010	-.0236	-.0168
40.82	15.10	2.3543	.0532	-.3656	.0593	-.0337	-.0409
40.82	20.04	2.3626	.0516	-.3543	.0184	-.0369	-.0572
40.79	29.98	2.2904	.0460	-.3515	-.2214	-.0527	-.1021

APPENDIX - Continued

RUN 114		Q= 13.00 PSF	RN/FT= .318		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.54	.18	2.2803	.0418	-.3235	.0291	.0069	.0003
50.71	.17	2.4986	-.0652	-.1840	.0355	.0066	.0035
60.46	.17	2.6212	-.1533	-.0159	.0127	-.0078	.0010
80.00	.18	2.5279	-.2323	-.0386	.0090	.0082	.0009
90.50	.18	2.4283	-.2625	-.2589	-.0052	.0018	0.0000
70.06	.19	2.5251	-.1968	-.0099	.0115	.0262	-.0030
70.09	.18	2.5354	-.1954	-.0154	.0086	.0202	-.0013

RUN 115		Q= 14.50 PSF	RN/FT= .348		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
90.57	-9.75	2.3960	-.2512	-.3037	-.0312	.0042	.0283
90.58	-7.73	2.3941	-.2549	-.2971	-.0323	.0039	.0234
90.57	-3.80	2.4126	-.2587	-.2695	.0038	.0092	.0124
90.56	.20	2.4282	-.2608	-.2610	.0032	.0018	-.0001
90.55	4.15	2.4289	-.2568	-.2732	.0066	-.0048	-.0120
90.53	8.11	2.4115	-.2491	-.3053	.0246	.0007	-.0242
90.53	10.10	2.3976	-.2465	-.3071	.0247	.0024	-.0297
90.52	15.04	2.3894	-.2332	-.3126	.0078	-.0165	-.0408
90.52	19.98	2.3578	-.2155	-.3333	-.0542	-.0463	-.0519
90.50	29.89	2.2342	-.1959	-.3599	-.1429	-.0785	-.0714

APPENDIX - Continued

RUN 116		Q= 14.60 PSF		RN/FT= .349		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.18	29.89	2.2742	-.1878	-.3205	-.1586	-.0956	-.0661
85.21	20.02	2.3951	-.2082	-.2831	-.0500	-.0597	-.0496
85.22	15.07	2.4142	-.2247	-.2490	.0144	-.0211	-.0391
85.21	10.13	2.4356	-.2352	-.2516	.0319	.0057	-.0270
85.21	8.10	2.4363	-.2389	-.2381	.0571	.0107	-.0227
85.23	4.14	2.4741	-.2425	-.2147	.0290	.0058	-.0119
85.24	.16	2.4968	-.2482	-.1919	.0117	.0024	.0002
85.25	-3.80	2.4811	-.2456	-.2295	-.0078	-.0035	.0109
85.27	-7.76	2.4331	-.2439	-.2633	-.0196	-.0066	.0223
85.27	-9.76	2.4204	-.2435	-.2639	-.0171	-.0009	.0265

RUN 117		Q= 14.70 PSF		RN/FT= .352		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.05	-9.76	2.4792	-.2286	-.1589	.0094	.0154	.0246
80.05	-7.77	2.4782	-.2272	-.1515	-.0116	.0006	.0186
80.04	-3.80	2.5128	-.2311	-.1234	-.0192	-.0052	.0096
80.02	.15	2.5380	-.2356	-.0580	.0202	.0106	.0003
80.01	4.12	2.5138	-.2304	-.1178	.0444	.0173	-.0102
80.00	8.13	2.4955	-.2271	-.1390	.0475	.0108	-.0199
79.99	10.09	2.4904	-.2249	-.1533	.0217	-.0024	-.0246
79.98	15.07	2.4745	-.2161	-.1791	-.0105	-.0326	-.0358
79.97	19.99	2.4231	-.1993	-.2251	-.0696	-.0573	-.0459
79.95	29.92	2.2950	-.1773	-.2764	-.1858	-.1015	-.0619

APPENDIX - Continued

RUN 118		Q= 15.00 PSF		RN/FT= .356		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
75.00	29.93	2.2916	-.1630	-.2135	-.2234	-.1174	-.0571
75.02	20.02	2.4375	-.1765	-.1737	-.1032	-.0768	-.0403
75.04	15.07	2.4940	-.1923	-.1259	-.0331	-.0473	-.0311
75.03	10.09	2.5117	-.2094	-.1136	.0320	-.0061	-.0215
75.03	8.10	2.5165	-.2121	-.1053	.0276	.0064	-.0188
75.05	4.16	2.5295	-.2174	-.0683	.0282	.0140	-.0088
75.06	.17	2.5456	-.2231	-.0180	.0094	.0138	-.0001
75.07	-3.80	2.5450	-.2232	-.0428	-.0266	-.0065	.0089
75.08	-7.77	2.5088	-.2180	-.1027	-.0424	.0013	.0167
75.09	-9.76	2.4939	-.2173	-.1165	-.0030	.0243	.0199

RUN 119		Q= 14.50 PSF		RN/FT= .351		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
70.07	-9.75	2.4972	-.1774	-.0956	-.0502	.0117	.0189
70.06	-7.73	2.5104	-.1823	-.0891	-.0660	0.0000	.0156
70.07	-3.77	2.5481	-.1930	-.0471	-.0631	-.0231	.0093
70.06	.17	2.5350	-.2029	-.0296	-.0006	.0101	-.0008
70.04	4.14	2.5368	-.1859	-.0839	.0435	.0221	-.0098
70.09	8.11	2.5226	-.1751	-.1003	.0364	.0044	-.0173
70.09	10.10	2.5308	-.1714	-.1091	.0333	-.0062	-.0211
70.08	15.05	2.4867	-.1582	-.1208	-.0243	-.0439	-.0284
70.08	20.02	2.4470	-.1536	-.1601	-.1563	-.0967	-.0365
70.06	29.95	2.3147	-.1391	-.1162	-.2750	-.1168	-.0598

APPENDIX - Continued

RUN 120		Q= 15.00 PSF		RN/FT= .358		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.26	29.93	2.3537	-.1211	.0092	-.2826	-.1039	-.0579
65.27	20.05	2.4292	-.1406	-.0496	-.1291	-.0776	-.0326
65.29	15.05	2.4891	-.1430	-.0654	-.0327	-.0292	-.0270
65.30	10.11	2.5385	-.1393	-.0927	.0388	-.0018	-.0192
65.30	8.13	2.5349	-.1415	-.1066	.0747	.0129	-.0160
65.30	4.11	2.5255	-.1469	-.1237	.0944	.0428	-.0104
65.34	.16	2.5844	-.1900	.0168	-.0425	-.0283	.0030
65.32	-3.80	2.5698	-.1669	-.0360	-.0550	-.0394	.0115
65.33	-7.77	2.5509	-.1428	-.0870	-.0372	-.0100	.0164
65.33	-9.76	2.5366	-.1420	-.0877	-.0240	.0055	.0189

RUN 121		Q= 14.40 PSF		RN/FT= .352		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.47	-9.75	2.6382	-.1725	.1144	-.0583	-.0176	.0198
60.46	-7.76	2.5958	-.1698	.0930	-.0494	-.0331	.0195
60.43	-3.78	2.5706	-.1497	-.0377	-.0509	-.0366	.0154
60.43	.18	2.5756	-.1620	-.0252	-.0562	-.0358	.0049
60.41	4.14	2.5427	-.1486	-.0228	.0848	.0742	-.0125
60.45	8.08	2.5537	-.1548	.0864	.0936	.0672	-.0208
60.44	10.12	2.5188	-.1317	.0377	.0769	.0382	-.0195
60.45	15.06	2.5390	-.1422	.0857	-.0028	-.0055	-.0252
60.47	20.00	2.6115	-.1516	.1809	-.0022	-.0139	-.0364
60.44	29.91	2.4432	-.1037	.0623	-.2940	-.1048	-.0765

APPENDIX - Continued

RUN 122		Q= 15.00 PSF		RN/FT= .360		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
50.73	29.88	2.3823	-.0485	.3674	-.0690	.0150	-.0749
50.73	20.03	2.5005	-.0754	.2354	.0090	.0365	-.0559
50.74	15.05	2.4936	-.0765	.2218	.0176	.0570	-.0448
50.74	10.11	2.4852	-.0761	.1271	.0799	.0814	-.0414
50.73	8.11	2.4786	-.0768	.0540	.1023	.0856	-.0357
50.73	4.12	2.4575	-.0774	-.0754	.1165	.0906	-.0175
50.74	.16	2.4364	-.0939	-.1903	.0363	.0044	.0044
50.76	-3.78	2.4715	-.0830	-.1437	-.0576	-.0158	.0166
50.78	-7.76	2.5185	-.0823	-.0491	-.0584	-.0043	.0249
50.80	-9.72	2.5519	-.0745	.0149	-.0951	-.0263	.0329

RUN 123		Q= 14.00 PSF		RN/FT= .349		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.55	-9.72	2.2584	.0144	-.2240	.1288	.0383	.0175
40.53	-7.76	2.2418	.0187	-.2611	.0921	.0294	.0103
40.51	-3.81	2.2150	.0209	-.3213	.0247	.0070	.0027
40.50	.18	2.2147	.0206	-.3278	.0225	.0067	-.0003
40.48	4.13	2.2071	.0299	-.2738	.1126	.0206	-.0160
40.48	8.11	2.2274	.0418	-.1529	.1080	.0365	-.0251
40.47	10.09	2.2101	.0424	-.1029	.0848	.0381	-.0237
40.48	15.03	2.1784	.0300	-.0183	-.0107	.0420	-.0332
40.52	20.01	2.1932	.0400	.0676	-.0284	.0394	-.0455
40.50	29.94	2.0870	.0450	.1369	-.2026	-.0037	-.0823

APPENDIX - Continued

RUN 124 Q= 14.30 PSF RN/FT= .354 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.56	.16	2.2034	.0174	-.3306	.0309	.0066	-.0007
50.68	.17	2.4267	-.0888	-.2014	.0318	.0068	.0043
60.43	.17	2.5490	-.1614	-.0343	-.0461	-.0426	.0059
70.13	.17	2.5431	-.1998	-.0422	.0114	.0152	-.0003
80.06	.16	2.5183	-.2385	-.0542	.0155	.0080	.0005
90.58	.17	2.4293	-.2640	-.2721	.0023	-.0003	.0004

RUN 125 Q= 14.70 PSF RN/FT= .348 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
90.56	.17	2.5037	-.2257	-.1767	-.0027	.0020	.0007
80.03	.17	2.6060	-.2206	.0542	.0031	.0059	-.0002
70.09	.16	2.6887	-.2311	.1476	.0237	.0251	-.0023
60.54	.19	2.8060	-.2515	.1873	-.0463	-.0350	-.0008
50.78	.16	2.6959	-.2125	.0270	.0497	.0103	-.0008
40.59	.17	2.3942	-.1051	-.1564	.0228	.0048	-.0015

APPENDIX - Continued

RUN 126		Q= 14.10 PSF		RN/FT= .341		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.61	-9.75	2.3335	-.1027	-.0504	.1514	.0294	.0246
40.60	-7.77	2.3463	-.1027	-.0731	.1073	.0220	.0193
40.59	-3.79	2.3688	-.1024	-.1299	-.0207	.0039	.0205
40.58	.16	2.4133	-.1007	-.1566	.0251	.0051	-.0024
40.57	4.10	2.3866	-.0949	-.0897	.1309	.0248	-.0264
40.57	8.11	2.3988	-.0954	.0100	.1301	.0359	-.0288
40.57	10.06	2.4178	-.0887	.0615	.1245	.0389	-.0323
40.57	15.04	2.3391	-.0860	.1215	.0037	.0377	-.0391
40.56	20.01	2.3304	-.0738	.1913	-.0259	.0371	-.0499
40.54	29.88	2.2282	-.0474	.2986	-.1427	.0188	-.0822

RUN 127		Q= 15.00 PSF		RN/FT= .354		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
50.76	29.88	2.5476	-.1429	.4599	-.0963	.0041	-.0965
50.78	20.02	2.6064	-.1913	.4210	-.0474	.0338	-.0576
50.80	15.05	2.6618	-.2084	.4589	-.0066	.0552	-.0478
50.81	10.08	2.7125	-.2071	.3906	.1079	.0830	-.0381
50.82	8.09	2.7080	-.2035	.3342	.1385	.0793	-.0292
50.83	4.09	2.7063	-.2074	.1980	.1755	.0753	-.0068
50.83	.21	2.7228	-.2147	.0211	.0536	.0093	-.0002
50.85	-3.80	2.7355	-.2074	.0749	-.0122	-.0198	.0237
50.86	-7.80	2.7257	-.2057	.1692	.0202	-.0173	.0363
50.88	-9.72	2.7497	-.2037	.2394	-.0292	-.0435	.0383

APPENDIX - Continued

RUN 128		Q= 15.50 PSF		RN/FT= .361		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.54	-9.69	2.7457	-.2300	.2785	-.0037	-.0319	.0320
60.54	-7.75	2.7720	-.2348	.2574	-.0265	-.0368	.0297
60.53	-3.82	2.7649	-.2352	.1854	-.0552	-.0396	.0197
60.52	.18	2.7940	-.2443	.1781	-.0258	-.0405	-.0019
60.51	4.11	2.7682	-.2375	.2266	.0955	.0898	-.0134
60.50	8.10	2.7508	-.2323	.3320	.0981	.0777	-.0245
60.50	10.10	2.7328	-.2256	.2885	.0670	.0447	-.0273
60.50	15.06	2.7298	-.2191	.2926	-.0085	.0015	-.0352
60.49	19.99	2.7176	-.2126	.2901	-.0508	-.0247	-.0509
60.44	29.89	2.5492	-.1706	.2137	-.2551	-.1080	-.0956

RUN 129		Q= 15.30 PSF		RN/FT= .359		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.31	29.89	2.5593	-.1973	.1933	-.1971	-.1137	-.0713
65.31	20.03	2.6557	-.2175	.1482	-.1570	-.0891	-.0417
65.32	15.07	2.6792	-.2227	.1654	-.0647	-.0375	-.0317
65.32	10.14	2.6874	-.2154	.1425	.0341	.0162	-.0235
65.32	8.12	2.6472	-.2099	.1024	.0545	.0309	-.0194
65.33	4.18	2.6463	-.2201	.0996	.0952	.0614	-.0124
65.37	.13	2.7617	-.2441	.1993	-.0426	-.0283	.0024
65.34	-3.79	2.7102	-.2314	.1690	-.0500	-.0349	.0115
65.34	-7.75	2.6698	-.2206	.1675	-.0382	-.0277	.0205
65.34	-9.75	2.6781	-.2212	.1827	-.0128	-.0119	.0234

APPENDIX - Continued

RUN 130		Q= 15.50 PSF		RN/FT= .362		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.12	-9.76	2.6404	-.2145	.0965	-.0331	.0003	.0212
70.12	-7.77	2.6294	-.2112	.0961	-.0378	-.0143	.0177
70.10	-3.80	2.6540	-.2254	.1291	-.0508	-.0297	.0108
70.09	.22	2.6838	-.2329	.1518	.0224	.0189	-.0016
70.07	4.18	2.6480	-.2184	.0774	.0427	.0305	-.0111
70.05	8.10	2.5986	-.2099	.0754	.0397	.0159	-.0181
70.06	10.14	2.6207	-.2124	.0803	.0047	.0031	-.0222
70.11	15.03	2.6101	-.2139	.0950	-.0660	-.0386	-.0313
70.11	20.04	2.5423	-.2076	.0310	-.1870	-.1098	-.0398
70.07	29.92	2.3984	-.1892	.0412	-.2981	-.1177	-.0754

RUN 131		Q= 14.10 PSF		RN/FT= .346		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
74.99	29.91	2.3485	-.1874	-.0953	-.2483	-.1334	-.0620
75.02	20.02	2.5102	-.2050	-.0179	-.1503	-.0860	-.0414
75.03	15.06	2.5615	-.2137	.0151	-.0688	-.0446	-.0317
75.04	10.06	2.5951	-.2199	.0421	-.0011	-.0008	-.0225
75.03	8.14	2.5926	-.2182	.0420	.0352	.0124	-.0185
75.05	4.15	2.6291	-.2216	.0706	.0322	.0170	-.0091
75.07	.17	2.6449	-.2277	.1096	.0264	.0149	-.0014
75.08	-3.80	2.6445	-.2262	.0909	-.0075	-.0099	.0080
75.10	-7.78	2.6134	-.2239	.0443	-.0108	-.0001	.0169
75.10	-9.77	2.6057	-.2233	.0336	.0254	.0192	.0207

APPENDIX - Continued

RUN 132 Q= 14.40 PSF RN/FT= .351 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.04	-9.77	2.5454	-.2173	-.0609	-.0110	.0015	.0230
80.06	-7.71	2.5640	-.2191	-.0575	-.0176	-.0054	.0185
80.04	-3.76	2.5643	-.2154	-.0180	-.0095	-.0111	.0095
80.03	.21	2.6045	-.2185	.0549	.0032	.0059	-.0002
80.02	4.18	2.5802	-.2154	-.0197	.0436	.0243	-.0101
80.01	8.10	2.5676	-.2170	-.0449	.0423	.0161	-.0193
80.00	10.14	2.5690	-.2146	-.0508	.0127	.0065	-.0241
80.00	15.01	2.5237	-.2020	-.0770	-.0136	-.0193	-.0344
79.99	20.04	2.4849	-.1932	-.0875	-.0949	-.0519	-.0432
79.96	29.94	2.3514	-.1714	-.1786	-.1939	-.1068	-.0631

RUN 133 Q= 14.50 PSF RN/FT= .353 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.18	29.94	2.2878	-.1661	-.2501	-.1982	-.0956	-.0649
85.20	20.02	2.4473	-.1901	-.1910	-.0815	-.0513	-.0445
85.21	15.05	2.4978	-.2015	-.1810	-.0132	-.0193	-.0359
85.21	10.07	2.5357	-.2127	-.1763	.0297	.0064	-.0255
85.22	8.06	2.5340	-.2169	-.1704	.0425	.0118	-.0205
85.23	4.14	2.5668	-.2205	-.1359	.0122	-.0055	-.0091
85.23	.16	2.5593	-.2234	-.1268	.0186	-.0004	.0012
85.25	-3.80	2.5653	-.2221	-.1497	-.0039	.0037	.0109
85.26	-7.77	2.5310	-.2185	-.1774	-.0085	-.0071	.0222
85.26	-9.73	2.5195	-.2195	-.1715	-.0178	-.0023	.0255

APPENDIX - Continued

RUN 134		Q= 14.60 PSF		RN/FT= .356		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
90.53	-9.73	2.4834	-.2168	-.2507	.0137	.0106	.0274
90.54	-7.71	2.4974	-.2204	-.2190	.0086	.0120	.0219
90.53	-3.80	2.4824	-.2234	-.1995	.0064	.0094	.0126
90.52	.18	2.4890	-.2255	-.1903	.0016	.0031	.0010
90.50	4.17	2.4977	-.2217	-.1865	.0006	-.0052	-.0112
90.49	8.10	2.4843	-.2157	-.2180	.0001	-.0079	-.0228
90.48	10.12	2.4721	-.2119	-.2423	-.0081	-.0069	-.0279
90.48	15.10	2.4359	-.2028	-.2464	-.0474	-.0279	-.0380
90.47	20.00	2.3777	-.1891	-.2660	-.1111	-.0503	-.0487
90.44	29.91	2.2164	-.1633	-.3083	-.2165	-.0746	-.0689

RUN 135		Q= 14.60 PSF		RN/FT= .349		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.65	.21	2.6296	-.1184	.0648	.0464	.0126	-.0002
50.83	.20	2.9196	-.1605	.1564	.0286	.0067	.0123
60.52	.19	2.9035	-.1691	.2593	-.0217	-.0270	-.0052
70.13	.19	2.7810	-.1554	.1866	.0283	.0278	-.0026
80.05	.19	2.6842	-.1496	.0506	-.0027	.0025	-.0002
90.62	.19	2.5691	-.1458	-.1698	-.0169	.0035	.0028

APPENDIX - Continued

RUN 136		Q= 14.80 PSF	RN/FT= .352		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
90.52	-9.73	2.5412	-.1416	-.2138	.0286	.0143	.0275
90.53	-7.76	2.5542	-.1414	-.2002	.0308	.0176	.0230
90.52	-3.82	2.5605	-.1437	-.1725	.0082	.0148	.0141
90.50	.20	2.5414	-.1452	-.1551	.0000	.0022	.0015
90.50	4.13	2.5821	-.1417	-.1739	.0029	-.0082	-.0112
90.49	8.10	2.5498	-.1352	-.1945	-.0021	-.0119	-.0222
90.51	10.08	2.5554	-.1332	-.2224	-.0019	-.0142	-.0288
90.51	15.02	2.5129	-.1253	-.2236	-.0562	-.0296	-.0375
90.52	20.02	2.4629	-.1165	-.2465	-.1098	-.0476	-.0478
90.48	29.95	2.2933	-.0998	-.2768	-.1891	-.0669	-.0669

RUN 137		Q= 15.00 PSF	RN/FT= .356		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
85.19	29.94	2.3532	-.1095	-.1702	-.1612	-.0771	-.0627
85.21	19.98	2.5047	-.1225	-.1719	-.0839	-.0493	-.0443
85.22	15.05	2.5550	-.1302	-.1547	-.0231	-.0228	-.0348
85.21	10.06	2.5841	-.1377	-.1411	.0069	-.0015	-.0247
85.22	8.11	2.6022	-.1394	-.1391	.0164	.0056	-.0199
85.22	4.17	2.6225	-.1413	-.1043	.0107	-.0088	-.0100
85.24	.15	2.6142	-.1451	-.1019	.0124	.0019	.0024
85.25	-3.76	2.6199	-.1438	-.1241	.0145	.0051	.0120
85.26	-7.77	2.6141	-.1428	-.1523	-.0083	.0010	.0223
85.25	-9.77	2.5961	-.1420	-.1483	.0177	.0072	.0255

APPENDIX - Continued

RUN 138 Q= 14.90 PSF RN/FT= .355 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.01	-9.75	2.6163	-.1447	-.0379	-.0055	-.0047	.0238
80.02	-7.72	2.6227	-.1455	-.0283	-.0173	-.0115	.0200
80.00	-3.80	2.6485	-.1456	-.0219	-.0284	-.0154	.0107
79.99	.15	2.6457	-.1493	.0479	-.0064	.0036	.0002
79.98	4.16	2.6363	-.1467	-.0048	.0411	.0234	-.0099
79.96	8.15	2.6126	-.1426	-.0231	.0358	.0200	-.0199
79.95	10.09	2.5937	-.1397	-.0375	.0154	.0128	-.0240
79.94	15.08	2.5403	-.1346	-.0417	-.0294	-.0136	-.0332
79.93	20.08	2.4791	-.1282	-.0678	-.1052	-.0435	-.0414
79.91	29.93	2.3921	-.1154	-.1029	-.1870	-.0878	-.0604

RUN 139 Q= 14.50 PSF RN/FT= .352 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
74.97	29.93	2.4102	-.1198	-.0368	-.2248	-.1154	-.0568
75.00	20.08	2.5487	-.1347	.0198	-.1392	-.0682	-.0398
74.99	15.07	2.5965	-.1416	.0464	-.0618	-.0339	-.0310
75.00	10.08	2.6524	-.1526	.0824	-.0069	-.0005	-.0213
75.00	8.13	2.6289	-.1531	.0853	.0327	.0127	-.0172
75.01	4.17	2.6790	-.1572	.1201	.0302	.0193	-.0086
75.02	.17	2.6805	-.1613	.1589	.0121	.0114	-.0010
75.04	-3.77	2.6794	-.1597	.1406	-.0126	-.0109	.0073
75.05	-7.75	2.6629	-.1561	.0814	-.0074	.0023	.0170
75.05	-9.77	2.6471	-.1537	.0551	.0240	.0188	.0204

APPENDIX - Continued

RUN 140 Q= 14.20 PSF RN/FT= .349 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.11	-9.76	2.6959	-.1511	.1453	-.0088	.0037	.0213
70.11	-7.72	2.7092	-.1494	.1537	-.0141	-.0129	.0179
70.11	-3.82	2.7394	-.1527	.1799	-.0218	-.0268	.0104
70.10	.23	2.7768	-.1578	.1955	.0301	.0245	-.0020
70.09	4.17	2.7516	-.1491	.1446	.0353	.0308	-.0098
70.08	8.16	2.7173	-.1423	.1360	.0207	.0121	-.0174
70.08	10.08	2.7118	-.1426	.1341	-.0045	-.0096	-.0196
70.07	15.04	2.6671	-.1381	.1180	-.0707	-.0541	-.0272
70.07	20.06	2.5831	-.1307	.0653	-.1695	-.1053	-.0345
70.04	29.92	2.5031	-.1177	.0200	-.2265	-.1276	-.0557

RUN 141 Q= 14.50 PSF RN/FT= .354 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.26	29.91	2.5611	-.1218	.1845	-.2084	-.1018	-.0569
65.28	20.03	2.6542	-.1350	.1773	-.1560	-.0957	-.0335
65.27	15.05	2.6871	-.1396	.1656	-.0738	-.0532	-.0261
65.28	10.06	2.7220	-.1426	.1953	.0337	.0114	-.0199
65.28	8.13	2.7352	-.1432	.1703	.0565	.0286	-.0172
65.29	4.12	2.7146	-.1467	.1438	.0871	.0577	-.0123
65.33	.13	2.8024	-.1665	.2713	-.0120	-.0279	.0024
65.34	-3.71	2.7818	-.1521	.2144	-.0368	-.0370	.0119
65.34	-7.76	2.7742	-.1458	.2046	-.0169	-.0243	.0188
65.35	-9.72	2.7446	-.1453	.2080	.0109	-.0070	.0213

APPENDIX - Continued

RUN 142		Q= 14.20 PSF		RN/FT= .352		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.51	-9.69	2.8413	-.1560	.3275	-.0040	-.0273	.0248
60.50	-7.77	2.8555	-.1576	.3099	-.0181	-.0369	.0234
60.49	-3.81	2.8502	-.1580	.2557	-.0546	-.0352	.0160
60.50	.18	2.8943	-.1659	.2513	-.0147	-.0298	-.0044
60.48	4.13	2.8114	-.1555	.2613	.0929	.0920	-.0106
60.46	8.10	2.7883	-.1479	.3235	.0749	.0796	-.0201
60.45	10.06	2.7558	-.1428	.2830	.0357	.0323	-.0195
60.42	15.06	2.7611	-.1433	.3349	-.0206	.0020	-.0284
60.51	20.04	2.7470	-.1418	.3420	-.0806	-.0252	-.0415
60.42	29.89	2.5878	-.1165	.2719	-.2537	-.0900	-.0835

RUN 143		Q= 14.00 PSF		RN/FT= .350		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
50.78	29.91	2.6818	-.1495	.6513	-.1037	.0149	-.0970
50.79	19.99	2.7691	-.1607	.5841	.0174	.0535	-.0620
50.79	15.06	2.8001	-.1654	.6370	.0263	.0665	-.0441
50.81	10.09	2.8476	-.1627	.5508	.1128	.0906	-.0357
50.81	8.09	2.8358	-.1615	.5030	.1516	.0900	-.0288
50.81	4.14	2.7997	-.1600	.3593	.1683	.0825	-.0119
50.82	.15	2.8838	-.1657	.1622	.0271	.0046	.0133
50.85	-3.78	2.9257	-.1657	.2402	-.0363	-.0191	.0192
50.86	-7.76	2.9146	-.1648	.3406	-.0269	-.0346	.0321
50.87	-9.73	2.9225	-.1673	.4273	-.0661	-.0566	.0341

APPENDIX - Continued

RUN 144		Q= 13.40 PSF		RN/FT= .343		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.62	-9.75	2.5287	-.1284	.2007	.1520	.0331	.0309
40.61	-7.76	2.5429	-.1228	.1605	.1016	.0282	.0268
40.61	-3.75	2.6139	-.1189	.0931	-.0260	.0041	.0215
40.61	.15	2.6198	-.1198	.0691	.0512	.0122	.0000
40.62	4.14	2.7130	-.1232	.1320	.1395	.0270	-.0226
40.61	8.09	2.7909	-.1288	.2386	.1572	.0368	-.0310
40.62	10.10	2.8155	-.1301	.2994	.1435	.0433	-.0392
40.59	15.06	2.6113	-.1179	.3805	.0222	.0502	-.0525
40.61	20.01	2.6078	-.1199	.4461	-.0134	.0553	-.0655
40.60	29.88	2.4182	-.0986	.3648	-.1598	-.0052	-.1048

RUN 145		Q= 24.90 PSF		RN/FT= .595		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.62	.22	2.2314	.0537	-.3744	.0101	.0146	.0006
50.79	.20	2.4226	-.0526	-.2859	-.0149	.0244	-.0077
60.51	.21	2.5093	-.1115	-.1757	.0340	.0378	-.0046
70.21	.22	2.5105	-.1573	-.2486	-.0010	.0091	.0001
80.13	.20	2.5444	-.2153	-.1292	-.0313	-.0093	.0010
90.61	.20	2.4878	-.2474	-.2827	-.0015	.0026	.0005

APPENDIX - Continued

RUN 146		Q= 25.30 PSF		RN/FT= .604		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
90.64	-9.75	2.4471	-.2362	-.3329	-.0568	.0001	.0309
90.65	-7.75	2.4396	-.2366	-.3340	-.0382	-.0030	.0241
90.66	-3.79	2.4573	-.2421	-.2974	-.0063	.0102	.0119
90.65	.16	2.4662	-.2453	-.2811	-.0132	.0033	.0004
90.64	4.15	2.4710	-.2414	-.2961	.0066	-.0060	-.0129
90.63	8.11	2.4661	-.2366	-.3358	.0110	-.0022	-.0238
90.63	10.06	2.4552	-.2320	-.3414	.0128	-.0016	-.0295
90.61	15.06	2.4264	-.2184	-.3372	.0036	-.0146	-.0414
90.61	19.97	2.4104	-.2015	-.3378	-.0313	-.0372	-.0510
90.59	29.89	2.2931	-.1824	-.3668	-.1506	-.0796	-.0710

RUN 147		Q= 24.50 PSF		RN/FT= .599		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.24	29.88	2.3279	-.1756	-.3386	-.1560	-.0994	-.0662
85.27	20.00	2.4438	-.1953	-.2859	-.0440	-.0454	-.0491
85.27	15.06	2.4647	-.2101	-.2542	.0271	-.0124	-.0397
85.27	10.09	2.4787	-.2184	-.2656	.0567	.0134	-.0280
85.28	8.09	2.5020	-.2217	-.2627	.0652	.0157	-.0226
85.29	4.14	2.5124	-.2215	-.2447	.0328	.0076	-.0121
85.29	.14	2.5402	-.2276	-.1989	.0007	-.0020	.0005
85.31	-3.80	2.5091	-.2234	-.2493	-.0336	-.0127	.0119
85.32	-7.74	2.4864	-.2225	-.2815	-.0478	-.0145	.0225
85.33	-9.73	2.4757	-.2213	-.2729	-.0366	-.0031	.0287

APPENDIX - Continued

RUN 148		Q= 24.40 PSF	RN/FT= .601		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
80.11	-9.72	2.5223	-.2114	-.1824	-.0021	.0167	.0253
80.12	-7.74	2.5177	-.2117	-.1717	-.0307	.0068	.0203
80.11	-3.79	2.5360	-.2135	-.1585	-.0222	-.0011	.0099
80.09	.22	2.5339	-.2147	-.1142	-.0015	-.0073	.0019
80.08	4.12	2.5380	-.2174	-.1921	.0366	.0145	-.0101
80.06	8.11	2.5178	-.2069	-.1815	.0256	.0052	-.0193
80.06	10.13	2.4991	-.2046	-.1823	.0156	-.0051	-.0241
80.04	15.07	2.4991	-.2003	-.2161	-.0294	-.0373	-.0344
80.04	19.99	2.4590	-.1871	-.2344	-.0554	-.0549	-.0451
80.02	29.94	2.3467	-.1623	-.2903	-.1898	-.1115	-.0616

RUN 149		Q= 24.10 PSF	RN/FT= .587		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
75.06	29.95	2.3426	-.1455	-.2350	-.2392	-.1229	-.0578
75.10	20.06	2.4860	-.1642	-.2340	-.1133	-.0919	-.0395
75.12	15.04	2.5118	-.1735	-.1892	-.0546	-.0687	-.0306
75.12	10.13	2.5328	-.1848	-.1702	-.0117	-.0338	-.0192
75.12	8.10	2.5515	-.1886	-.1709	.0040	-.0242	-.0145
75.12	4.15	2.5525	-.1905	-.1802	-.0130	-.0204	-.0059
75.13	.16	2.5771	-.1957	-.1533	.0155	-.0020	.0013
75.15	-3.79	2.5699	-.1928	-.1392	-.0054	.0121	.0079
75.17	-7.75	2.5543	-.1895	-.1543	-.0081	.0249	.0156
75.17	-9.77	2.5490	-.1915	-.1617	.0075	.0443	.0201

APPENDIX - Continued

RUN 150		Q= 24.80 PSF		RN/FT= .596		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
70.15	-9.77	2.5439	-.1516	-.1788	.0205	.0638	.0167
70.15	-7.76	2.5438	-.1550	-.1696	.0060	.0387	.0134
70.15	-3.82	2.5624	-.1595	-.1571	.0065	.0227	.0059
70.13	.15	2.5303	-.1562	-.2420	.0210	.0179	.0001
70.11	4.14	2.5240	-.1544	-.2200	-.0123	-.0213	-.0052
70.11	8.07	2.5443	-.1516	-.2041	-.0385	-.0469	-.0120
70.11	10.14	2.5341	-.1510	-.2046	-.0500	-.0632	-.0152
70.11	15.06	2.4895	-.1405	-.2040	-.0994	-.0935	-.0260
70.11	20.05	2.4577	-.1310	-.2200	-.1696	-.1154	-.0355
70.08	29.95	2.3332	-.1187	-.1226	-.2766	-.1107	-.0602

RUN 151		Q= 24.70 PSF		RN/FT= .595		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
65.33	29.96	2.3817	-.0947	-.0164	-.2690	-.0967	-.0564
65.34	20.03	2.4587	-.1181	-.0959	-.1466	-.0919	-.0321
65.32	15.04	2.4729	-.1096	-.2149	-.1181	-.1122	-.0210
65.32	10.07	2.5064	-.1200	-.2401	-.0682	-.0776	-.0127
65.32	8.15	2.5067	-.1155	-.2423	-.0363	-.0551	-.0104
65.32	4.16	2.5173	-.1104	-.2549	.0402	.0130	-.0070
65.34	.23	2.5089	-.1111	-.2695	.0614	.0394	-.0022
65.37	-3.79	2.5357	-.1166	-.2126	.0373	.0386	.0042
65.38	-7.79	2.5196	-.1141	-.2088	.0358	.0570	.0118
65.38	-9.75	2.5155	-.1132	-.2122	.0481	.0745	.0145

APPENDIX - Continued

RUN 152		Q= 25.20 PSF	RN/FT= .602		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
60.51	-9.75	2.4941	-.0975	-.1910	.0631	.0733	.0158
60.50	-7.73	2.4787	-.1054	-.1825	.0346	.0542	.0123
60.49	-3.78	2.4639	-.1078	-.2012	.0150	.0316	.0036
60.48	.17	2.5024	-.1134	-.1723	.0320	.0389	-.0044
60.47	4.15	2.5052	-.1144	-.1082	.0666	.0568	-.0141
60.47	8.09	2.5037	-.1123	-.1220	.0461	.0131	-.0143
60.44	10.17	2.4735	-.0857	-.2385	-.0565	-.0582	-.0138
60.46	15.09	2.4626	-.1014	-.1279	-.1504	-.0986	-.0212
60.47	20.07	2.4491	-.1056	-.0833	-.2055	-.1207	-.0281
60.47	29.95	2.4264	-.0804	.0175	-.3082	-.1131	-.0786

RUN 153		Q= 25.50 PSF	RN/FT= .607		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
50.85	29.96	2.6059	-.0251	-.0919	-.2289	-.1205	-.1125
50.86	20.03	2.7011	-.0297	-.0928	-.0683	-.0751	-.0618
50.86	15.06	2.7257	-.0406	-.1138	.0419	-.0654	-.0494
50.82	10.11	2.5295	-.0539	.0393	.0564	.0657	-.0349
50.81	8.11	2.4728	-.0500	.0104	.0754	.0894	-.0376
50.81	4.14	2.4789	-.0550	-.1410	.1180	.0747	-.0153
50.81	.18	2.4306	-.0555	-.2808	-.0084	.0235	-.0070
50.83	-3.80	2.4779	-.0548	-.2833	-.0493	.0299	.0092
50.89	-7.79	2.6403	-.0539	-.2335	-.0563	.0739	.0276
50.90	-9.75	2.6697	-.0465	-.2440	-.0418	.0889	.0314

APPENDIX - Continued

RUN 154		Q= 23.50 PSF		RN/FT= .583		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.62	-9.75	2.3308	.0478	-.2934	.1012	.0537	.0238
40.59	-7.76	2.2737	.0512	-.3086	.0916	.0367	.0158
40.58	-3.82	2.2368	.0531	-.3567	.0635	.0072	.0043
40.56	.21	2.2328	.0557	-.3770	.0180	.0157	.0011
40.55	4.12	2.2028	.0565	-.3072	-.0090	.0319	.0023
40.56	8.13	2.2451	.0648	-.1945	.0674	.0384	-.0236
40.55	10.13	2.2396	.0666	-.1484	.0546	.0415	-.0238
40.57	15.05	2.2874	.0549	-.1598	-.0503	-.0072	-.0401
40.59	20.04	2.3301	.0625	-.2323	-.1546	-.0533	-.0641
40.58	29.93	2.3112	.0670	-.2525	-.2659	-.0595	-.1060

RUN 155		Q= 39.20 PSF		RN/FT= .903		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.92	.18	2.1576	.0463	-.3720	-.0069	.0151	.0026
50.90	.21	2.3182	-.0554	-.2988	-.0170	.0110	-.0035
60.58	.22	2.3655	-.1184	-.2659	.0015	.0067	.0006
70.30	.21	2.4092	-.1545	-.3470	-.0129	.0030	.0006
80.13	.20	2.4562	-.2100	-.3042	-.0869	-.0412	.0018
90.68	.21	2.4182	-.2419	-.2767	-.0001	-.0008	.0002

APPENDIX - Continued

RUN 156		Q= 39.40 PSF	RN/FT= .915		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
90.64	29.96	2.2272	-.1916	-.3525	-.1302	-.0792	-.0686
90.64	20.01	2.3423	-.1991	-.3469	-.0423	-.0416	-.0497
90.64	15.06	2.3929	-.2185	-.3479	-.0014	-.0175	-.0408
90.68	10.10	2.4101	-.2306	-.3491	.0414	.0077	-.0287
90.69	8.13	2.4252	-.2350	-.3391	.0310	.0001	-.0234
90.72	4.10	2.4257	-.2428	-.3076	.0115	.0050	-.0107
90.72	.17	2.4173	-.2431	-.2798	.0024	.0001	-.0004
90.73	-3.75	2.4257	-.2424	-.3246	-.0331	-.0158	.0137
90.72	-7.84	2.4065	-.2348	-.3416	-.0393	-.0057	.0254
90.74	-9.76	2.3946	-.2323	-.3427	-.0331	-.0005	.0302

RUN 157		Q= 37.00 PSF	RN/FT= .892		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.35	-9.75	2.4344	-.2198	-.2722	-.0496	-.0075	.0277
85.35	-7.73	2.4222	-.2183	-.3056	-.0544	-.0082	.0234
85.34	-3.77	2.4277	-.2200	-.3168	-.0529	-.0232	.0119
85.34	.13	2.4674	-.2240	-.2288	-.0248	-.0148	.0005
85.32	4.12	2.4385	-.2216	-.3032	.0361	.0152	-.0109
85.31	8.15	2.4244	-.2167	-.3218	.0489	.0126	-.0219
85.31	10.13	2.4297	-.2166	-.3222	.0447	.0037	-.0271
85.30	15.03	2.4119	-.2079	-.3046	.0059	-.0196	-.0367
85.29	20.00	2.3775	-.1953	-.2930	-.0482	-.0456	-.0467
85.28	29.93	2.2807	-.1815	-.3265	-.1494	-.0928	-.0646

APPENDIX - Continued

RUN 158		Q= 37.70 PSF		RN/FT= .904		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.21	29.94	2.2964	-.1646	-.2939	-.1747	-.1127	-.0591
80.22	19.96	2.3958	-.1851	-.2702	-.0661	-.0653	-.0421
80.23	15.05	2.4160	-.1971	-.2488	-.0198	-.0365	-.0336
80.23	10.09	2.4543	-.1968	-.2654	.0290	-.0024	-.0242
80.24	8.13	2.4494	-.1971	-.2669	.0467	.0075	-.0190
80.26	4.14	2.4689	-.2046	-.2584	.0505	.0110	-.0109
80.25	.11	2.4649	-.2135	-.2996	-.0868	-.0634	.0034
80.25	-3.79	2.4545	-.2028	-.2672	-.0349	-.0163	.0118
80.27	-7.72	2.4487	-.2058	-.2614	-.0277	.0053	.0198
80.27	-9.71	2.4428	-.2071	-.2155	-.0185	.0107	.0248

RUN 159		Q= 37.10 PSF		RN/FT= .899		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
75.16	-9.70	2.4821	-.1939	-.1748	-.0085	.0379	.0209
75.16	-7.76	2.4702	-.1881	-.2046	-.0361	.0292	.0167
75.15	-3.81	2.4801	-.1895	-.2593	-.0078	.0226	.0090
75.12	.21	2.4384	-.1892	-.3125	.0165	.0185	.0002
75.12	4.19	2.4513	-.1884	-.2740	-.0234	-.0161	-.0068
75.12	8.15	2.4522	-.1847	-.2499	-.0073	-.0249	-.0172
75.13	10.10	2.4409	-.1794	-.2692	-.0343	-.0444	-.0199
75.16	15.12	2.4343	-.1803	-.2529	-.0799	-.0788	-.0290
75.14	20.05	2.3688	-.1618	-.2859	-.1468	-.1112	-.0370
75.12	29.95	2.2798	-.1400	-.2404	-.2065	-.1185	-.0552

APPENDIX - Continued

RUN 160		Q= 37.10 PSF		RN/FT= .901		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.24	29.94	2.3010	-.1207	-.1291	-.2146	-.1110	-.0525
70.25	20.06	2.3642	-.1360	-.2418	-.1439	-.1140	-.0333
70.26	15.03	2.4119	-.1508	-.2471	-.0912	-.0926	-.0251
70.25	10.16	2.4221	-.1593	-.3073	-.0769	-.0764	-.0159
70.25	8.15	2.4406	-.1564	-.3289	-.0702	-.0626	-.0119
70.24	4.19	2.4144	-.1526	-.3559	-.0454	-.0349	-.0049
70.24	.16	2.4428	-.1569	-.3534	-.0156	.0015	.0007
70.25	-3.78	2.4278	-.1567	-.3479	.0103	.0353	.0065
70.28	-7.75	2.4508	-.1579	-.2396	-.0059	.0464	.0138
70.30	-9.75	2.4351	-.1550	-.2214	.0201	.0636	.0159

RUN 161		Q= 36.10 PSF		RN/FT= .892		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.38	-9.73	2.4090	-.1129	-.2618	.0277	.0696	.0138
65.39	-7.75	2.4144	-.1118	-.2915	.0085	.0549	.0112
65.36	-3.78	2.3889	-.1122	-.3704	.0022	.0319	.0049
65.35	.18	2.3968	-.1106	-.3718	-.0109	.0026	.0003
65.34	4.18	2.3881	-.1092	-.3701	-.0393	-.0255	-.0041
65.34	8.14	2.3877	-.1055	-.3568	-.0739	-.0623	-.0091
65.35	10.17	2.3937	-.1166	-.3120	-.0689	-.0673	-.0127
65.37	15.10	2.3814	-.1084	-.2674	-.1249	-.1093	-.0203
65.38	20.06	2.3710	-.1071	-.1785	-.1348	-.0926	-.0304
65.38	29.95	2.3348	-.1051	.0250	-.2156	-.0839	-.0527

APPENDIX - Continued

RUN 162		Q= 36.50 PSF	RN/FT= .899		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.66	29.97	2.3776	-.0924	-.0174	-.2912	-.1189	-.0725
60.63	20.06	2.3360	-.0829	-.2023	-.2305	-.1364	-.0270
60.62	15.05	2.3655	-.0935	-.2353	-.1339	-.0929	-.0207
60.60	10.14	2.3713	-.0750	-.3403	-.0599	-.0674	-.0117
60.61	8.16	2.3796	-.0808	-.3453	-.0371	-.0490	-.0086
60.61	4.12	2.3686	-.1088	-.3059	.0086	-.0107	-.0026
60.63	.15	2.4060	-.1222	-.2793	.0149	.0078	.0018
60.64	-3.78	2.3684	-.1056	-.3042	.0067	.0248	.0034
60.66	-7.73	2.3585	-.0765	-.3350	.0488	.0628	.0101
60.66	-9.73	2.3650	-.0805	-.2898	.0682	.0793	.0136

RUN 163		Q= 36.10 PSF	RN/FT= .897		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
50.90	-9.71	2.5390	-.0436	-.2676	-.0608	.0602	.0323
50.89	-7.73	2.4817	-.0458	-.2735	-.0820	.0460	.0271
50.84	-3.71	2.3496	-.0448	-.3147	-.0615	.0336	.0034
50.83	.16	2.3228	-.0535	-.3039	-.0152	.0132	-.0053
50.82	4.12	2.3605	-.0555	-.2517	.0157	.0185	-.0197
50.83	8.10	2.4204	-.0479	-.2539	.0753	-.0265	-.0211
50.84	10.14	2.4878	-.0403	-.2548	.0677	-.0392	-.0289
50.86	15.10	2.4971	-.0331	-.2130	-.0178	-.0648	-.0388
50.88	20.07	2.5269	-.0232	-.1999	-.0626	-.0719	-.0570
50.83	29.94	2.4519	-.0080	-.2029	-.1353	-.0764	-.1108

APPENDIX - Continued

RUN 164 Q= 36.40 PSF RN/FT= .903 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.73	29.94	2.1944	.0524	-.2622	-.2134	-.0484	-.0995
40.78	20.03	2.3591	.0539	-.3506	-.0285	-.0532	-.0562
40.75	15.04	2.2611	.0432	-.2968	-.0653	-.0551	-.0387
40.72	10.10	2.1814	.0511	-.2953	-.0530	-.0269	-.0261
40.71	8.14	2.1558	.0500	-.3102	-.0427	-.0043	-.0168
40.70	4.15	2.1191	.0488	-.3525	-.0747	.0295	-.0055
40.72	.18	2.1610	.0488	-.3737	-.0035	.0139	.0028
40.73	-3.79	2.1412	.0463	-.3527	.0712	.0032	.0043
40.76	-7.77	2.1673	.0452	-.3147	.0578	.0149	.0166
40.77	-9.78	2.2266	.0442	-.3051	.0579	.0413	.0217

RUN 165 Q= 43.70 PSF RN/FT= 1.067 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.70	.18	2.1319	.0483	-.3767	-.0164	.0136	.0024
50.85	.17	2.3124	-.0577	-.3169	-.0030	.0012	.0001
60.66	.16	2.3411	-.1241	-.2824	.0123	.0047	.0020
70.34	.15	2.4148	-.1563	-.3542	-.0180	.0013	.0009
80.34	.17	2.3958	-.2100	-.3337	-.0569	-.0394	.0019
90.79	.16	2.3826	-.2425	-.3176	-.0289	-.0157	.0011

APPENDIX - Continued

RUN 166		Q= 44.60 PSF		RN/FT= 1.078		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
90.81	-9.74	2.3797	-.2362	-.3463	-.0417	-.0037	.0302
90.79	-7.77	2.3738	-.2382	-.3484	-.0505	-.0122	.0251
90.79	-3.79	2.4070	-.2443	-.3398	-.0570	-.0229	.0150
90.78	.17	2.3882	-.2429	-.3113	-.0314	-.0136	.0002
90.77	4.14	2.3850	-.2396	-.3531	-.0089	-.0079	-.0115
90.75	8.11	2.3597	-.2321	-.3895	-.0027	-.0109	-.0226
90.75	10.13	2.3613	-.2308	-.3932	-.0127	-.0180	-.0288
90.74	15.05	2.3376	-.2201	-.4003	-.0524	-.0393	-.0392
90.73	20.05	2.3204	-.2013	-.3601	-.0708	-.0516	-.0484
90.70	29.93	2.2160	-.1982	-.3500	-.1198	-.0742	-.0677

RUN 167		Q= 43.60 PSF		RN/FT= 1.067		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
85.43	29.93	2.2782	-.1868	-.3293	-.1449	-.0919	-.0644
85.44	20.04	2.3347	-.2008	-.3040	-.0548	-.0496	-.0455
85.45	15.10	2.3845	-.2143	-.2937	.0016	-.0198	-.0365
85.46	10.13	2.3944	-.2203	-.2999	.0423	.0070	-.0264
85.45	8.10	2.3800	-.2211	-.3439	.0306	-.0036	-.0222
85.46	4.15	2.3949	-.2293	-.3057	.0461	.0180	-.0103
85.48	.19	2.4235	-.2294	-.2893	-.0141	-.0197	.0009
85.49	-3.79	2.3941	-.2247	-.3244	-.0638	-.0294	.0125
85.49	-7.77	2.3802	-.2269	-.3188	-.0487	-.0088	.0234
85.50	-9.71	2.3750	-.2267	-.3137	-.0319	.0001	.0263

APPENDIX - Continued

RUN 168		Q= 43.30 PSF		RN/FT= 1.062		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.22	-9.70	2.4062	-.2195	-.2639	-.0297	.0074	.0248
80.21	-7.76	2.4067	-.2157	-.2741	-.0397	-.0038	.0199
80.20	-3.81	2.4198	-.2124	-.2747	-.0677	-.0264	.0106
80.19	.16	2.4025	-.2128	-.3249	-.0731	-.0384	.0017
80.19	4.16	2.3922	-.2126	-.2960	.0032	-.0029	-.0105
80.17	8.13	2.3977	-.1985	-.3352	-.0064	-.0065	-.0195
80.18	10.12	2.3706	-.1955	-.3386	-.0222	-.0330	-.0223
80.18	15.04	2.4077	-.2009	-.2497	-.0388	-.0417	-.0348
80.17	20.05	2.3529	-.1897	-.2746	-.0941	-.0743	-.0412
80.15	29.93	2.2719	-.1684	-.2927	-.1652	-.1103	-.0588

RUN 169		Q= 44.10 PSF		RN/FT= 1.072		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
75.22	29.95	2.2902	-.1515	-.1774	-.1534	-.0926	-.0547
75.23	20.01	2.3588	-.1671	-.3010	-.1478	-.1120	-.0367
75.25	15.05	2.3957	-.1837	-.2600	-.0714	-.0747	-.0287
75.23	10.11	2.3702	-.1832	-.3658	-.0732	-.0638	-.0190
75.24	8.09	2.4011	-.1851	-.3582	-.0449	-.0511	-.0141
75.25	4.16	2.4070	-.1899	-.3514	-.0082	-.0219	-.0062
75.25	.14	2.4063	-.1953	-.3518	.0145	.0253	.0006
75.28	-3.80	2.4464	-.1944	-.2897	-.0386	.0102	.0093
75.29	-7.75	2.4299	-.1964	-.2696	-.0197	.0263	.0176
75.31	-9.78	2.4299	-.1978	-.2294	.0047	.0356	.0215

APPENDIX - Continued

RUN 170		Q= 43.80 PSF		RN/FT= 1.069		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.32	-9.77	2.4166	-.1568	-.2803	.0314	.0631	.0166
70.31	-7.79	2.3893	-.1546	-.3339	.0208	.0609	.0127
70.29	-3.80	2.3875	-.1569	-.3611	.0124	.0378	.0062
70.28	.17	2.3924	-.1561	-.3526	-.0157	.0006	.0012
70.27	4.17	2.4018	-.1553	-.3606	-.0527	-.0360	-.0049
70.25	8.15	2.3807	-.1594	-.3720	-.0782	-.0646	-.0119
70.25	10.12	2.3826	-.1588	-.3827	-.0868	-.0820	-.0155
70.25	15.04	2.3670	-.1495	-.3087	-.1369	-.1041	-.0248
70.25	20.04	2.3476	-.1369	-.2483	-.1683	-.1125	-.0332
70.25	29.96	2.3169	-.1315	-.0419	-.1626	-.0714	-.0530

RUN 171		Q= 43.70 PSF		RN/FT= 1.067		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.47	29.97	2.2932	-.1118	-.0068	-.2022	-.0866	-.0504
65.47	20.07	2.3183	-.1114	-.2134	-.1742	-.1230	-.0285
65.46	15.06	2.3257	-.1123	-.2700	-.1096	-.1004	-.0213
65.45	10.09	2.3554	-.1191	-.3463	-.0664	-.0697	-.0124
65.45	8.10	2.3614	-.1212	-.3599	-.0531	-.0553	-.0099
65.44	4.14	2.3469	-.1129	-.3661	-.0382	-.0326	-.0046
65.44	.15	2.3713	-.1159	-.3739	-.0205	.0018	.0004
65.45	-3.79	2.3601	-.1143	-.3754	-.0033	.0350	.0040
65.48	-7.79	2.3538	-.1130	-.3612	.0170	.0624	.0100
65.50	-9.74	2.3615	-.1144	-.3332	.0355	.0741	.0128

APPENDIX - Continued

RUN 172		Q= 43.40 PSF		RN/FT= 1.064		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.59	-9.73	2.3296	-.0789	-.3370	.0524	.0755	.0125
60.58	-7.79	2.3369	-.0781	-.3525	.0386	.0623	.0095
60.57	-3.78	2.3233	-.1054	-.3028	-.0024	.0208	.0032
60.58	.17	2.3374	-.1267	-.2818	.0116	.0042	.0017
60.56	4.12	2.3316	-.1093	-.3067	-.0005	-.0132	-.0020
60.57	8.12	2.3389	-.0833	-.3434	-.0430	-.0454	-.0094
60.57	10.15	2.3324	-.0756	-.3459	-.0582	-.0640	-.0117
60.58	15.07	2.3098	-.0828	-.2965	-.1595	-.0946	-.0205
60.60	20.05	2.3085	-.0802	-.2299	-.2580	-.1375	-.0266
60.62	29.95	2.3212	-.1001	-.0169	-.3130	-.1188	-.0541

RUN 173		Q= 43.60 PSF		RN/FT= 1.067		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
50.92	29.93	2.4253	-.0205	-.2079	-.1302	-.0703	-.1070
50.93	10.11	2.4346	-.0401	-.2658	.0580	-.0322	-.0288
50.91	8.13	2.4005	-.0424	-.2891	.0661	-.0289	-.0190
50.90	4.16	2.3331	-.0507	-.3282	.0520	-.0258	-.0002
50.90	.16	2.3302	-.0598	-.3212	-.0048	.0003	.0005
50.91	-3.77	2.3450	-.0481	-.3254	-.0599	.0311	.0046
50.96	-7.74	2.4726	-.0489	-.2795	-.0757	.0393	.0297
50.98	-9.74	2.4817	-.0450	-.2842	-.0843	.0446	.0329
50.96	20.07	2.5133	-.0344	-.2279	-.0754	-.0667	-.0570
50.95	15.07	2.4795	-.0376	-.2341	-.0069	-.0550	-.0393

APPENDIX - Continued

RUN 174		Q= 44.30 PSF		RN/FT= 1.076		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.76	-9.75	2.2078	.0462	-.3486	.0040	.0274	.0201
40.74	-7.73	2.1483	.0471	-.3422	.0221	.0118	.0161
40.73	-3.79	2.1150	.0470	-.3605	.0496	.0023	.0045
40.71	.16	2.1172	.0485	-.3781	-.0258	.0150	.0012
40.68	4.13	2.0943	.0479	-.3595	-.0830	.0171	-.0051
40.69	8.16	2.1410	.0505	-.3370	-.0343	-.0116	-.0183
40.71	10.13	2.1913	.0502	-.3473	.0053	-.0199	-.0165
40.74	15.04	2.2759	.0467	-.3420	-.0251	-.0474	-.0345
40.76	20.04	2.3262	.0526	-.3395	.0018	-.0418	-.0568
40.74	29.96	2.2250	.0475	-.3142	-.2176	-.0490	-.1017

RUN 175		Q= 23.70 PSF		RN/FT= .590		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.64	.21	2.2365	.0520	-.3683	-.0110	.0094	-.0003
50.74	.21	2.4047	-.0584	-.2863	.0069	-.0002	.0052
60.51	.20	2.4342	-.1186	-.2643	.0234	.0136	.0023
70.18	.20	2.4724	-.1564	-.3392	.0001	.0124	-.0001
80.13	.21	2.4390	-.2110	-.4125	-.0057	.0024	.0006
90.62	.22	2.3704	-.2557	-.4884	-.0040	.0062	.0008

APPENDIX - Continued

RUN 176		Q= 25.00 PSF	RN/FT= .604		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
90.65	-9.71	2.3552	-.2406	-.4954	.0845	.0925	.0248
90.66	-7.75	2.3578	-.2426	-.4832	.0630	.0809	.0215
90.66	-3.79	2.3716	-.2503	-.4519	.0417	.0502	.0098
90.64	.19	2.3679	-.2535	-.4921	-.0085	.0067	.0002
90.63	4.17	2.3865	-.2509	-.4792	-.0227	-.0218	-.0120
90.63	8.14	2.3816	-.2405	-.4612	-.1141	-.0799	-.0210
90.63	10.10	2.3819	-.2399	-.4759	-.1180	-.0887	-.0256
90.62	15.04	2.3522	-.2238	-.5054	-.1626	-.1066	-.0362
90.62	20.05	2.3148	-.2079	-.5332	-.1988	-.1266	-.0468
90.60	29.96	2.2047	-.1924	-.5462	-.2701	-.1388	-.0661

RUN 177		Q= 24.40 PSF	RN/FT= .598		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
85.27	29.97	2.2519	-.1824	-.5308	-.2747	-.1609	-.0617
85.29	20.03	2.3460	-.2040	-.5174	-.2013	-.1375	-.0439
85.31	15.07	2.3926	-.2179	-.4803	-.1539	-.1128	-.0341
85.31	10.10	2.4041	-.2258	-.4546	-.1011	-.0810	-.0237
85.31	8.11	2.4321	-.2282	-.4437	-.0875	-.0703	-.0178
85.31	4.16	2.4238	-.2306	-.4257	-.0427	-.0379	-.0088
85.31	.17	2.4312	-.2344	-.4168	.0052	.0018	.0009
85.33	-3.77	2.4187	-.2328	-.4243	.0321	.0370	.0091
85.35	-7.78	2.4099	-.2267	-.4503	.0866	.0770	.0178
85.35	-9.77	2.4003	-.2255	-.4614	.0896	.0932	.0227

APPENDIX - Continued

RUN 178		Q= 25.10 PSF		RN/FT= .606		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.10	-9.77	2.4208	-.2112	-.4236	.0992	.1003	.0208
80.11	-7.75	2.4252	-.2102	-.4127	.0726	.0819	.0159
80.10	-3.77	2.4292	-.2123	-.4109	.0347	.0414	.0080
80.09	.17	2.4370	-.2095	-.4123	-.0007	.0037	.0006
80.07	4.14	2.4442	-.2117	-.4013	-.0314	-.0365	-.0077
80.07	8.10	2.4390	-.2058	-.4042	-.0980	-.0743	-.0160
80.06	10.13	2.4327	-.2038	-.4191	-.1244	-.0967	-.0200
80.06	15.10	2.3969	-.1999	-.4686	-.1846	-.1291	-.0299
80.06	20.04	2.3602	-.1881	-.4745	-.2120	-.1420	-.0396
80.03	29.95	2.2450	-.1621	-.4889	-.3066	-.1725	-.0566

RUN 179		Q= 25.30 PSF		RN/FT= .610		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
75.09	29.96	2.2419	-.1410	-.4397	-.3304	-.1739	-.0539
75.12	20.05	2.3482	-.1619	-.4605	-.2736	-.1709	-.0341
75.12	15.10	2.4147	-.1692	-.4430	-.2022	-.1432	-.0263
75.11	10.12	2.4621	-.1789	-.4020	-.1334	-.1041	-.0171
75.12	8.15	2.4566	-.1785	-.3972	-.1140	-.0840	-.0130
75.12	4.14	2.4697	-.1843	-.3815	-.0574	-.0404	-.0052
75.13	.18	2.4695	-.1857	-.3718	-.0031	.0101	.0006
75.15	-3.80	2.4548	-.1855	-.3776	.0323	.0452	.0068
75.17	-7.76	2.4496	-.1835	-.3999	.0749	.0865	.0129
75.17	-9.76	2.4188	-.1853	-.4099	.0942	.1054	.0184

APPENDIX - Continued

RUN 180		Q= 25.30 PSF		RN/FT= .610		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.18	-9.76	2.4267	-.1456	-.3747	.0845	.1008	.0143
70.18	-7.75	2.4469	-.1491	-.3731	.0561	.0828	.0111
70.17	-3.77	2.4585	-.1517	-.3594	.0277	.0488	.0046
70.16	.16	2.4743	-.1568	-.3463	-.0001	.0121	.0007
70.14	4.15	2.4646	-.1535	-.3608	-.0475	-.0388	-.0040
70.13	8.12	2.4625	-.1439	-.3728	-.0954	-.0766	-.0107
70.13	10.09	2.4486	-.1438	-.3769	-.1198	-.0986	-.0137
70.13	15.08	2.3976	-.1384	-.3978	-.2019	-.1515	-.0221
70.13	20.06	2.3442	-.1281	-.4175	-.2979	-.1764	-.0313
70.11	29.97	2.2571	-.1173	-.3131	-.3601	-.1614	-.0557

RUN 181		Q= 25.00 PSF		RN/FT= .608		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.32	29.97	2.2887	-.0934	-.1565	-.3314	-.1325	-.0527
65.34	20.06	2.3650	-.1187	-.2844	-.2920	-.1604	-.0277
65.33	15.06	2.3976	-.1072	-.3509	-.1809	-.1415	-.0185
65.32	10.12	2.4387	-.1126	-.3519	-.1015	-.0900	-.0104
65.32	8.13	2.4269	-.1141	-.3489	-.0635	-.0689	-.0083
65.32	4.15	2.4638	-.1061	-.3523	-.0106	-.0217	-.0047
65.33	.13	2.4576	-.1090	-.3459	.0141	.0164	-.0008
65.35	-3.79	2.4401	-.1108	-.3490	.0225	.0483	.0034
65.37	-7.76	2.4221	-.1077	-.3714	.0343	.0814	.0082
65.37	-9.78	2.4039	-.1067	-.3683	.0600	.0971	.0110

APPENDIX - Continued

RUN 182		Q= 25.60 PSF		RN/FT= .615		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.49	-9.77	2.3837	-.0738	-.3296	.0520	.0785	.0112
60.49	-7.73	2.3896	-.0709	-.3557	.0385	.0736	.0078
60.48	-3.76	2.4091	-.1010	-.2998	.0068	.0310	.0028
60.47	.20	2.3933	-.1179	-.2391	.0082	.0082	.0010
60.45	4.16	2.3922	-.1046	-.2837	.0081	-.0047	-.0035
60.44	8.11	2.3874	-.0784	-.3263	-.0482	-.0467	-.0091
60.44	10.11	2.3795	-.0747	-.3236	-.0823	-.0753	-.0107
60.47	15.11	2.4193	-.1156	-.1177	-.1773	-.0961	-.0216
60.47	20.04	2.3483	-.1013	-.1760	-.2561	-.1310	-.0274
60.46	29.94	2.3407	-.0956	.0180	-.3230	-.1252	-.0579

RUN 183		Q= 25.60 PSF		RN/FT= .617		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
50.81	29.96	2.5464	-.0255	-.1381	-.2506	-.1258	-.1082
50.83	20.06	2.6123	-.0392	-.1313	-.0783	-.0677	-.0503
50.81	15.07	2.5521	-.0405	-.1769	-.0254	-.0692	-.0328
50.80	10.10	2.5071	-.0617	-.1787	.0280	-.0464	-.0130
50.81	8.13	2.5132	-.0709	-.1531	.0517	-.0213	-.0140
50.78	4.15	2.4177	-.0616	-.2575	.0333	-.0125	-.0104
50.79	.16	2.4007	-.0600	-.2883	.0037	.0010	.0036
50.81	-3.77	2.4280	-.0534	-.3114	-.0674	.0370	.0040
50.85	-7.75	2.5639	-.0525	-.2885	-.0675	.0611	.0228
50.86	-9.78	2.5826	-.0490	-.2927	-.0534	.0718	.0261

APPENDIX - Continued

RUN 184		Q= 25.30 PSF		RN/FT= .614		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.63	-9.76	2.2777	.0404	-.2961	.0587	.0287	.0252
40.61	-7.76	2.2339	.0439	-.3139	.0650	.0170	.0171
40.59	-3.78	2.1908	.0475	-.3582	.0590	.0045	.0057
40.57	.19	2.1839	.0494	-.3679	-.0157	.0118	.0004
40.55	4.15	2.1631	.0499	-.3458	-.0821	.0235	-.0052
40.55	8.14	2.1680	.0490	-.2916	-.0758	.0067	-.0178
40.57	10.10	2.2300	.0467	-.2652	-.0735	-.0068	-.0283
40.59	15.05	2.2839	.0371	-.2235	-.0623	-.0195	-.0416
40.60	20.03	2.2872	.0511	-.2032	-.1450	-.0392	-.0591
40.57	29.95	2.1962	.0607	-.2073	-.2560	-.0540	-.0962

RUN 185		Q= 25.00 PSF		RN/FT= .594		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.59	.22	2.2048	.0617	-.3132	.0338	.0102	.0002
50.84	.21	2.4847	-.0456	-.1157	.0111	.0042	.0028
60.55	.22	2.6146	-.1391	.1321	-.0179	-.0002	.0050
70.28	.20	2.6499	-.1744	.1646	-.0592	-.0327	.0006
80.21	.21	2.6061	-.2132	.1315	-.0225	-.0084	.0006
90.74	.20	2.5372	-.2484	-.0841	-.0108	-.0003	.0005

APPENDIX - Continued

RUN 186		Q= 25.90 PSF	RN/FT= .606		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
90.75	-9.75	2.5122	-.2407	-.0994	-.0266	.0153	.0290
90.76	-7.79	2.5256	-.2419	-.0851	-.0166	.0133	.0240
90.75	-3.79	2.5197	-.2458	-.0791	-.0132	.0088	.0118
90.74	.17	2.5400	-.2510	-.0795	-.0110	.0008	.0010
90.72	4.16	2.5256	-.2504	-.0789	-.0084	-.0043	-.0107
90.71	8.15	2.5119	-.2412	-.0993	-.0065	-.0140	-.0233
90.71	10.11	2.5137	-.2393	-.0958	-.0005	-.0146	-.0288
90.69	15.06	2.4768	-.2232	-.1143	.0251	-.0092	-.0426
90.68	20.06	2.4350	-.2042	-.1497	.0216	.0012	-.0539
90.65	29.90	2.3410	-.1917	-.1519	-.0492	-.0231	-.0708

RUN 187		Q= 25.70 PSF	RN/FT= .605		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.29	29.91	2.3742	-.1819	-.1193	-.0621	-.0375	-.0672
85.31	20.00	2.4634	-.2002	-.1031	.0314	-.0021	-.0510
85.34	15.05	2.5351	-.2154	-.0717	.0085	-.0192	-.0392
85.34	10.09	2.5460	-.2252	-.0433	.0034	-.0199	-.0261
85.34	8.11	2.5491	-.2254	-.0344	.0013	-.0175	-.0224
85.35	4.11	2.5785	-.2334	-.0285	.0145	-.0043	-.0096
85.34	.20	2.5776	-.2344	-.0286	-.0058	-.0019	.0001
85.36	-3.77	2.5590	-.2344	-.0275	-.0144	.0068	.0104
85.37	-7.74	2.5441	-.2338	-.0390	-.0068	.0180	.0205
85.38	-9.77	2.5431	-.2337	-.0413	-.0132	.0231	.0265

APPENDIX - Continued

RUN 188		Q= 25.40 PSF	RN/FT= .602		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.14	-9.75	2.5478	-.2126	.0805	-.0145	.0239	.0245
80.16	-7.72	2.5834	-.2167	.1005	-.0185	.0203	.0193
80.15	-3.79	2.5868	-.2216	.1369	-.0240	.0065	.0095
80.13	.17	2.5868	-.2206	.1410	-.0296	-.0080	.0005
80.12	4.13	2.5739	-.2137	.1181	-.0516	-.0260	-.0086
80.11	8.16	2.5661	-.2080	.0899	-.0514	-.0355	-.0189
80.10	10.12	2.5480	-.2042	.0725	-.0576	-.0366	-.0227
80.09	15.09	2.5060	-.2003	.0086	-.0034	-.0048	-.0365
80.07	20.07	2.4620	-.1926	-.0144	.0097	.0002	-.0467
80.04	29.91	2.3675	-.1743	-.0319	-.0957	-.0481	-.0624

RUN 189		Q= 25.90 PSF	RN/FT= .608		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
75.10	29.92	2.3607	-.1555	.0321	-.1287	-.0588	-.0587
75.12	20.02	2.5009	-.1685	.0196	-.0122	-.0207	-.0422
75.13	15.07	2.5254	-.1755	.0337	-.0005	-.0181	-.0316
75.14	10.05	2.5805	-.1838	.1006	-.0656	-.0600	-.0203
75.15	8.08	2.5921	-.1873	.1091	-.0680	-.0560	-.0156
75.16	4.14	2.6294	-.1981	.1443	-.0598	-.0442	-.0073
75.17	.18	2.6310	-.2012	.1686	-.0549	-.0324	.0005
75.19	-3.78	2.6362	-.2019	.1823	-.0609	-.0238	.0091
75.19	-7.76	2.6293	-.1961	.1690	-.0338	.0005	.0174
75.19	-9.75	2.6310	-.1942	.1615	-.0404	.0056	.0207

APPENDIX - Continued

RUN 190		Q= 25.00 PSF		RN/FT= .599		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.20	-9.74	2.5910	-.1682	.1311	-.0296	.0156	.0204
70.21	-7.77	2.6061	-.1705	.1394	-.0443	.0143	.0166
70.22	-3.78	2.6514	-.1775	.1940	-.0806	-.0443	.0093
70.20	.18	2.6485	-.1772	.1715	-.0629	-.0367	.0005
70.18	4.17	2.6311	-.1712	.1454	-.0898	-.0631	-.0046
70.17	8.16	2.6100	-.1636	.1102	-.1097	-.0759	-.0134
70.16	10.16	2.5930	-.1568	.0885	-.0941	-.0748	-.0177
70.14	15.05	2.5335	-.1442	.0271	-.0327	-.0370	-.0283
70.15	20.06	2.5092	-.1549	.0752	-.0445	-.0370	-.0382
70.13	29.94	2.4111	-.1385	.1787	-.1826	-.0535	-.0619

RUN 191		Q= 26.00 PSF		RN/FT= .610		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.38	29.94	2.4570	-.1268	.2854	-.2016	-.0648	-.0565
65.39	20.06	2.5101	-.1341	.1337	-.0804	-.0556	-.0340
65.39	15.07	2.5266	-.1546	.1194	-.0583	-.0395	-.0269
65.39	10.13	2.5736	-.1666	.1199	-.0512	-.0518	-.0188
65.40	8.10	2.6095	-.1771	.1455	-.0643	-.0607	-.0145
65.42	4.14	2.6560	-.1845	.1720	-.0575	-.0644	-.0065
65.42	.18	2.6468	-.1790	.1854	-.0575	-.0380	.0003
65.43	-3.79	2.6275	-.1665	.1929	-.0472	-.0077	.0116
65.44	-7.77	2.6005	-.1544	.2088	-.0542	-.0177	.0186
65.44	-9.77	2.5818	-.1471	.1786	-.0438	-.0093	.0215

APPENDIX - Continued

RUN 192		Q= 25.00 PSF		RN/FT= .599		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.57	-9.75	2.5489	-.1335	.2025	-.0785	-.0409	.0300
60.57	-7.79	2.5792	-.1245	.1930	-.0932	-.0467	.0275
60.56	-3.76	2.5694	-.1321	.1564	-.0491	-.0279	.0201
60.55	.18	2.6315	-.1429	.1386	.0297	.0410	-.0044
60.54	4.10	2.6338	-.1451	.1334	-.0085	-.0239	-.0068
60.52	8.13	2.5955	-.1428	.0790	-.0557	-.0587	-.0103
60.55	10.15	2.5792	-.1411	.0899	-.0623	-.0524	-.0156
60.55	15.06	2.5520	-.1335	.1521	-.0281	-.0344	-.0265
60.56	20.06	2.5431	-.1311	.1966	-.0515	-.0529	-.0305
60.55	29.96	2.5244	-.0980	.3336	-.1520	-.0385	-.0631

RUN 193		Q= 25.20 PSF		RN/FT= .603		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
50.84	29.98	2.6010	-.0118	.1228	-.1008	-.0578	-.1086
50.84	20.04	2.6256	-.0230	.0231	.0070	-.0393	-.0581
50.83	15.11	2.6585	-.0409	-.0289	.0292	-.0598	-.0438
50.81	10.11	2.5720	-.0546	-.0207	-.0195	-.0301	-.0378
50.79	8.10	2.4782	-.0457	.0022	-.0035	.0444	-.0330
50.80	4.11	2.4709	-.0512	-.0336	.0624	.0621	-.0206
50.80	.16	2.4853	-.0486	-.1039	.0026	.0031	.0035
50.82	-3.76	2.4788	-.0555	-.0162	-.0703	-.0471	.0206
50.84	-7.79	2.5016	-.0501	.0721	-.0953	-.0577	.0311
50.85	-9.72	2.4975	-.0463	.1134	-.1111	-.0546	.0351

APPENDIX - Continued

RUN 194		Q= 25.20 PSF		RN/FT= .604		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.60	-9.73	2.1826	.0582	-.1090	-.0139	-.0147	.0239
40.59	-7.76	2.1555	.0562	-.1493	.0024	-.0120	.0184
40.57	-3.79	2.1718	.0540	-.2304	-.0004	-.0072	.0151
40.57	.19	2.2075	.0557	-.3024	.0351	.0103	-.0010
40.59	4.19	2.1763	.0587	-.2199	.0181	.0274	-.0045
40.59	8.08	2.1736	.0656	-.1371	.0268	.0375	-.0150
40.59	10.07	2.1710	.0696	-.1133	.0147	.0347	-.0245
40.61	15.03	2.2385	.0599	-.0939	-.0760	.0033	-.0342
40.62	20.06	2.2334	.0571	-.0520	-.1103	-.0287	-.0534
40.60	29.98	2.1552	.0600	.0539	-.2495	-.0285	-.0866

RUN 195		Q= 25.80 PSF		RN/FT= .605		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.69	.17	2.3269	.0553	-.1710	.0193	.0042	-.0004
50.76	.19	2.6137	-.0517	.0494	.0032	.0024	.0033
60.56	.18	2.6805	-.1435	.1867	.0234	.0238	-.0068
70.25	.18	2.6440	-.1674	.0898	-.0261	-.0101	.0015
80.15	.16	2.5767	-.2097	.0139	-.0022	-.0029	.0010
90.69	.17	2.5059	-.2426	-.1846	.0079	.0047	.0007

APPENDIX - Continued

RUN 196		Q= 25.20 PSF		RN/FT= .596		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
90.72	-9.76	2.4865	-.2333	-.2378	.0649	.0721	.0285
90.72	-7.81	2.5141	-.2364	-.2205	.0657	.0591	.0233
90.72	-3.80	2.5064	-.2389	-.1993	.0422	.0329	.0115
90.71	.22	2.5186	-.2429	-.1894	-.0051	.0064	.0010
90.70	4.16	2.5237	-.2404	-.1993	-.1720	-.0341	-.0134
90.69	8.16	2.5086	-.2360	-.2242	-.0535	-.0512	-.0235
90.69	10.14	2.5056	-.2307	-.2393	-.0806	-.0608	-.0286
90.68	15.06	2.4584	-.2183	-.2557	-.1265	-.0853	-.0385
90.66	20.05	2.4218	-.2000	-.2906	-.1600	-.1085	-.0504
90.63	29.94	2.3087	-.1867	-.3173	-.2201	-.1138	-.0700

RUN 197		Q= 25.60 PSF		RN/FT= .601		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.27	29.93	2.3370	-.1734	-.2964	-.2344	-.1328	-.0656
85.29	20.09	2.4497	-.1952	-.2686	-.1822	-.1199	-.0474
85.31	15.03	2.5009	-.2088	-.2170	-.1224	-.0970	-.0360
85.32	10.11	2.5228	-.2180	-.1654	-.0643	-.0713	-.0261
85.32	8.10	2.5305	-.2175	-.1440	-.0572	-.0561	-.0204
85.32	4.17	2.5368	-.2224	-.1383	-.0234	-.0258	-.0095
85.31	.17	2.5383	-.2253	-.1461	.0097	.0032	.0011
85.33	-3.81	2.5387	-.2241	-.1513	.0330	.0359	.0117
85.35	-7.83	2.5182	-.2217	-.1799	.0677	.0665	.0201
85.35	-9.77	2.5119	-.2221	-.1803	.0783	.0780	.0252

APPENDIX - Continued

RUN 198		Q= 25.10 PSF	RN/FT= .597		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.15	-9.77	2.5289	-.2106	-.0963	.0826	.0833	.0235
80.16	-7.74	2.5460	-.2124	-.0664	.0517	.0721	.0195
80.16	-3.83	2.5814	-.2157	.0058	.0211	.0314	.0115
80.15	.15	2.5845	-.2148	.0136	-.0010	-.0004	.0014
80.13	4.21	2.5979	-.2109	-.0236	-.0498	-.0465	-.0079
80.12	8.14	2.5522	-.2040	-.0600	-.1105	-.0775	-.0177
80.12	10.09	2.5488	-.2038	-.0867	-.1173	-.0905	-.0220
80.11	15.03	2.4927	-.1945	-.1575	-.1280	-.1047	-.0338
80.10	20.07	2.4533	-.1819	-.2139	-.1775	-.1223	-.0432
80.08	29.95	2.3404	-.1574	-.2546	-.2496	-.1438	-.0601

RUN 199		Q= 25.20 PSF	RN/FT= .599		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
75.12	29.94	2.3430	-.1383	-.1930	-.2820	-.1491	-.0584
75.14	20.10	2.4669	-.1606	-.1760	-.2442	-.1536	-.0388
75.15	15.09	2.5224	-.1731	-.0986	-.1937	-.1379	-.0280
75.15	10.10	2.5687	-.1845	-.0360	-.1566	-.1104	-.0177
75.15	8.12	2.5744	-.1871	-.0127	-.1283	-.0942	-.0136
75.16	4.17	2.6044	-.1965	.0357	-.0705	-.0514	-.0053
75.17	.16	2.6210	-.2008	.0532	-.0348	-.0199	.0011
75.18	-3.79	2.6270	-.2001	.0768	-.0285	.0047	.0104
75.19	-7.79	2.5953	-.1964	.0743	.0026	.0420	.0183
75.21	-9.73	2.5818	-.1930	.0441	.0229	.0640	.0221

APPENDIX - Continued

RUN 200		Q= 25.50 PSF		RN/FT= .603		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.20	-9.74	2.5749	-.1773	.1169	.0053	.0415	.0209
70.19	-7.78	2.5786	-.1708	.0915	-.0107	.0279	.0173
70.19	-3.75	2.5979	-.1883	.1306	-.0315	-.0087	.0096
70.17	.20	2.6046	-.1721	.0937	-.0355	-.0098	.0009
70.16	4.17	2.6185	-.1671	.0670	-.0916	-.0596	-.0041
70.15	8.14	2.5762	-.1579	.0228	-.1414	-.1019	-.0111
70.14	10.11	2.5557	-.1533	.0005	-.1698	-.1162	-.0142
70.14	15.12	2.5081	-.1484	-.0681	-.2011	-.1458	-.0266
70.11	20.06	2.4166	-.1369	-.1108	-.2649	-.1597	-.0349
70.09	29.95	2.3463	-.1205	-.0401	-.3172	-.1302	-.0608

RUN 201		Q= 25.00 PSF		RN/FT= .598		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.35	29.94	2.4044	-.1119	.0789	-.3243	-.1349	-.0582
65.36	20.04	2.4630	-.1132	.0076	-.2024	-.1246	-.0318
65.36	15.08	2.5352	-.1172	.0072	-.1868	-.1281	-.0235
65.37	10.12	2.6019	-.1295	.0413	-.1285	-.1097	-.0134
65.38	8.17	2.6166	-.1362	.0492	-.1215	-.0971	-.0107
65.39	4.15	2.6225	-.1741	.1488	-.0580	-.0455	-.0056
65.41	.16	2.6436	-.1634	.1727	-.0082	.0202	-.0008
65.43	-3.76	2.6529	-.1737	.1930	-.0826	-.0409	.0142
65.44	-7.75	2.6126	-.1499	.1954	-.0362	.0007	.0196
65.45	-9.76	2.6158	-.1489	.1703	-.0087	.0171	.0226

APPENDIX - Continued

RUN 202		Q= 24.80 PSF		RN/FT= .597		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
60.58	-9.75	2.6633	-.1561	.3253	-.0497	-.0125	.0209
60.57	-7.70	2.6029	-.1337	.2494	-.0292	-.0147	.0231
60.56	-3.72	2.6505	-.1403	.1903	-.0889	-.0486	.0224
60.55	.20	2.6822	-.1475	.1768	.0202	.0252	-.0050
60.53	4.16	2.6600	-.1428	.1800	.0018	.0102	-.0132
60.53	8.17	2.6642	-.1416	.2154	-.0345	-.0615	-.0165
60.53	10.12	2.6650	-.1355	.2200	-.0454	-.0727	-.0191
60.50	15.09	2.5455	-.0895	.0933	-.1484	-.1001	-.0220
60.49	20.05	2.4709	-.0853	.0420	-.2101	-.1196	-.0282
60.48	29.95	2.4683	-.0819	.1354	-.2995	-.1222	-.0759

RUN 203		Q= 24.70 PSF		RN/FT= .596		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
50.85	29.97	2.6736	-.0264	.0283	-.2693	-.1440	-.1133
50.87	19.97	2.7572	-.0459	.0911	-.0960	-.1007	-.0624
50.86	15.06	2.6897	-.0591	.1254	-.1161	-.0678	-.0535
50.84	10.13	2.6346	-.0567	.1273	.0358	.0067	-.0361
50.82	8.12	2.5562	-.0563	.1326	.0238	.0648	-.0317
50.83	4.09	2.5385	-.0582	.1348	.1002	.0698	-.0204
50.85	.21	2.6197	-.0568	.0480	.0020	.0031	.0021
50.86	-3.78	2.5709	-.0626	.1324	-.0958	-.0666	.0243
50.86	-7.75	2.5059	-.0615	.1513	-.0310	-.0603	.0390
50.87	-9.74	2.5120	-.0538	.1476	.0101	-.0426	.0405

APPENDIX - Continued

RUN 204		Q= 24.20 PSF	RN/FT= .591		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.60	-9.73	2.2012	.0497	-.0864	.0498	-.0341	.0254
40.61	-7.69	2.2493	.0512	-.0751	-.0003	-.0307	.0155
40.61	-3.78	2.2825	.0505	-.1051	-.0687	-.0187	.0226
40.61	.22	2.3287	.0526	-.1749	.0245	.0046	-.0024
40.58	4.11	2.2500	.0557	-.0972	.0680	.0279	-.0053
40.57	8.13	2.2576	.0568	-.0881	-.0308	.0450	-.0104
40.55	10.18	2.2228	.0577	-.0937	-.0713	.0454	-.0239
40.55	15.09	2.2089	.0452	-.0660	-.1336	.0134	-.0354
40.59	20.05	2.2599	.0426	-.0788	-.2155	-.0476	-.0557
40.64	29.98	2.4191	.0547	-.1769	-.3440	-.0911	-.0956

RUN 205		Q= 25.50 PSF	RN/FT= .604		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.57	.20	2.1458	.0488	-.3624	.0196	.0065	.0010
50.78	.19	2.4016	-.0667	-.3049	-.0150	.0418	-.0052
60.48	.17	2.4529	-.1320	-.2277	.0473	.0276	-.0013
65.29	.17	2.4794	-.1246	-.2491	.0579	.0542	-.0044
70.18	.17	2.4910	-.1702	-.2214	.0796	.0739	-.0043
75.10	.17	2.5164	-.2110	-.1177	.0377	.0338	-.0001
80.14	.18	2.5146	-.2298	-.1266	-.0402	-.0167	.0024
85.30	.17	2.4820	-.2377	-.1539	-.0183	.0013	-.0002
90.65	.17	2.4312	-.2462	-.3043	-.0059	.0019	.0007

APPENDIX - Continued

RUN 206		Q= 25.10 PSF		RN/FT= .600		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
90.64	-9.72	2.3976	-.2358	-.3620	-.0237	.0043	.0293
90.65	-7.76	2.4045	-.2365	-.3640	-.0347	.0020	.0237
90.65	-3.77	2.4362	-.2430	-.3104	-.0135	.0077	.0124
90.63	.16	2.4363	-.2453	-.2950	-.0086	.0025	.0009
90.63	4.13	2.4354	-.2432	-.3067	-.0015	-.0013	-.0131
90.62	8.10	2.4254	-.2399	-.3409	.0434	.0142	-.0248
90.62	10.11	2.4304	-.2345	-.3436	.0473	.0115	-.0299
90.60	15.04	2.4053	-.2192	-.3372	.0164	-.0033	-.0417
90.62	20.02	2.3724	-.2005	-.3475	-.0291	-.0306	-.0514
90.61	29.90	2.2452	-.1849	-.3631	-.1489	-.0756	-.0698

RUN 207		Q= 25.40 PSF		RN/FT= .605		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.30	29.90	2.3011	-.1784	-.3438	-.1731	-.0966	-.0655
85.31	20.00	2.4097	-.1977	-.2967	-.0454	-.0462	-.0486
85.33	15.03	2.4327	-.2150	-.2686	.0125	-.0121	-.0393
85.33	10.10	2.4409	-.2232	-.2530	.0439	.0157	-.0284
85.33	8.11	2.4459	-.2247	-.2652	.0498	.0214	-.0231
85.34	4.14	2.4635	-.2287	-.2602	.0414	.0219	-.0113
85.35	.16	2.4976	-.2372	-.1578	-.0017	.0019	.0007
85.36	-3.80	2.4712	-.2288	-.2564	-.0363	-.0214	.0128
85.34	-7.80	2.4415	-.2249	-.3333	-.0393	.0005	.0232
85.29	-9.74	2.4331	-.2232	-.3275	-.0196	.0095	.0269

APPENDIX - Continued

RUN 208 Q= 25.00 PSF RN/FT= .602 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.12	-9.72	2.4953	-.2227	-.1829	-.0245	.0189	.0258
80.13	-7.76	2.4971	-.2231	-.1624	-.0309	.0031	.0209
80.12	-3.80	2.5249	-.2290	-.1491	-.0423	-.0108	.0115
80.11	.19	2.5146	-.2311	-.1270	-.0234	-.0177	.0018
80.10	4.14	2.5052	-.2250	-.1563	-.0025	-.0035	-.0086
80.11	8.12	2.5092	-.2199	-.1731	.0177	-.0068	-.0179
80.15	10.10	2.4983	-.2171	-.1736	.0104	-.0115	-.0229
80.14	15.03	2.4663	-.2097	-.2051	-.0349	-.0444	-.0345
80.13	20.03	2.4170	-.1900	-.2545	-.0760	-.0600	-.0444
80.10	29.92	2.3052	-.1649	-.2907	-.1931	-.1081	-.0605

RUN 209 Q= 25.00 PSF RN/FT= .602 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
75.12	29.92	2.3222	-.1569	-.2060	-.2317	-.1270	-.0556
75.14	20.03	2.4398	-.1737	-.1872	-.0956	-.0829	-.0390
75.11	15.06	2.4891	-.1860	-.1631	-.0559	-.0606	-.0298
75.10	10.11	2.5268	-.1971	-.1697	-.0259	-.0322	-.0200
75.11	8.11	2.5324	-.2005	-.1749	-.0061	-.0260	-.0142
75.11	4.17	2.5396	-.2069	-.1716	-.0005	-.0198	-.0058
75.13	.18	2.5531	-.2128	-.1265	.0619	.0157	.0011
75.14	-3.79	2.5543	-.2072	-.1548	-.0803	-.0315	.0119
75.17	-7.75	2.5536	-.2023	-.1513	-.0541	-.0021	.0194
75.17	-9.75	2.5060	-.1982	-.1401	-.0459	.0119	.0234

APPENDIX - Continued

RUN 210		Q= 24.80 PSF		RN/FT= .601		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.18	-9.74	2.5028	-.1655	-.1181	-.0734	-.0088	.0215
70.18	-7.77	2.5273	-.1715	-.1290	-.0965	-.0261	.0180
70.17	-3.78	2.5212	-.1784	-.1605	-.0791	-.0247	.0106
70.15	.16	2.4860	-.1725	-.2105	.0921	.0747	-.0038
70.13	4.12	2.5098	-.1695	-.1563	.0960	.0642	-.0103
70.15	8.10	2.5203	-.1669	-.1568	.0338	.0060	-.0146
70.15	10.11	2.4928	-.1615	-.2057	-.0569	-.0591	-.0152
70.15	15.07	2.4736	-.1591	-.2027	-.1025	-.0861	-.0255
70.14	20.05	2.4272	-.1465	-.1759	-.1253	-.0881	-.0359
70.12	29.95	2.3451	-.1284	-.1085	-.2686	-.1081	-.0596

RUN 211		Q= 24.10 PSF		RN/FT= .593		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.32	29.95	2.3355	-.1049	-.0090	-.2564	-.0867	-.0559
65.31	20.08	2.4468	-.1275	-.0765	-.2350	-.0936	-.0351
65.30	15.05	2.4814	-.1295	-.0361	-.0058	-.0214	-.0257
65.31	10.07	2.5244	-.1377	-.0487	.0748	.0208	-.0184
65.31	8.10	2.5237	-.1371	-.0875	.0989	.0391	-.0155
65.32	4.12	2.5100	-.1319	-.1054	-.0027	.0746	-.0136
65.31	.15	2.4514	-.1285	-.2453	.0666	.0561	-.0039
65.35	-3.79	2.4984	-.1782	-.0974	-.0679	-.0344	.0126
65.38	-7.72	2.5529	-.1515	-.0017	-.1646	-.0574	.0180
65.37	-9.75	2.5139	-.1455	-.0296	-.1334	-.0374	.0200

APPENDIX - Continued

RUN 212		Q= 25.30 PSF		RN/FT= .610		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
60.50	-9.74	2.5058	-.1257	.0794	-.1357	-.0528	.0210
60.50	-7.75	2.5337	-.1213	.0475	-.1631	-.0572	.0162
60.49	-3.78	2.4812	-.1497	-.0997	-.0976	-.0354	.0093
60.48	.14	2.4158	-.1326	-.2121	.0141	.0239	-.0043
60.48	4.13	2.4684	-.1371	-.1387	.0640	.0528	-.0146
60.49	8.08	2.5034	-.1324	.0633	.1206	.0867	-.0189
60.48	10.05	2.4865	-.1141	.0221	.0902	.0637	-.0201
60.51	15.07	2.5497	-.1461	.0667	.0008	-.0200	-.0273
60.52	20.05	2.5315	-.1319	.0563	-.1028	-.0736	-.0371
60.48	29.93	2.4129	-.0940	.0456	-.2926	-.1055	-.0712

RUN 213		Q= 24.10 PSF		RN/FT= .596		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
50.80	29.94	2.5830	-.0206	-.1421	-.2364	-.1172	-.1110
50.83	20.07	2.6733	-.0371	-.1212	-.1265	-.1023	-.0641
50.83	15.10	2.6705	-.0430	-.1257	-.0291	-.0914	-.0462
50.78	10.09	2.4501	-.0451	-.0180	.0385	.0574	-.0360
50.78	8.10	2.4453	-.0487	-.0135	.0864	.0802	-.0345
50.78	4.11	2.4373	-.0611	-.1617	.0900	.0768	-.0209
50.78	.14	2.4041	-.0728	-.3054	-.0106	.0401	-.0040
50.79	-3.79	2.4445	-.0651	-.1779	-.1226	-.0408	.0151
50.78	-7.72	2.4630	-.0338	-.0360	-.1404	-.0507	.0252
50.79	-9.74	2.5015	-.0514	.0387	-.0922	-.0676	.0373

APPENDIX - Continued

RUN 214		Q= 25.70 PSF		RN/FT= .616		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.64	-9.72	2.2081	.0583	-.1577	-.1159	-.0290	.0277
40.63	-7.74	2.2242	.0526	-.2144	-.1000	-.0248	.0299
40.58	-3.77	2.1652	.0428	-.3166	.0012	-.0104	.0109
40.58	.16	2.1934	.0461	-.3755	.0183	.0069	.0007
40.61	4.13	2.1485	.0462	-.3338	-.0418	.0152	.0058
40.64	8.09	2.2528	.0640	-.2156	.1202	.0152	-.0269
40.63	10.07	2.2096	.0659	-.1488	.1229	.0263	-.0267
40.64	15.10	2.2746	.0446	-.2928	-.1809	-.0625	-.0441
40.65	20.01	2.2907	.0575	-.2904	-.1596	-.0632	-.0641
40.64	29.97	2.2688	.0596	-.2596	-.2757	-.0645	-.1040

RUN 215		Q= 25.20 PSF		RN/FT= .612		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.50	.21	2.2243	.0442	-.3549	-.1379	-.0118	.0171
50.70	.18	2.5294	-.0728	-.1914	-.0504	-.0955	-.0080
60.45	.17	2.5279	-.1244	-.1145	-.0899	-.0350	.0064
70.06	.16	2.5332	-.1753	-.1767	-.0313	-.0135	.0013
79.98	.16	2.5007	-.2337	-.2872	-.0126	.0017	.0003
90.46	.16	2.3970	-.2573	-.5260	-.0119	.0034	.0015

APPENDIX - Continued

RUN 216 Q= 24.70 PSF RN/FT= .607 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
90.50	-9.72	2.3690	-.2471	-.5711	.0690	.0895	.0257
90.52	-7.77	2.3906	-.2480	-.5547	.0418	.0739	.0219
90.50	-3.81	2.4047	-.2553	-.5261	.0234	.0392	.0123
90.49	.18	2.4191	-.2593	-.5123	-.0009	.0035	-.0003
90.48	4.14	2.4110	-.2578	-.5264	-.0477	-.0308	-.0103
90.48	8.12	2.3916	-.2504	-.5413	-.0911	-.0630	-.0193
90.47	10.11	2.3753	-.2443	-.5618	-.1139	-.0782	-.0238
90.47	15.05	2.3505	-.2345	-.5984	-.1854	-.1215	-.0337
90.47	20.00	2.2865	-.2227	-.6749	-.2899	-.1713	-.0429
90.45	29.94	2.1409	-.2181	-.8719	-.4318	-.2396	-.0596

RUN 217 Q= 24.70 PSF RN/FT= .607 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.18	29.95	2.1451	-.1997	-.8401	-.4480	-.2571	-.0561
85.21	20.02	2.3266	-.2155	-.6298	-.3123	-.1898	-.0397
85.22	15.06	2.4072	-.2263	-.5093	-.1936	-.1341	-.0312
85.23	10.12	2.4282	-.2387	-.4538	-.1272	-.0878	-.0207
85.23	8.09	2.4401	-.2377	-.4484	-.0926	-.0736	-.0185
85.23	4.12	2.4643	-.2410	-.4181	-.0541	-.0363	-.0068
85.23	.12	2.4537	-.2374	-.4377	-.0073	.0034	.0013
85.24	-3.77	2.4318	-.2340	-.4457	.0307	.0415	.0111
85.26	-7.75	2.4203	-.2351	-.4562	.0697	.0785	.0188
85.26	-9.75	2.4050	-.2385	-.4640	.0858	.0959	.0240

APPENDIX - Continued

RUN 218 Q= 24.10 PSF RN/FT= .600 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.00	-9.75	2.4687	-.2354	-.3423	.0909	.1025	.0204
80.00	-7.77	2.4767	-.2278	-.3250	.0734	.0818	.0167
79.99	-3.81	2.5069	-.2361	-.2854	.0366	.0429	.0091
79.99	.19	2.5019	-.2353	-.2850	-.0135	.0018	.0014
79.99	4.16	2.5051	-.2293	-.3300	-.0600	-.0456	-.0065
79.97	8.10	2.4506	-.2187	-.3576	-.1022	-.0824	-.0141
79.97	10.09	2.4362	-.2306	-.3742	-.1420	-.1005	-.0189
79.96	15.07	2.3908	-.2200	-.4375	-.2216	-.1446	-.0270
79.94	20.03	2.3172	-.2048	-.5843	-.3312	-.1984	-.0363
79.96	29.93	2.1397	-.1772	-.8389	-.4897	-.2695	-.0526

RUN 219 Q= 24.70 PSF RN/FT= .609 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
74.98	20.05	2.3303	-.1779	-.5142	-.3270	-.1894	-.0327
75.00	15.10	2.4240	-.1909	-.3679	-.2135	-.1403	-.0249
74.97	10.11	2.4615	-.1960	-.3298	-.1245	-.0785	-.0182
74.97	8.12	2.4841	-.2023	-.3298	-.1226	-.0923	-.0109
74.98	4.17	2.4972	-.2004	-.2915	-.0678	-.0463	-.0048
74.99	.18	2.5057	-.2033	-.2602	-.0182	-.0021	.0011
75.01	-3.82	2.5105	-.2068	-.2608	.0179	.0422	.0065
74.99	-7.76	2.5084	-.2121	-.2771	.0524	.0843	.0137
75.00	-9.78	2.4955	-.2123	-.3024	.0697	.1058	.0170

APPENDIX - Continued

RUN 220 Q= 24.20 PSF RN/FT= .603 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.06	-9.77	2.4897	-.1782	-.2578	.0718	.0990	.0148
70.06	-7.77	2.5197	-.1831	-.2342	.0473	.0783	.0114
70.06	-3.82	2.5379	-.1821	-.1825	.0040	.0308	.0056
70.05	.15	2.5427	-.1781	-.1775	-.0267	-.0138	.0013
70.03	4.13	2.5528	-.1810	-.1918	-.0498	-.0442	-.0026
70.04	8.12	2.5068	-.1703	-.3157	-.1001	-.0900	-.0067
70.03	10.10	2.4758	-.1654	-.2984	-.0803	-.0683	-.0150
70.07	15.05	2.4655	-.1624	-.3204	-.1904	-.1374	-.0227
70.06	20.05	2.3604	-.1497	-.4113	-.2769	-.1746	-.0306
70.02	29.92	2.1437	-.1219	-.6716	-.5002	-.2386	-.0525

RUN 221 Q= 25.00 PSF RN/FT= .613 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.20	29.94	2.1944	-.1044	-.4503	-.4469	-.1980	-.0501
65.25	20.06	2.3986	-.1299	-.3109	-.2513	-.1568	-.0255
65.24	15.04	2.4692	-.1303	-.2879	-.1599	-.1218	-.0197
65.25	10.12	2.5358	-.1315	-.1991	-.0930	-.0797	-.0135
65.24	8.11	2.5045	-.1679	-.2324	-.0899	-.0503	-.0135
65.26	4.14	2.5556	-.1432	-.1591	-.0639	-.0522	.0003
65.28	.19	2.5894	-.1437	-.0779	-.0163	-.0065	.0032
65.22	-3.80	2.5364	-.1368	-.1626	-.0029	.0240	.0056
65.23	-7.78	2.5150	-.1347	-.1962	.0263	.0691	.0099
65.24	-9.78	2.4902	-.1340	-.2146	.0417	.0876	.0122

APPENDIX - Continued

RUN 222		Q= 25.80 PSF		RN/FT= .623		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.45	-9.77	2.5175	-.1169	-.1237	.0857	.0877	.0144
60.45	-7.78	2.5499	-.1275	-.0932	.0382	.0644	.0126
60.45	-3.80	2.5627	-.1360	-.0712	-.0399	.0016	.0101
60.43	.20	2.5381	-.1294	-.1041	-.0882	-.0374	.0063
60.41	4.14	2.5031	-.1169	-.1908	-.1083	-.0758	.0016
60.41	8.12	2.4980	-.1444	-.1714	-.0588	-.0360	-.0047
60.39	10.09	2.4824	-.1116	-.1813	-.0119	-.0258	-.0166
60.40	15.05	2.4694	-.0991	-.2013	-.1786	-.1154	-.0192
60.41	20.06	2.4242	-.1279	-.2153	-.2702	-.1558	-.0245
60.38	29.96	2.2502	-.1148	-.2267	-.4099	-.1756	-.0496

RUN 223		Q= 27.90 PSF		RN/FT= .648		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
50.80	29.99	2.4522	-.0329	-.3632	-.4036	-.2151	-.1013
50.84	20.07	2.6850	-.0419	-.2250	-.2409	-.1560	-.0585
50.83	15.11	2.6707	-.0626	-.1395	-.0686	-.1050	-.0447
50.75	10.09	2.3880	-.0598	-.1299	-.0397	.0249	-.0348
50.76	8.11	2.4310	-.0569	-.1375	.0851	.0344	-.0264
50.77	4.14	2.4009	-.0760	-.1907	-.2244	-.0621	-.0198
50.79	.18	2.5104	-.0746	-.1925	-.0631	-.0980	-.0063
50.79	-3.79	2.4368	-.0677	-.1558	-.0630	-.0757	.0275
50.79	-7.75	2.3861	-.0702	-.0980	.0229	-.0243	.0302
50.80	-9.70	2.3891	-.0744	-.0909	.0737	.0063	.0304

APPENDIX - Continued

RUN 224		Q= 25.90 PSF		RN/FT= .626		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.46	-9.70	2.0758	.0383	-.2904	.0711	-.0079	.0240
40.47	-7.75	2.1163	.0409	-.2790	-.0027	-.0209	.0133
40.46	-3.77	2.1513	.0415	-.2794	-.1283	-.0281	.0076
40.46	.16	2.1883	.0418	-.3559	-.1450	-.0108	.0159
40.46	4.16	2.2030	.0460	-.3419	.0676	-.0039	-.0168
40.44	8.10	2.1451	.0467	-.2736	.0565	.0123	-.0167
40.42	10.12	2.0898	.0478	-.2903	-.0523	.0074	-.0189
40.45	15.06	2.1754	.0323	-.2842	-.2257	-.0511	-.0365
40.49	20.07	2.3178	.0502	-.3891	-.2748	-.1188	-.0555
40.48	30.01	2.2332	.0504	-.4401	-.4428	-.1314	-.0778

RUN 225		Q= 91.40 PSF		RN/FT= 2.218		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.91	.25	2.2303	.0373	-.4206	-.0249	-.0113	.0011
51.14	.23	2.4208	-.0855	-.3746	-.0052	-.0196	.0069
60.89	.21	2.5002	-.1742	-.3342	.0029	.0067	-.0031
70.57	.19	2.4871	-.2234	-.3813	.0232	.0159	-.0001
80.54	.21	2.4829	-.2616	-.4310	.0041	.0069	.0013
91.05	.20	2.4133	-.2760	-.5364	.0033	-.0013	.0015

APPENDIX - Continued

RUN 226		Q= 93.60 PSF		RN/FT= 2.231		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
91.03	-9.75	2.3995	-.2677	-.5643	.0471	.0606	.0279
91.00	-7.72	2.4028	-.2717	-.5501	.0393	.0508	.0232
91.00	-3.77	2.3991	-.2695	-.5432	.0205	.0244	.0123
90.98	.19	2.4202	-.2795	-.5374	-.0058	-.0005	.0016
90.97	4.18	2.3978	-.2641	-.5390	-.0123	-.0257	-.0107
90.96	8.15	2.4058	-.2705	-.5521	-.0567	-.0514	-.0207
90.96	10.10	2.4145	-.2716	-.5713	-.0703	-.0651	-.0276
90.97	15.04	2.3625	-.2616	-.5951	-.1317	-.0928	-.0373
90.94	20.01	2.3053	-.2443	-.6498	-.1835	-.1145	-.0483
90.95	29.93	2.2119	-.2462	-.6887	-.2599	-.1487	-.0675

RUN 227		Q= 94.20 PSF		RN/FT= 2.230		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.64	29.95	2.2362	-.2290	-.6680	-.2790	-.1596	-.0636
85.62	20.02	2.3083	-.2353	-.6047	-.1778	-.1088	-.0454
85.64	15.09	2.3710	-.2499	-.5612	-.1379	-.1024	-.0354
85.65	10.10	2.4065	-.2555	-.5214	-.0837	-.0704	-.0256
85.65	8.15	2.4019	-.2559	-.5077	-.0677	-.0576	-.0199
85.67	4.16	2.4195	-.2596	-.4818	-.0277	-.0315	-.0091
85.63	.16	2.4275	-.2685	-.4606	-.0065	-.0060	.0018
85.63	-3.80	2.4211	-.2624	-.4827	.0188	.0281	.0115
85.64	-7.77	2.4135	-.2608	-.5080	.0475	.0555	.0209
85.64	-9.75	2.4017	-.2593	-.5158	.0481	.0687	.0271

APPENDIX - Continued

RUN 228		Q= 91.40 PSF		RN/FT= 2.191		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
80.45	-9.75	2.4505	-.2497	-.4687	.0496	.0564	.0246
80.44	-7.74	2.4162	-.2488	-.4579	.0358	.0446	.0186
80.43	-3.79	2.4493	-.2526	-.4576	.0048	.0201	.0107
80.43	.16	2.4644	-.2578	-.4331	.0017	.0109	.0011
80.43	4.17	2.4741	-.2534	-.4177	-.0241	-.0262	-.0097
80.42	8.11	2.4637	-.2470	-.4484	-.0684	-.0585	-.0176
80.48	10.11	2.4381	-.2408	-.4686	-.0881	-.0756	-.0228
80.45	15.09	2.3934	-.2341	-.5167	-.1366	-.1004	-.0332
80.43	20.08	2.3437	-.2205	-.5706	-.1788	-.1123	-.0431
80.40	29.94	2.2695	-.2001	-.5485	-.1650	-.0869	-.0621

RUN 229		Q= 92.50 PSF		RN/FT= 2.199		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
75.44	29.95	2.2754	-.1713	-.4871	-.1624	-.0855	-.0576
75.47	20.06	2.3499	-.1908	-.5366	-.1794	-.1075	-.0402
75.49	15.08	2.3927	-.2055	-.4896	-.1100	-.0833	-.0316
75.52	10.14	2.4467	-.2245	-.4007	-.0398	-.0444	-.0207
75.53	8.13	2.4906	-.2292	-.4040	-.0264	-.0315	-.0170
75.53	4.14	2.4671	-.2307	-.4040	.0139	-.0012	-.0081
75.53	.13	2.4660	-.2354	-.4268	.0035	.0028	.0016
75.55	-3.77	2.4829	-.2369	-.4415	.0116	.0252	.0095
75.57	-7.75	2.4634	-.2334	-.4447	.0276	.0414	.0166
75.58	-9.73	2.4474	-.2284	-.4355	.0369	.0506	.0211

APPENDIX - Continued

RUN 230		Q= 92.40 PSF		RN/FT= 2.191		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.54	-9.72	2.4615	-.1969	-.4057	.0046	.0350	.0181
70.52	-7.78	2.4670	-.1976	-.4187	.0054	.0330	.0142
70.52	-3.83	2.4837	-.1985	-.4180	.0031	.0179	.0079
70.52	.14	2.4847	-.2224	-.3880	.0166	.0162	.0002
70.49	4.13	2.4970	-.1958	-.4163	.0175	-.0003	-.0062
70.49	8.14	2.4970	-.1889	-.4064	.0157	-.0176	-.0142
70.50	10.12	2.4813	-.1865	-.3928	.0155	-.0246	-.0179
70.49	15.10	2.4259	-.1772	-.3855	-.0586	-.0592	-.0266
70.45	20.04	2.3787	-.1688	-.4107	-.1021	-.0560	-.0372
70.38	29.97	2.2337	-.1450	-.4537	-.2011	-.0848	-.0549

RUN 231		Q= 90.50 PSF		RN/FT= 2.166		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.69	29.98	2.2384	-.1173	-.3635	-.2010	-.0673	-.0538
65.69	22.11	2.3321	-.1316	-.3631	-.0837	-.0401	-.0372
65.74	15.10	2.4451	-.1420	-.3686	-.0311	-.0405	-.0271
65.78	10.08	2.4639	-.1490	-.3855	.0290	-.0217	-.0166
65.80	4.16	2.4737	-.1512	-.3549	.0387	.0088	-.0082
65.82	.14	2.4871	-.1919	-.3401	.0198	.0114	-.0020
65.82	-3.79	2.4924	-.1521	-.3619	-.0696	-.0258	.0098
65.84	-7.80	2.4854	-.1530	-.3562	-.0640	-.0010	.0156
65.85	-9.77	2.4689	-.1524	-.3592	-.0411	.0160	.0186

APPENDIX - Continued

RUN 232		Q= 92.00 PSF		RN/FT= 2.179		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.87	-9.75	2.4606	-.1130	-.3532	-.0341	.0079	.0176
60.87	-7.70	2.4621	-.1163	-.3477	-.0835	-.0195	.0150
60.88	-3.77	2.4794	-.1613	-.2610	-.1052	-.0522	.0111
60.88	.19	2.4792	-.1717	-.3346	-.0055	.0076	-.0039
60.86	4.08	2.4665	-.1569	-.2581	.1141	.0592	-.0091
60.84	8.08	2.4712	-.1398	-.3298	.0806	.0258	-.0135
60.82	10.10	2.4309	-.1182	-.3556	.0302	-.0055	-.0158
60.80	15.07	2.3652	-.1027	-.3462	-.0624	-.0360	-.0238
60.78	20.10	2.3352	-.1011	-.3438	-.1228	-.0601	-.0308
60.80	30.01	2.3133	-.1012	-.2952	-.2329	-.0677	-.0725

RUN 233		Q= 89.60 PSF		RN/FT= 2.148		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
51.26	29.96	2.5641	-.0579	-.0499	-.0506	-.0069	-.1015
51.24	20.02	2.5743	-.0562	-.2829	.0421	-.0194	-.0431
51.22	15.01	2.5389	-.0557	-.2919	.1007	.0039	-.0408
51.20	10.09	2.4834	-.0599	-.3246	.1641	.0233	-.0255
51.20	8.06	2.4556	-.0716	-.3068	.1454	.0348	-.0127
51.18	4.15	2.3629	-.0643	-.3308	-.0087	.0543	-.0261
51.21	.15	2.4162	-.0870	-.3769	-.0023	-.0225	.0087
51.20	-3.75	2.3735	-.0671	-.3286	-.0068	-.0540	.0279
51.23	-7.74	2.4423	-.0705	-.3074	-.1545	-.0374	.0162
51.25	-9.68	2.4609	-.0644	-.3071	-.1557	-.0284	.0247

APPENDIX - Continued

RUN 234		Q= 91.20 PSF		RN/FT= 2.164		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.83	-9.69	2.1150	.0396	-.3802	.0505	-.0337	.0246
40.83	-7.73	2.1185	.0410	-.3901	.0785	-.0351	.0200
40.85	-3.75	2.1850	.0400	-.4194	.0389	-.0358	.0082
40.87	.18	2.2028	.0395	-.4198	-.0297	-.0150	.0021
40.84	4.18	2.1960	.0401	-.4255	-.0407	.0219	-.0011
40.81	8.10	2.1520	.0456	-.4030	-.0690	.0361	-.0197
40.80	10.08	2.1155	.0436	-.3775	-.0798	.0316	-.0245
40.80	15.11	2.1004	.0339	-.3199	-.1246	.0141	-.0328
40.84	20.07	2.1676	.0224	-.2391	-.1097	-.0033	-.0407
40.87	29.95	2.1637	.0376	.0212	-.1301	.0118	-.0776

RUN 235		Q= 93.20 PSF		RN/FT= 2.214		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.92	.19	2.2134	.0433	-.3945	-.0305	.0148	.0007
51.16	.20	2.4082	-.0673	-.3554	.0193	-.0080	.0076
60.95	.18	2.4323	-.1471	-.3089	-.0139	-.0076	.0000
70.59	.17	2.4792	-.1796	-.3935	-.0020	.0007	.0009
80.57	.17	2.4877	-.2467	-.4242	-.0041	.0013	.0005
91.06	.17	2.4124	-.2727	-.4957	-.0098	.0026	.0019

APPENDIX - Continued

RUN 236 Q= 97.80 PSF RN/FT= 2.259 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
91.06	-9.75	2.3920	-.2614	-.5295	.0527	.0669	.0272
91.05	-7.75	2.4045	-.2631	-.5192	.0442	.0582	.0226
91.01	-3.80	2.4220	-.2655	-.5121	.0135	.0291	.0120
90.99	.21	2.4258	-.2741	-.4919	-.0078	.0046	.0014
90.98	4.13	2.4080	-.2605	-.4926	-.0288	-.0266	-.0116
90.97	8.14	2.4006	-.2656	-.5184	-.0658	-.0561	-.0211
90.97	10.11	2.4006	-.2646	-.5232	-.0876	-.0676	-.0254
91.02	15.03	2.3803	-.2590	-.5610	-.1325	-.0970	-.0374
90.99	20.01	2.3170	-.2448	-.6027	-.1662	-.1030	-.0485
90.95	29.94	2.2484	-.2420	-.5919	-.1343	-.0695	-.0703

RUN 237 Q= 95.80 PSF RN/FT= 2.233 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.64	29.96	2.2633	-.2238	-.5536	-.1434	-.0788	-.0656
85.67	20.01	2.3458	-.2346	-.5570	-.1815	-.1074	-.0462
85.63	15.07	2.4060	-.2496	-.5031	-.1361	-.0966	-.0364
85.63	10.13	2.4231	-.2535	-.4665	-.0958	-.0708	-.0246
85.63	8.10	2.4145	-.2536	-.4535	-.0713	-.0561	-.0206
85.64	4.16	2.4549	-.2586	-.4319	-.0332	-.0306	-.0091
85.65	.16	2.4402	-.2607	-.4249	-.0004	.0000	.0007
85.66	-3.80	2.4689	-.2627	-.4409	.0316	.0318	.0114
85.69	-7.76	2.4464	-.2616	-.4503	.0527	.0648	.0211
85.69	-9.77	2.4213	-.2557	-.4649	.0614	.0777	.0251

APPENDIX - Continued

RUN 238		Q= 96.60 PSF		RN/FT= 2.239		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
80.47	-9.77	2.4343	-.2348	-.4519	.0691	.0800	.0228
80.47	-7.77	2.4621	-.2375	-.4433	.0526	.0673	.0185
80.45	-3.79	2.4797	-.2425	-.4301	.0173	.0350	.0097
80.45	.17	2.4640	-.2454	-.4252	-.0122	.0021	.0008
80.48	4.13	2.4862	-.2406	-.4199	-.0365	-.0327	-.0103
80.47	8.15	2.4507	-.2344	-.4388	-.0807	-.0610	-.0179
80.51	15.09	2.3942	-.2245	-.4913	-.1500	-.1003	-.0326
80.47	20.07	2.3542	-.2158	-.5319	-.1906	-.1110	-.0440
80.45	29.93	2.2848	-.1928	-.5382	-.1591	-.0846	-.0623
80.51	10.11	2.4436	-.2330	-.4597	-.1005	-.0762	-.0221

RUN 239		Q= 95.70 PSF		RN/FT= 2.223		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
75.44	29.93	2.2622	-.1609	-.5505	-.1863	-.0956	-.0577
75.47	20.04	2.3439	-.1795	-.5525	-.2003	-.1128	-.0398
75.45	15.06	2.3970	-.1933	-.5036	-.1559	-.1060	-.0304
75.47	10.12	2.4604	-.2070	-.4630	-.0977	-.0790	-.0196
75.48	8.13	2.4554	-.2072	-.4435	-.0721	-.0604	-.0153
75.49	4.13	2.4803	-.2142	-.4243	-.0323	-.0325	-.0068
75.49	.15	2.4846	-.2168	-.4208	-.0036	.0001	.0009
75.50	-3.81	2.4677	-.2156	-.4245	.0178	.0338	.0085
75.51	-7.79	2.4612	-.2108	-.4510	.0578	.0686	.0156
75.52	-9.80	2.4395	-.2081	-.4616	.0711	.0845	.0202

APPENDIX - Continued

RUN 240		Q= 94.70 PSF		RN/FT= 2.207		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.58	-9.80	2.4507	-.1760	-.4340	.0570	.0813	.0164
70.57	-7.79	2.4643	-.1782	-.4218	.0375	.0676	.0132
70.56	-3.80	2.4855	-.1815	-.4021	.0122	.0324	.0061
70.56	.17	2.4708	-.1805	-.3921	-.0046	-.0002	.0003
70.56	4.12	2.4906	-.1762	-.3891	-.0215	-.0298	-.0060
70.56	8.13	2.4929	-.1733	-.4142	-.0496	-.0578	-.0123
70.56	10.09	2.4837	-.1719	-.4336	-.0666	-.0739	-.0168
70.54	15.10	2.4643	-.1634	-.4684	-.1313	-.0980	-.0266
70.51	20.07	2.4107	-.1473	-.5344	-.1800	-.1029	-.0380
70.51	29.96	2.3346	-.1358	-.5604	-.2373	-.1039	-.0566

RUN 241		Q= 93.20 PSF		RN/FT= 2.186		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.70	29.97	2.3511	-.1082	-.4778	-.2599	-.0929	-.0576
65.71	20.07	2.3538	-.1184	-.4538	-.1489	-.0763	-.0336
65.73	15.11	2.3944	-.1248	-.4395	-.1253	-.0849	-.0243
65.74	10.10	2.4543	-.1347	-.4267	-.0560	-.0697	-.0149
65.75	8.16	2.4652	-.1372	-.4188	-.0393	-.0539	-.0114
65.75	4.16	2.4643	-.1549	-.3794	-.0251	-.0237	-.0041
65.75	.20	2.4743	-.1405	-.3830	-.0240	-.0052	.0004
65.77	-3.78	2.4514	-.1352	-.3919	-.0066	.0213	.0060
65.73	-7.82	2.4509	-.1305	-.4174	.0224	.0602	.0112
65.74	-9.81	2.4426	-.1307	-.4173	.0303	.0748	.0141

APPENDIX - Continued

RUN 242		Q= 93.70 PSF		RN/FT= 2.187		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.86	-9.81	2.4023	-.1003	-.3923	.0435	.0663	.0132
60.86	-7.80	2.4278	-.1090	-.3799	.0192	.0517	.0105
60.85	-3.83	2.4529	-.1290	-.3330	-.0303	.0085	.0043
60.87	.21	2.4205	-.1457	-.3045	-.0196	-.0090	.0003
60.87	4.17	2.4336	-.1353	-.3418	-.0060	-.0095	-.0037
60.90	8.18	2.4173	-.1226	-.3594	-.0373	-.0395	-.0098
60.90	10.17	2.4264	-.1107	-.3854	-.0629	-.0602	-.0131
60.87	15.11	2.3826	-.1034	-.3961	-.1081	-.0600	-.0231
60.85	20.04	2.3366	-.0940	-.3770	-.1235	-.0505	-.0315
60.88	29.99	2.3247	-.1090	-.3154	-.2230	-.0817	-.0604

RUN 243		Q= 94.30 PSF		RN/FT= 2.191		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
51.25	30.02	2.4816	-.0349	-.3667	-.1767	-.0779	-.1027
51.26	20.07	2.5391	-.0408	-.3138	-.0119	-.0389	-.0513
51.26	15.04	2.5233	-.0480	-.3188	.0330	-.0296	-.0416
51.27	10.08	2.5299	-.0457	-.3198	.0461	-.0263	-.0332
51.27	8.12	2.4981	-.0463	-.3284	.0606	-.0251	-.0260
51.25	.21	2.4095	-.0677	-.3562	.0245	-.0093	.0075
51.26	4.16	2.4342	-.0523	-.3600	.0599	-.0117	-.0038
51.25	-3.80	2.3948	-.0574	-.3628	-.0530	.0202	.0031
51.28	-7.83	2.4209	-.0453	-.3305	-.0492	.0307	.0197
51.23	-9.75	2.4707	-.0471	-.3225	-.0637	.0313	.0276

APPENDIX - Continued

RUN 244		Q= 95.80 PSF		RN/FT= 2.205		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.99	-9.76	2.2979	.0439	-.3606	-.0138	.0398	.0160
40.95	-7.77	2.2453	.0433	-.3709	.0444	.0254	.0189
40.90	-3.82	2.1894	.0449	-.3794	.0570	-.0002	.0073
40.91	.19	2.2239	.0460	-.3987	-.0475	.0167	.0005
40.89	4.17	2.1999	.0467	-.3753	-.0861	.0097	-.0096
40.91	8.15	2.2335	.0458	-.3512	-.0585	-.0081	-.0187
40.94	10.12	2.2856	.0447	-.3553	-.0299	-.0036	-.0187
40.97	15.07	2.3618	.0461	-.3668	-.0283	-.0138	-.0356
40.98	20.09	2.3959	.0540	-.4082	-.0580	-.0330	-.0579
41.04	30.06	2.3329	.0476	-.5000	-.3051	-.0728	-.0964

RUN 245		Q= 91.30 PSF		RN/FT= 2.196		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.93	.19	2.1164	.0232	-.2658	-.0233	.0144	-.0016
51.15	.19	2.3478	-.0882	-.2639	.0212	-.0079	.0100
60.90	.19	2.3926	-.1692	-.2449	-.0176	-.0074	-.0006
65.74	.18	2.4145	-.1687	-.3212	-.0150	-.0054	-.0003
70.57	.17	2.4598	-.2071	-.3448	-.0032	.0013	.0008
75.49	.16	2.4692	-.2454	-.3929	.0022	.0010	.0006
80.54	.17	2.4728	-.2776	-.4090	.0047	.0018	.0013
85.68	.16	2.4608	-.2923	-.4222	.0026	.0006	.0009
91.02	.16	2.4221	-.3020	-.5018	.0005	.0039	.0013

APPENDIX - Continued

RUN 246		Q= 91.80 PSF		RN/FT= 2.192		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.05	.19	2.2924	-.1102	-.0637	-.0125	.0069	.0056
51.31	.17	2.5546	-.2093	-.0041	.0259	-.0074	.0070
61.05	.16	2.6383	-.2373	-.0112	-.0048	.0007	.0011
65.81	.16	2.5896	-.2003	-.1378	.0023	.0023	.0008
70.68	.17	2.5910	-.2083	-.1727	-.0058	.0002	.0015
75.62	.16	2.5906	-.2202	-.2404	.0005	-.0006	.0008
80.62	.16	2.5880	-.2297	-.2827	.0070	.0009	.0008
85.75	.17	2.5655	-.2403	-.3388	.0052	.0045	.0013
91.02	.17	2.5162	-.2441	-.4082	.0002	.0060	.0023

RUN 247		Q= 92.10 PSF		RN/FT= 2.190		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.21	.18	2.5569	-.1232	.1785	.0101	.0007	-.0011
51.42	.19	2.8087	-.1510	.1579	.0118	-.0105	.0081
61.12	.19	2.7329	-.1535	.0695	-.0061	-.0070	.0058
65.82	.17	2.6462	-.1375	-.0686	-.0069	.0022	.0016
70.68	.17	2.6598	-.1478	-.1127	-.0083	.0002	.0009
75.56	.16	2.6413	-.1493	-.1891	-.0079	.0005	.0019
80.62	.17	2.6307	-.1577	-.2327	-.0039	.0019	.0018
85.69	.17	2.5809	-.1613	-.3048	-.0073	.0030	.0015
91.01	.17	2.5744	-.1677	-.3676	.0018	-.0005	.0011

APPENDIX - Continued

RUN 248 Q= 23.60 PSF RN/FT= .587 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.63	.18	2.5678	-.1076	.1890	.0350	.0086	-.0026
50.79	.19	2.8843	-.1519	.2269	.0323	.0169	.0034
60.51	.16	2.8298	-.1593	.2476	.0498	.0360	-.0067
65.31	.17	2.7549	-.1482	.1636	-.0506	-.0197	-.0003
70.14	.18	2.7451	-.1518	.0916	-.0852	-.0486	.0035
75.05	.17	2.7384	-.1576	.0579	-.0951	-.0512	.0039
80.04	.16	2.7025	-.1580	.0554	-.0110	-.0032	.0025
85.20	.17	2.6677	-.1548	-.0731	-.0071	-.0014	.0010
90.54	.17	2.6087	-.1586	-.1422	-.0116	.0006	.0009

RUN 249 Q= 24.20 PSF RN/FT= .592 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.57	.17	2.3031	-.0956	-.0268	.0247	.0105	.0003
50.77	.18	2.6337	-.2018	.0987	.0142	.0233	-.0015
60.51	.17	2.7517	-.2430	.1823	.0429	.0487	-.0038
65.30	.16	2.7188	-.2364	.1711	.0662	.0577	-.0026
70.13	.16	2.6644	-.2179	.0330	-.0786	-.0446	.0036
75.04	.16	2.6426	-.2227	-.0067	-.0960	-.0544	.0046
80.07	.17	2.6415	-.2329	.0233	-.0372	-.0158	.0030
85.20	.16	2.6230	-.2369	-.0993	-.0036	.0016	.0012
90.58	.17	2.5758	-.2413	-.1849	-.0105	.0019	.0010

APPENDIX - Continued

RUN 250		Q= 23.90 PSF		RN/FT= .590		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.48	.17	2.1159	.0286	-.2189	.0111	.0161	-.0011
50.67	.18	2.3990	-.0906	-.1445	-.0216	.0250	-.0007
60.46	.16	2.5034	-.1642	-.0366	.0392	.0437	-.0083
65.27	.17	2.5308	-.1880	-.0036	.0534	.0559	-.0032
70.10	.17	2.5530	-.2010	-.0189	-.0045	.0143	-.0011
75.03	.19	2.5223	-.2266	-.1192	-.0899	-.0459	.0033
80.05	.16	2.5210	-.2527	-.0805	-.0284	-.0180	.0022
85.21	.17	2.5014	-.2653	-.1741	-.0093	.0015	.0008
90.55	.17	2.4653	-.2922	-.2542	-.0067	.0033	.0011

RUN 251		Q= 93.80 PSF		RN/FT= 2.259		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.87	.19	2.0695	-.0205	-.2650	-.0178	.0117	-.0008
51.13	.19	2.3118	-.1320	-.2664	.0264	-.0110	.0120
60.93	.19	2.3934	-.2180	-.2512	-.0148	-.0092	.0006
65.73	.17	2.4160	-.2169	-.3321	-.0134	-.0077	.0006
70.62	.17	2.4606	-.2549	-.3534	.0030	-.0007	.0012
75.45	.17	2.4470	-.2930	-.3907	.0028	-.0008	.0007
80.55	.16	2.4596	-.3240	-.4085	-.0016	-.0001	.0025
85.68	.15	2.4485	-.3378	-.4340	-.0017	.0008	.0018
91.00	.17	2.4082	-.3479	-.5052	-.0011	.0033	.0017

APPENDIX - Continued

RUN 252		Q= 88.30 PSF	RN/FT= 2.173		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.97	.17	2.2463	-.1567	-.0726	-.0218	.0053	.0059
51.28	.18	2.5462	-.2583	-.0144	.0216	-.0094	.0105
61.07	.17	2.6131	-.2878	-.0109	-.0083	.0008	.0001
65.82	.17	2.5685	-.2487	-.1465	-.0041	.0005	.0017
70.64	.17	2.5911	-.2564	-.1787	-.0122	-.0017	.0019
75.55	.17	2.5695	-.2672	-.2465	-.0063	-.0008	.0016
80.59	.17	2.5738	-.2755	-.2856	-.0056	.0006	.0018
85.70	.17	2.5367	-.2823	-.3515	.0110	.0058	.0018
91.01	.17	2.4917	-.2856	-.4092	.0055	.0043	.0022

RUN 253		Q= 89.30 PSF	RN/FT= 2.172		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.17	.17	2.5185	-.1753	.1738	-.0058	-.0007	.0018
51.45	.16	2.7978	-.2030	.1564	.0102	-.0146	.0108
61.15	.16	2.7077	-.2001	.0658	-.0152	-.0057	.0045
65.85	.17	2.6461	-.1845	-.0761	-.0023	.0009	.0021
70.68	.17	2.6493	-.1944	-.1120	-.0126	-.0005	.0029
75.56	.17	2.6405	-.1959	-.1915	-.0025	-.0017	.0017
80.60	.17	2.6414	-.2027	-.2412	.0002	-.0006	.0020
85.72	.17	2.5853	-.2026	-.3124	-.0047	.0045	.0025
91.04	.17	2.5556	-.2090	-.3623	.0057	.0051	.0033

APPENDIX - Continued

RUN 254 Q= 24.30 PSF RN/FT= .586 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.65	.19	2.5182	-.1574	.1860	.0393	.0109	-.0030
50.80	.19	2.8781	-.2064	.2380	.0323	.0184	.0042
60.50	.16	2.8440	-.2145	.2586	.0202	.0442	.0115
65.26	.17	2.8033	-.2060	.2304	.0548	.0446	-.0020
70.13	.18	2.7649	-.2083	.1859	-.0054	-.0096	.0013
75.06	.17	2.7350	-.2047	.0871	-.0676	-.0391	.0046
80.04	.16	2.7121	-.2024	.0459	-.0079	-.0010	.0024
85.21	.15	2.6875	-.2018	-.0805	-.0019	.0014	.0015
90.56	.15	2.6276	-.2028	-.1532	.0004	.0000	.0014

RUN 255 Q= 24.10 PSF RN/FT= .588 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.55	.18	2.2815	-.1414	-.0372	.0296	.0122	.0012
50.76	.16	2.6390	-.2537	.0950	.0225	.0207	.0014
60.50	.16	2.7410	-.2957	.1800	.0555	.0512	-.0039
65.31	.14	2.7253	-.2879	.1734	.0702	.0567	-.0014
70.16	.15	2.6867	-.2722	.0788	-.0367	-.0225	.0016
75.05	.16	2.6604	-.2711	.0076	-.0783	-.0466	.0049
80.07	.16	2.6421	-.2796	.0237	-.0272	-.0128	.0037
85.22	.16	2.6244	-.2842	-.1143	.0062	.0029	.0021
90.55	.16	2.5749	-.2873	-.1900	.0007	.0029	.0030

APPENDIX - Continued

RUN 256		Q= 24.20 PSF	RN/FT= .593		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.52	.16	2.0935	-.0137	-.2191	.0128	.0187	.0000
50.70	.17	2.3889	-.1367	-.1465	-.0156	.0284	.0016
60.44	.16	2.5017	-.2072	-.0390	.0547	.0448	-.0086
65.24	.16	2.5501	-.2358	-.0041	.0685	.0565	-.0021
70.12	.16	2.5739	-.2486	-.0103	.0268	.0222	.0000
75.03	.15	2.5501	-.2734	-.1022	-.0600	-.0366	.0033
80.04	.17	2.5413	-.2979	-.0802	-.0259	-.0148	.0033
85.22	.15	2.5277	-.3104	-.1881	.0049	.0015	.0012
90.57	.16	2.4748	-.3324	-.2678	.0065	.0060	.0029

RUN 257		Q= 89.30 PSF	RN/FT= 2.174		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.81	.18	1.9938	-.0398	-.2340	-.0214	.0113	-.0012
51.09	.18	2.2756	-.1557	-.2376	.0252	-.0092	.0117
60.89	.17	2.3623	-.2416	-.2211	.0002	-.0018	-.0015
65.70	.16	2.3897	-.2328	-.3121	-.0104	-.0029	-.0001
70.57	.16	2.4096	-.2773	-.3356	-.0006	.0007	.0004
75.49	.16	2.4281	-.3192	-.3739	.0027	.0015	.0005
80.50	.16	2.4321	-.3496	-.3887	.0081	.0021	.0007
85.64	.16	2.4316	-.3642	-.4102	.0056	.0018	.0016
91.02	.16	2.4115	-.3769	-.4938	.0071	.0051	.0012

APPENDIX - Continued

RUN 258		Q= 89.90 PSF		RN/FT= 2.167		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.96	.18	2.1672	-.1790	-.0388	-.0183	.0088	.0030
51.22	.17	2.4865	-.2832	.0194	.0282	-.0087	.0108
61.04	.17	2.5660	-.3132	.0204	-.0007	.0015	.0026
65.82	.17	2.5652	-.2792	-.1239	-.0008	.0034	.0006
70.66	.18	2.5381	-.2811	-.1586	-.0069	.0000	.0012
80.54	.16	2.5468	-.3016	-.2613	.0036	.0051	.0016
85.67	.17	2.5079	-.3076	-.3282	.0058	.0063	.0007
91.03	.16	2.4925	-.3133	-.3936	.0030	.0056	.0018
75.50	.17	2.5291	-.2931	-.2238	-.0043	.0006	.0010

RUN 259		Q= 90.50 PSF		RN/FT= 2.167		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
41.13	.18	2.4277	-.2015	.2015	.0060	.0038	-.0004
51.36	.18	2.7583	-.2337	.1954	.0050	-.0137	.0113
61.05	.18	2.6741	-.2266	.1021	-.0096	-.0067	.0057
65.81	.17	2.5983	-.2103	-.0443	-.0012	.0017	.0010
70.68	.16	2.6118	-.2194	-.0925	-.0088	-.0002	.0013
75.56	.17	2.6119	-.2201	-.1722	-.0060	.0011	.0008
80.56	.16	2.5800	-.2249	-.2177	-.0021	.0040	.0011
85.70	.17	2.5754	-.2298	-.2883	.0090	.0031	.0004
91.01	.16	2.5394	-.2324	-.3579	.0029	.0043	.0025

APPENDIX - Continued

RUN 260		Q= 22.40 PSF	RN/FT= .566		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.64	.20	2.4397	-.1804	.2223	.0436	.0087	-.0028
50.83	.17	2.8416	-.2354	.2667	.0267	.0147	.0024
60.47	.16	2.7696	-.2315	.2658	.0671	.0370	-.0090
65.30	.17	2.7364	-.2257	.2094	-.0024	-.0071	-.0008
70.13	.17	2.6464	-.2207	.1075	-.0776	-.0483	.0033
75.01	.17	2.6503	-.2253	.0856	-.0790	-.0452	.0031
80.00	.16	2.6632	-.2273	.0665	-.0003	-.0032	.0016
85.19	.16	2.6333	-.2249	-.0663	.0038	.0006	.0002
90.52	.15	2.5905	-.2276	-.1387	.0057	.0000	.0007

RUN 261		Q= 24.00 PSF	RN/FT= .584		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.54	.19	2.1738	-.1618	-.0029	.0261	.0132	-.0004
50.75	.16	2.5583	-.2784	.1251	.0174	.0184	-.0018
60.52	.15	2.6503	-.3142	.1968	.0611	.0495	-.0080
65.30	.16	2.6522	-.3090	.1823	.0522	.0302	-.0025
70.16	.15	2.5907	-.2900	.0512	-.0609	-.0419	.0025
75.03	.17	2.5825	-.2932	.0216	-.0784	-.0489	.0043
80.02	.15	2.5858	-.3019	.0413	-.0257	-.0137	.0020
85.20	.15	2.5638	-.3065	-.0961	.0057	.0028	.0020
90.56	.16	2.5402	-.3117	-.1669	-.0007	.0024	.0014

APPENDIX - Continued

RUN 262		Q= 24.10 PSF	RN/FT= .585		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.45	.18	1.9929	-.0330	-.1842	.0053	.0200	-.0029
50.67	.16	2.3085	-.1595	-.1087	-.0043	.0235	.0002
60.48	.16	2.4475	-.2353	-.0096	.0617	.0483	-.0099
65.22	.15	2.4695	-.2537	.0115	.0660	.0549	-.0034
70.09	.15	2.4773	-.2631	-.1011	-.0727	-.0396	.0025
74.98	.17	2.4931	-.2970	-.0778	-.0552	-.0377	.0020
80.01	.17	2.5044	-.3202	-.0690	-.0284	-.0153	.0031
85.18	.15	2.4907	-.3390	-.1736	.0033	.0018	.0009
90.54	.17	2.4341	-.3579	-.2477	.0104	.0040	.0014

RUN 263		Q= 92.50 PSF	RN/FT= 2.217		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.88	.22	2.1088	.0089	-.3515	-.0595	-.0004	.0215
51.10	.19	2.3464	-.1026	-.3069	.0021	-.0118	.0240
60.89	.18	2.3737	-.1843	-.2719	-.0519	-.0056	.0155
70.60	.17	2.4398	-.2185	-.3703	-.0480	-.0038	.0148
80.51	.18	2.4256	-.2876	-.4012	-.0460	.0009	.0100
91.05	.17	2.3951	-.3169	-.4763	-.0386	.0008	.0078

APPENDIX - Continued

RUN 264 Q= 96.90 PSF RN/FT= 2.257 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.51	-9.77	2.3826	-.2736	-.4244	.0423	.0771	.0345
80.50	-7.77	2.3951	-.2762	-.4153	.0168	.0651	.0296
80.49	-3.80	2.4158	-.2837	-.4040	-.0101	.0318	.0206
80.48	.16	2.4358	-.2905	-.4007	-.0475	.0010	.0102
80.48	4.17	2.4370	-.2891	-.4022	-.0849	-.0341	.0005
80.48	8.15	2.4204	-.2864	-.4138	-.1301	-.0630	-.0089
80.51	10.12	2.3966	-.2810	-.4377	-.1488	-.0803	-.0141
80.49	15.12	2.3642	-.2720	-.4813	-.2045	-.1033	-.0270
80.49	20.07	2.3460	-.2662	-.5386	-.2422	-.1242	-.0376
80.45	29.97	2.2446	-.2494	-.5685	-.2304	-.1044	-.0586

RUN 265 Q= 95.40 PSF RN/FT= 2.234 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.95	30.02	2.3254	-.1605	-.3734	-.2924	-.0925	-.0649
60.86	20.08	2.2576	-.1306	-.3966	-.1591	-.0650	-.0189
60.86	15.09	2.3155	-.1478	-.3744	-.1401	-.0683	-.0074
60.89	10.14	2.3545	-.1504	-.3627	-.1203	-.0636	.0043
60.89	8.13	2.3603	-.1624	-.3361	-.0941	-.0440	.0079
60.90	4.14	2.3725	-.1723	-.3100	-.0485	-.0114	.0139
60.91	.16	2.3639	-.1821	-.2775	-.0468	.0012	.0151
60.87	-3.78	2.3291	-.1599	-.2876	-.0605	.0040	.0227
60.87	-7.78	2.3224	-.1438	-.3274	-.0281	.0429	.0311
60.88	-9.78	2.3179	-.1376	-.3431	-.0146	.0598	.0348

APPENDIX - Continued

RUN 266		Q= 93.60 PSF		RN/FT= 2.208		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
51.13	-9.75	2.3577	-.0824	-.2624	-.1021	.0317	.0519
51.09	-7.75	2.2943	-.0795	-.2750	-.0846	.0291	.0385
51.08	-3.79	2.2724	-.0906	-.2991	-.0893	.0123	.0199
51.10	.19	2.3359	-.1014	-.3077	-.0003	-.0133	.0235
51.15	4.09	2.3956	-.0950	-.3190	.0514	-.0100	.0030
51.17	8.12	2.4502	-.0908	-.2972	.0122	-.0221	-.0109
51.19	10.11	2.4914	-.0932	-.2944	.0121	-.0249	-.0173
51.20	15.03	2.5283	-.0961	-.3092	.0010	-.0306	-.0307
51.21	20.05	2.5507	-.0930	-.3154	-.0481	-.0551	-.0412
51.19	30.05	2.4929	-.0925	-.3954	-.2302	-.0845	-.0929

RUN 267		Q= 94.70 PSF		RN/FT= 2.218		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.02	30.09	2.2920	-.0048	-.4847	-.3460	-.0833	-.0776
41.01	20.07	2.3601	.0017	-.4042	-.1020	-.0500	-.0365
40.99	15.07	2.2464	-.0032	-.3673	-.0631	-.0402	-.0074
40.96	10.13	2.1749	.0012	-.3384	-.0686	-.0261	.0093
40.93	8.14	2.1219	.0048	-.3328	-.1025	-.0199	.0073
40.87	4.18	2.0782	.0080	-.3336	-.1298	-.0020	.0178
40.89	.18	2.0949	.0103	-.3486	-.0676	.0001	.0206
40.84	-3.78	2.0155	.0154	-.3231	.0499	-.0192	.0350
40.88	-7.77	2.0527	.0114	-.2779	.0495	.0048	.0459
40.93	-9.79	2.1429	.0052	-.2867	-.0030	.0245	.0451

APPENDIX - Continued

RUN 268		Q= 92.70 PSF	RN/FT= 2.200		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.13	.20	2.5822	-.0418	-.0797	-.0816	.0076	-.0116
51.37	.18	2.7339	-.1003	-.0185	-.0659	.0127	-.0286
60.06	.17	2.6451	-.1116	-.0966	-.0581	.0045	-.0115
70.69	.17	2.6429	-.1117	-.2036	-.0514	-.0074	-.0107
80.56	.16	2.6062	-.1209	-.2984	-.0233	.0078	-.0074
91.04	.17	2.5214	-.1310	-.4031	-.0279	.0162	-.0024

RUN 269		Q= 98.10 PSF	RN/FT= 2.259		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.59	-9.75	2.6156	-.1429	-.3159	.0438	.0660	.0152
80.59	-7.74	2.6322	-.1428	-.3125	.0222	.0557	.0106
80.57	-3.80	2.6170	-.1342	-.2895	-.0081	.0320	.0016
80.54	.17	2.6089	-.1216	-.2996	-.0265	.0073	-.0068
80.53	4.16	2.6054	-.1166	-.3010	-.0608	-.0173	-.0157
80.51	8.14	2.5666	-.1114	-.3190	-.0929	-.0421	-.0236
80.51	10.12	2.5425	-.1074	-.3303	-.1137	-.0571	-.0284
80.49	15.14	2.5004	-.1001	-.3823	-.1639	-.0825	-.0382
80.47	20.04	2.4164	-.0934	-.4114	-.1855	-.0904	-.0474
80.42	29.95	2.3113	-.0753	-.4449	-.2017	-.0841	-.0678

APPENDIX - Continued

RUN 270		Q= 94.90 PSF		RN/FT= 2.219		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
61.01	29.99	2.3987	-.0492	-.2277	-.2040	-.0775	-.0666
61.02	20.10	2.4584	-.0656	-.1701	-.1592	-.0454	-.0448
61.07	15.13	2.5357	-.0753	-.1698	-.1701	-.0523	-.0368
61.10	10.12	2.5853	-.0822	-.1592	-.1693	-.0607	-.0259
61.11	8.15	2.6223	-.0887	-.1538	-.1435	-.0507	-.0216
61.13	4.17	2.6376	-.0975	-.1369	-.1055	-.0244	-.0149
61.16	.16	2.6618	-.1097	-.1285	-.0759	.0004	-.0091
61.18	-3.74	2.7033	-.1165	-.1488	-.0816	.0211	-.0023
61.19	-7.79	2.6704	-.1213	-.1501	-.0556	.0472	.0035
61.20	-9.79	2.6643	-.1251	-.1512	-.0385	.0574	.0080

RUN 271		Q= 93.30 PSF		RN/FT= 2.193		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
41.26	-9.75	2.7143	-.0451	-.0560	-.0640	.0198	.0076
41.22	-7.73	2.6346	-.0416	-.0602	-.0698	.0101	.0055
41.18	-3.77	2.5840	-.0438	-.0826	-.1028	.0051	.0070
41.13	.21	2.5932	-.0413	-.0834	-.0886	.0069	-.0116
41.10	4.24	2.5443	-.0402	-.0810	-.1415	.0062	-.0176
41.10	8.15	2.4946	-.0336	-.0799	-.1445	.0022	-.0311
41.10	10.21	2.5375	-.0289	-.0900	-.0967	-.0063	-.0292
41.07	15.08	2.5600	-.0187	-.1486	-.0225	-.0328	-.0457
41.08	20.01	2.5759	-.0099	-.1958	-.0059	-.0455	-.0759
40.97	30.06	2.3739	.0046	-.3412	-.2677	-.0697	-.1354

APPENDIX - Continued

RUN 272 Q= 23.80 PSF RN/FT= .596 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.68	.20	2.5910	-.0258	-.0483	-.0162	.0130	-.0148
50.81	.16	2.7700	-.0940	.0657	-.0388	.0262	-.0229
60.45	.17	2.7387	-.1269	.1060	-.0107	.0405	-.0134
70.11	.18	2.6660	-.1118	-.0197	-.1234	-.0549	-.0064
80.03	.17	2.6264	-.1156	-.0236	-.0204	.0094	-.0075
90.50	.17	2.5720	-.1188	-.1931	-.0165	.0130	-.0039

RUN 273 Q= 26.10 PSF RN/FT= .618 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.04	-9.72	2.6250	-.1272	-.0713	-.0573	-.0099	.0168
80.06	-7.68	2.6498	-.1270	-.0729	-.0729	-.0185	.0118
80.05	-3.80	2.6454	-.1196	-.0759	-.0601	-.0119	.0022
80.04	.17	2.6422	-.1153	-.0285	-.0071	.0114	-.0078
80.02	4.12	2.6125	-.1103	-.0767	.0214	.0252	-.0180
80.01	8.15	2.5849	-.1089	-.0691	.0259	.0264	-.0277
80.01	10.14	2.5624	-.1027	-.0823	.0184	.0216	-.0330
80.00	15.01	2.5638	-.0938	-.0684	-.0175	-.0047	-.0431
79.98	20.04	2.5019	-.0806	-.0924	-.0602	-.0342	-.0514
79.95	29.96	2.3692	-.0552	-.1485	-.1747	-.0876	-.0674

APPENDIX - Continued

RUN 274		Q= 25.30 PSF		RN/FT= .607		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.43	29.96	2.5309	-.0443	.1887	-.2050	-.0797	-.0746
60.46	19.98	2.6217	-.0663	.1159	-.2006	-.0908	-.0454
60.45	15.06	2.6245	-.0754	.0702	-.2004	-.0905	-.0353
60.46	10.14	2.6940	-.0870	.0187	-.1617	-.0815	-.0247
60.46	8.11	2.6634	-.0922	.0267	-.1222	-.0541	-.0213
60.47	4.19	2.7098	-.1055	.0642	-.0377	.0125	-.0195
60.51	.11	2.7419	-.1289	.1104	-.0014	.0426	-.0133
60.54	-3.79	2.8059	-.1401	.2610	-.1392	-.0758	.0003
60.55	-7.76	2.7917	-.1370	.2690	-.1519	-.0577	.0120
60.56	-9.72	2.8032	-.1379	.2287	-.1219	-.0237	.0138

RUN 275		Q= 23.80 PSF		RN/FT= .589		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.69	-9.72	2.8098	-.0606	.1273	-.1224	.0061	.0096
40.66	-7.72	2.6639	-.0536	.0802	-.0790	.0046	.0107
40.60	-3.80	2.6223	-.0412	-.0219	-.0920	.0006	-.0002
40.58	.18	2.5738	-.0271	-.0475	-.0098	.0152	-.0159
40.56	4.13	2.5036	-.0166	.0345	.0361	.0299	-.0339
40.56	8.12	2.5540	-.0125	.1138	.0699	.0319	-.0514
40.56	10.17	2.5648	-.0109	.1525	.0840	.0383	-.0550
40.55	15.04	2.4894	-.0147	.2491	.0263	.0465	-.0604
40.53	20.05	2.4733	-.0087	.1927	-.0773	.0100	-.0672
40.47	30.00	2.3674	.0177	-.0914	-.2145	-.0451	-.1327

APPENDIX - Continued

RUN 276		Q= 92.00 PSF	RN/FT= 2.189		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.29	-9.71	2.8043	.0209	.1189	-.0341	.0276	.0211
41.28	-7.72	2.7957	.0203	.1304	-.0411	.0146	.0254
41.27	-3.79	2.7690	.0215	.1243	-.0614	-.0001	.0235
41.30	.19	2.8638	.0209	.1110	-.0146	.0009	-.0007
41.25	4.15	2.8216	.0253	.1275	.0049	-.0028	-.0138
41.31	8.14	2.8523	.0275	.1144	.0263	-.0145	-.0206
41.30	10.09	2.8198	.0282	.0961	.0511	-.0202	-.0205
41.30	15.08	2.8686	.0280	.0565	.0871	-.0454	-.0318
41.30	20.04	2.8726	.0235	.0369	.0681	-.0497	-.0422
41.26	29.98	2.7700	.0181	-.1074	-.1414	-.0713	-.0853

RUN 277		Q= 95.20 PSF	RN/FT= 2.224		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
51.33	29.95	2.6470	.0126	-.0696	-.1023	-.0534	-.0976
51.38	20.06	2.7252	.0198	-.0079	-.0202	-.0423	-.0385
51.41	15.07	2.7979	.0189	-.0076	.0221	-.0515	-.0289
51.41	10.14	2.8760	.0137	.0190	.0203	-.0629	-.0199
51.40	8.14	2.8349	.0120	.0313	.0169	-.0564	-.0162
51.39	4.14	2.7922	.0093	.0681	.0250	-.0282	-.0066
51.42	.18	2.8206	.0057	.1038	.0135	-.0070	.0005
51.41	-3.79	2.7988	.0078	.0950	-.0276	.0168	.0086
51.40	-7.78	2.7838	.0092	.0334	-.0224	.0501	.0144
51.40	-9.73	2.7626	.0097	.0275	-.0268	.0539	.0174

APPENDIX - Continued

RUN 278		Q= 92.10 PSF		RN/FT= 2.219		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.28	.19	2.8654	.0208	.1104	-.0051	.0003	-.0002
51.39	.19	2.8032	.0063	.1037	.0114	-.0075	.0007
61.06	.17	2.6930	-.0027	-.0588	.0062	.0012	.0009
70.66	.17	2.6753	-.0115	-.1635	-.0045	.0007	.0014
80.52	.16	2.6206	-.0183	-.2764	.0012	.0049	.0007
90.98	.17	2.5433	-.0262	-.4016	-.0024	.0045	.0031

RUN 279		Q= 91.10 PSF		RN/FT= 2.192		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
91.01	-9.73	2.5332	-.0253	-.4326	.0710	.0583	.0256
91.00	-7.76	2.5368	-.0246	-.4235	.0490	.0524	.0207
91.00	-3.80	2.5644	-.0256	-.4053	.0378	.0242	.0111
90.98	.17	2.5430	-.0252	-.4012	-.0007	.0035	.0015
90.98	4.16	2.5426	-.0217	-.4076	-.0322	-.0189	-.0113
90.96	8.11	2.5378	-.0197	-.4282	-.0624	-.0419	-.0195
90.96	10.12	2.5325	-.0190	-.4320	-.0757	-.0559	-.0248
90.94	15.04	2.4883	-.0151	-.4594	-.1320	-.0745	-.0361
90.95	20.02	2.4605	-.0148	-.4655	-.1744	-.1020	-.0458
90.93	29.94	2.3436	-.0091	-.5466	-.2461	-.1283	-.0659

APPENDIX - Continued

RUN 280		Q= 90.90 PSF		RN/FT= 2.180		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.67	29.94	2.3670	-.0074	-.4963	-.2505	-.1354	-.0613
85.67	20.06	2.4901	-.0129	-.4304	-.1577	-.0946	-.0437
85.68	15.11	2.5224	-.0131	-.3948	-.1292	-.0880	-.0338
85.70	10.13	2.5500	-.0150	-.3689	-.0733	-.0570	-.0226
85.70	8.10	2.5710	-.0173	-.3539	-.0573	-.0452	-.0184
85.71	4.16	2.5790	-.0198	-.3420	-.0245	-.0208	-.0079
85.72	.17	2.5697	-.0224	-.3449	-.0024	.0038	.0016
85.73	-3.75	2.5763	-.0224	-.3435	.0392	.0201	.0084
85.73	-7.74	2.5725	-.0224	-.3601	.0624	.0518	.0188
85.74	-9.74	2.5679	-.0220	-.3740	.0694	.0642	.0241

RUN 281		Q= 90.40 PSF		RN/FT= 2.168		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.49	-9.74	2.5787	-.0199	-.3065	.0698	.0644	.0207
80.48	-7.74	2.6061	-.0205	-.2890	.0600	.0517	.0167
80.48	-3.83	2.6159	-.0195	-.2856	.0284	.0303	.0088
80.46	.19	2.6122	-.0184	-.2785	-.0057	.0038	.0008
80.46	4.15	2.6139	-.0175	-.2727	-.0407	-.0219	-.0071
80.45	8.13	2.5989	-.0145	-.2911	-.0718	-.0446	-.0169
80.45	10.14	2.5940	-.0139	-.3031	-.0957	-.0600	-.0201
80.43	15.09	2.5501	-.0111	-.3334	-.1407	-.0858	-.0299
80.42	20.05	2.5112	-.0095	-.3622	-.1427	-.0854	-.0413
80.43	29.95	2.4093	-.0084	-.4667	-.2513	-.1382	-.0584

APPENDIX - Continued

RUN 282		Q= 92.90 PSF		RN/FT= 2.191		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
75.51	29.98	2.4147	-.0024	-.4295	-.2338	-.1291	-.0550
75.53	20.06	2.5230	-.0045	-.3293	-.1342	-.0851	-.0385
75.54	15.10	2.5710	-.0063	-.2973	-.1377	-.0841	-.0275
75.56	10.15	2.5883	-.0077	-.2651	-.0854	-.0575	-.0185
75.57	8.11	2.6177	-.0098	-.2512	-.0648	-.0432	-.0154
75.59	4.14	2.6494	-.0122	-.2352	-.0287	-.0186	-.0072
75.60	.19	2.6559	-.0139	-.2368	.0028	.0023	.0014
75.61	-3.78	2.6417	-.0153	-.2267	.0348	.0248	.0087
75.63	-7.79	2.6189	-.0145	-.2538	.0701	.0488	.0145
75.63	-9.74	2.6209	-.0145	-.2715	.0791	.0628	.0191

RUN 283		Q= 92.60 PSF		RN/FT= 2.179		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.61	-9.72	2.6217	-.0088	-.2207	.0646	.0607	.0175
70.60	-7.80	2.6374	-.0095	-.2021	.0490	.0476	.0141
70.59	-3.82	2.6608	-.0106	-.1754	.0223	.0207	.0069
70.61	.16	2.6723	-.0107	-.1629	-.0056	.0001	.0004
70.60	4.17	2.6682	-.0079	-.1757	-.0318	-.0227	-.0067
70.59	8.12	2.6543	-.0054	-.1945	-.0554	-.0445	-.0137
70.59	10.10	2.6447	-.0047	-.2076	-.0838	-.0552	-.0168
70.58	15.08	2.6014	-.0011	-.2407	-.1215	-.0798	-.0270
70.55	20.06	2.5512	.0014	-.3002	-.1295	-.0855	-.0360
70.51	29.98	2.4531	.0038	-.3540	-.1569	-.0883	-.0560

APPENDIX - Continued

RUN 284		Q= 93.20 PSF		RN/FT= 2.178		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
65.77	29.99	2.4811	.0048	-.2485	-.1582	-.0772	-.0575
65.79	20.09	2.5509	.0045	-.2070	-.1107	-.0701	-.0360
65.81	15.11	2.6070	0.0000	-.1604	-.1024	-.0743	-.0253
65.82	10.12	2.6471	-.0028	-.1262	-.0765	-.0530	-.0153
65.81	8.16	2.6431	-.0034	-.1222	-.0553	-.0416	-.0122
65.83	4.15	2.6544	-.0061	-.1030	-.0284	-.0192	-.0046
65.84	.20	2.6827	-.0069	-.1111	.0011	.0002	.0015
65.89	-3.80	2.6737	-.0068	-.1214	.0222	.0219	.0072
65.90	-7.75	2.6648	-.0068	-.1334	.0495	.0461	.0133
65.91	-9.78	2.6309	-.0058	-.1425	.0673	.0574	.0164

RUN 285		Q= 93.50 PSF		RN/FT= 2.172		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
60.97	-9.79	2.6383	0.0000	-.1056	.0433	.0589	.0145
60.96	-7.79	2.6469	.0002	-.1001	.0335	.0499	.0114
60.96	-3.81	2.6775	-.0008	-.0819	.0100	.0223	.0066
60.95	.18	2.6905	-.0019	-.0585	.0049	.0003	.0011
60.95	4.15	2.6558	.0001	-.0651	-.0181	-.0182	-.0052
60.95	8.11	2.6720	.0026	-.0805	-.0459	-.0429	-.0106
60.95	10.12	2.6565	.0041	-.0904	-.0678	-.0560	-.0142
60.93	15.12	2.6347	.0073	-.1206	-.0904	-.0600	-.0239
60.89	20.06	2.5586	.0094	-.1399	-.0975	-.0461	-.0335
60.89	29.98	2.4831	.0088	-.1751	-.1605	-.0696	-.0589

APPENDIX - Continued

RUN 286		Q= 57.60 PSF		RN/FT= 1.390		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.30	.21	2.8749	.0233	.1076	.0138	.0035	.0015
51.08	.21	2.7674	.0093	.1120	.0076	.0001	-.0010
60.74	.19	2.6644	.0004	-.0546	.0048	.0003	.0006
65.58	.20	2.6559	-.0042	-.1049	.0022	.0010	.0012
70.33	.21	2.6504	-.0088	-.1544	.0001	.0035	.0007
75.24	.21	2.6083	-.0129	-.2078	.0039	.0090	.0008
80.22	.21	2.5682	-.0160	-.2697	.0049	.0111	.0012
85.42	.18	2.5525	-.0181	-.3337	.0057	.0037	-.0010
90.72	.21	2.5140	-.0234	-.3443	.0230	.0208	.0011

RUN 287		Q= 24.40 PSF		RN/FT= .590		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.66	.20	2.8543	.0224	.1493	.0386	.0098	.0020
50.76	.20	2.8898	0.0000	.2108	.0208	.0073	.0059
60.50	.19	2.7634	-.0228	.2145	.0356	.0468	-.0025
70.13	.20	2.7327	-.0272	.0540	-.0686	-.0448	.0020
79.99	.20	2.6871	-.0266	-.0285	-.0094	.0002	.0011
90.48	.20	2.5697	-.0269	-.1810	-.0143	.0023	.0011

APPENDIX - Continued

RUN 288		Q= 24.80 PSF	RN/FT= .593		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
90.50	-9.71	2.5664	-.0235	-.2034	-.0333	.0050	.0277
90.50	-7.77	2.5556	-.0250	-.2030	-.0246	.0030	.0217
90.48	-3.82	2.5495	-.0249	-.1963	-.0155	.0041	.0115
90.47	.17	2.5487	-.0266	-.1921	-.0160	.0016	.0006
90.46	4.13	2.5489	-.0250	-.2067	-.0016	-.0018	-.0100
90.45	8.11	2.5440	-.0222	-.1994	.0024	.0002	-.0222
90.47	10.10	2.5363	-.0203	-.2173	.0022	-.0023	-.0289
90.46	15.04	2.5110	-.0178	-.2188	-.0243	-.0136	-.0383
90.45	20.02	2.4682	-.0124	-.2319	-.0911	-.0394	-.0486
90.47	29.93	2.3324	-.0005	-.2460	-.1366	-.0596	-.0680

RUN 289		Q= 25.20 PSF	RN/FT= .597		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
85.12	29.92	2.3696	-.0057	-.1689	-.1350	-.0692	-.0637
85.15	20.03	2.5006	-.0118	-.1564	-.0554	-.0361	-.0468
85.16	15.06	2.5390	-.0169	-.1378	-.0032	-.0095	-.0361
85.16	10.11	2.5899	-.0198	-.1422	.0269	.0031	-.0255
85.17	8.13	2.5907	-.0210	-.1449	.0233	.0047	-.0203
85.16	4.13	2.5976	-.0235	-.1295	-.0025	-.0014	-.0087
85.18	.16	2.6052	-.0262	-.1187	-.0087	-.0006	.0001
85.19	-3.79	2.6011	-.0257	-.1362	-.0201	.0045	.0112
85.17	-7.77	2.6046	-.0244	-.1505	-.0343	-.0062	.0205
85.17	-9.76	2.5872	-.0237	-.1521	-.0442	.0019	.0261

APPENDIX - Continued

RUN 290		Q= 25.10 PSF		RN/FT= .596		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
80.00	-9.76	2.6297	-.0255	-.0707	-.0464	-.0086	.0238
80.00	-7.78	2.6072	-.0241	-.0715	-.0569	-.0174	.0180
80.00	-3.80	2.6407	-.0238	-.0699	-.0583	-.0140	.0104
79.99	.17	2.6584	-.0267	-.0264	-.0161	.0000	.0003
79.99	4.13	2.6400	-.0232	-.0667	.0248	.0117	-.0096
79.97	8.10	2.6352	-.0226	-.0773	.0379	.0160	-.0184
79.97	10.12	2.6297	-.0207	-.0665	.0324	.0157	-.0239
79.96	15.03	2.5967	-.0190	-.0578	.0033	-.0025	-.0334
79.95	20.06	2.5595	-.0145	-.0655	-.0287	-.0265	-.0430
79.93	29.92	2.4436	-.0081	-.1128	-.1424	-.0806	-.0600

RUN 291		Q= 25.30 PSF		RN/FT= .599		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
74.99	29.91	2.4784	-.0098	-.0497	-.1673	-.0940	-.0566
75.00	20.02	2.5765	-.0163	.0034	-.0348	-.0401	-.0396
75.02	15.03	2.6190	-.0225	.0201	-.0185	-.0223	-.0293
75.02	10.09	2.6578	-.0250	.0165	.0210	.0056	-.0204
75.03	8.14	2.6722	-.0250	.0160	.0423	.0111	-.0169
75.04	4.13	2.6867	-.0284	.0306	.0143	.0079	-.0080
75.05	.16	2.6976	-.0338	.0719	-.0285	-.0200	.0017
75.06	-3.78	2.6970	-.0297	.0428	-.0606	-.0318	.0099
75.07	-7.75	2.6797	-.0287	.0475	-.0566	-.0233	.0187
75.08	-9.75	2.6738	-.0295	.0547	-.0518	-.0148	.0220

APPENDIX - Continued

RUN 292		Q= 25.10 PSF	RN/FT= .597		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
70.12	-9.74	2.6969	-.0289	.1273	-.0375	-.0128	.0193
70.13	-7.75	2.7029	-.0284	.1201	-.0521	-.0199	.0166
70.11	-3.76	2.7015	-.0274	.0641	-.0851	-.0437	.0104
70.10	.20	2.6946	-.0274	.0437	-.0853	-.0469	.0029
70.09	4.10	2.7133	-.0283	.0753	-.0228	-.0128	-.0059
70.08	8.12	2.6780	-.0265	.0621	-.0211	-.0171	-.0128
70.08	10.07	2.6842	-.0263	.0639	-.0372	-.0255	-.0165
70.08	15.05	2.6573	-.0217	.0651	-.0698	-.0546	-.0273
70.07	20.04	2.6281	-.0184	.0499	-.1263	-.0837	-.0366
70.03	29.93	2.5271	-.0099	.0380	-.1810	-.1009	-.0574

RUN 293		Q= 25.40 PSF	RN/FT= .602		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
65.28	29.94	2.5597	-.0130	.1748	-.1765	-.0866	-.0569
65.32	20.01	2.6575	-.0234	.1823	-.1315	-.0835	-.0361
65.31	15.09	2.6756	-.0179	.0701	-.1226	-.0918	-.0249
65.30	10.09	2.7002	-.0201	.0634	-.0735	-.0583	-.0148
65.31	8.10	2.6989	-.0212	.0661	-.0529	-.0443	-.0112
65.31	4.15	2.7139	-.0213	.0609	-.0361	-.0363	-.0045
65.33	.17	2.7195	-.0240	.0925	-.0619	-.0375	.0007
65.35	-3.76	2.7194	-.0250	.1223	-.0650	-.0458	.0094
65.36	-7.74	2.7387	-.0262	.1850	-.0451	-.0324	.0161
65.37	-9.73	2.7189	-.0249	.1845	-.0285	-.0179	.0187

APPENDIX - Continued

RUN 294		Q= 25.10 PSF		RN/FT= .600		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.47	-9.73	2.7493	-.0241	.3066	-.0408	-.0270	.0188
60.48	-7.74	2.7750	-.0267	.3033	-.0676	-.0493	.0175
60.48	-3.79	2.7999	-.0291	.2385	-.1020	-.0761	.0089
60.45	.18	2.7578	-.0200	.1426	.0263	.0491	-.0040
60.42	4.14	2.7136	-.0140	.0502	-.0342	-.0342	-.0046
60.41	8.12	2.6818	-.0126	.0438	-.0707	-.0580	-.0112
60.41	10.14	2.7083	-.0115	.0453	-.1006	-.0806	-.0150
60.41	15.07	2.6630	-.0142	.1154	-.1358	-.0915	-.0249
60.41	20.06	2.6319	-.0132	.1387	-.1804	-.0959	-.0352
60.39	29.93	2.5674	-.0079	.1936	-.2030	-.0946	-.0658

RUN 295		Q= 25.20 PSF		RN/FT= .602		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
50.79	29.94	2.7743	.0065	.2800	-.0502	-.0389	-.1153
50.82	20.07	2.8690	.0053	.3161	.0186	-.0447	-.0606
50.82	15.07	2.8670	.0073	.1511	.0065	-.0816	-.0358
50.83	10.11	2.8950	-.0023	.2778	.0263	-.0463	-.0292
50.84	8.10	2.8973	-.0080	.3388	.0027	.0016	-.0268
50.85	4.14	2.9314	-.0207	.3610	.1095	.0548	.0016
50.83	.19	2.8282	-.0015	.2011	.0170	.0077	.0048
50.86	-3.76	2.8715	-.0119	.3108	-.0795	-.0278	-.0084
50.91	-7.75	2.9476	-.0266	.5001	-.1118	-.0535	.0129
50.91	-9.73	2.9227	-.0294	.5492	-.1033	-.0600	.0229

APPENDIX - Continued

RUN 296		Q= 25.80 PSF		RN/FT= .609		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.71	-9.73	2.9195	.0043	.3287	-.1320	.0086	.0187
40.70	-7.73	2.8680	.0092	.2807	-.0964	.0110	.0269
40.66	-3.78	2.7841	.0205	.1836	-.0838	.0011	.0142
40.64	.17	2.7981	.0200	.1404	.0306	.0100	.0009
40.63	4.12	2.7802	.0211	.2057	.1287	.0155	-.0193
40.64	8.13	2.8572	.0131	.3100	.1417	.0129	-.0305
40.62	10.11	2.7754	.0213	.1912	-.0034	-.0296	-.0253
40.61	15.07	2.7252	.0230	.1698	.0114	-.0483	-.0398
40.61	20.01	2.7323	.0191	.2212	.0241	-.0503	-.0558
40.58	29.95	2.7120	.0281	.0428	-.1312	-.0552	-.0954

RUN 299		Q=165.40 PSF		RN/FT= 3.613		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-42.01	-.15	-2.8204	.1090	-.1700	-.0372	-.0126	-.0065
-51.88	-.16	-2.6647	.1055	-.0474	-.0399	-.0069	-.0028
-61.51	-.16	-2.6285	.1012	.1245	-.0383	-.0061	.0005
-71.19	-.16	-2.6224	.0937	.2787	-.0372	-.0055	.0007
-81.01	-.15	-2.5831	.0792	.3246	-.0413	-.0066	.0008
-91.47	-.17	-2.5469	.0668	.4173	-.0330	-.0019	-.0002

APPENDIX - Continued

<div> <div>RUN 300</div> <div>Q=165.80 PSF</div> <div>RN/FT= 3.601</div> <div>MACH=0.20</div> </div>							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-81.02	9.80	-2.5365	.0825	.3698	-.3550	-.0350	.0184
-81.02	7.80	-2.5560	.0802	.3461	-.2827	-.0304	.0138
-81.01	3.79	-2.5822	.0807	.3332	-.1541	-.0223	.0084
-81.00	-.19	-2.5851	.0772	.3176	-.0288	-.0053	.0012
-80.99	-4.16	-2.5810	.0793	.3256	.0822	.0094	-.0085
-81.00	-8.19	-2.5721	.0813	.3369	.2108	.0154	-.0133
-80.98	-10.17	-2.5386	.0809	.3425	.2735	.0180	-.0174
-80.96	-15.09	-2.4705	.0813	.3749	.4371	.0160	-.0230
-80.93	-20.04	-2.3612	.0820	.3412	.5681	-.0016	-.0281
-80.82	-30.06	-2.0678	.0759	.1672	.8037	-.0732	-.0426
<div> <div>RUN 301</div> <div>Q=159.80 PSF</div> <div>RN/FT= 3.525</div> <div>MACH=0.20</div> </div>							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-61.36	-30.19	-2.0228	.0793	.0468	.7884	-.0164	-.0459
-61.44	-20.17	-2.3402	.0934	.1473	.5683	-.0028	-.0220
-61.42	-15.17	-2.4282	.0963	.1746	.4430	.0131	-.0171
-61.47	-10.12	-2.5414	.0988	.1494	.2844	.0105	-.0108
-61.49	-8.21	-2.5680	.0983	.1346	.2245	.0106	-.0089
-61.51	-4.19	-2.6096	.0982	.1266	.0894	.0060	-.0036
-61.51	-.16	-2.6329	.0986	.1315	-.0417	-.0051	.0008
-61.51	3.85	-2.6112	.0993	.1277	-.1742	-.0181	.0053
-61.53	7.89	-2.5741	.0999	.1406	-.3055	-.0204	.0097
-61.53	9.88	-2.5301	.0993	.1470	-.3641	-.0190	.0112

APPENDIX - Continued

RUN 302		Q=141.80 PSF		RN/FT= 3.311		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-41.66	9.86	-2.6400	.1106	-.1878	-.3042	.0229	.0276
-41.70	7.74	-2.6871	.1113	-.1938	-.2542	.0159	.0218
-41.74	3.80	-2.7830	.1111	-.1786	-.1391	.0062	.0093
-41.73	-.09	-2.7905	.1126	-.1581	-.0395	-.0166	-.0092
-41.67	-4.13	-2.7186	.1112	-.1657	.0713	-.0240	-.0158
-41.64	-8.17	-2.6759	.1077	-.1742	.1644	-.0322	-.0247
-41.63	-10.20	-2.6465	.1053	-.1715	.2097	-.0364	-.0277
-41.61	-15.14	-2.5807	.0990	-.1982	.3361	-.0340	-.0321
-41.61	-20.19	-2.5725	.0933	-.2358	.4426	-.0212	-.0242
-41.41	-30.12	-2.1956	.0786	-.2242	.6238	-.0241	-.0601

RUN 303		Q=140.70 PSF		RN/FT= 3.282		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-41.41	-.20	-2.4298	.0224	.0922	-.0086	-.0094	.0081
-51.67	-.18	-2.5463	.0049	.1420	-.0406	-.0062	-.0029
-61.34	-.20	-2.5728	-.0029	.1872	-.0322	-.0041	.0009
-71.05	-.19	-2.5752	-.0206	.2565	-.0321	-.0038	.0004
-80.90	-.19	-2.5161	-.0445	.3845	-.0338	-.0039	.0002
-91.33	-.19	-2.4443	-.0640	.4900	-.0331	-.0026	.0007

APPENDIX - Continued

<div> <div>RUN 304</div> <div>Q=158.10 PSF</div> <div>RN/FT= 3.471</div> <div>MACH=0.20</div> </div>							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-80.93	9.76	-2.4433	-.0363	.4201	-.3604	-.0402	.0146
-80.93	7.74	-2.4840	-.0409	.4070	-.2929	-.0373	.0125
-80.93	3.76	-2.4993	-.0425	.3913	-.1579	-.0230	.0062
-80.93	-.17	-2.5203	-.0456	.3832	-.0362	-.0045	-.0004
-80.92	-4.20	-2.5181	-.0442	.3876	.0895	.0112	-.0074
-80.92	-8.19	-2.4870	-.0412	.3951	.2170	.0223	-.0117
-80.90	-10.09	-2.4608	-.0385	.4026	.2826	.0250	-.0158
-80.87	-15.13	-2.3722	-.0314	.4225	.4311	.0238	-.0208
-80.85	-20.09	-2.2733	-.0195	.3841	.5483	.0020	-.0258
-80.79	-29.96	-2.0229	-.0059	.2100	.7872	-.0703	-.0393
<div> <div>RUN 305</div> <div>Q=149.70 PSF</div> <div>RN/FT= 3.379</div> <div>MACH=0.20</div> </div>							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-61.23	-30.10	-2.0067	.0036	.1400	.7851	-.0094	-.0422
-61.30	-20.17	-2.2850	.0007	.1931	.5688	-.0032	-.0179
-61.35	-15.14	-2.4105	-.0052	.2014	.4515	.0151	-.0117
-61.40	-10.18	-2.4916	-.0054	.1844	.2819	.0130	-.0064
-61.41	-8.18	-2.5376	-.0054	.1821	.2209	.0141	-.0049
-61.43	-4.18	-2.5887	-.0041	.1852	.0915	.0092	-.0020
-61.47	-.15	-2.5814	-.0038	.1894	-.0395	-.0038	.0007
-61.48	3.84	-2.5710	-.0036	.1822	-.1753	-.0181	.0035
-61.49	9.85	-2.5010	-.0049	.1800	-.3668	-.0192	.0079
-61.44	7.81	-2.5212	-.0040	.1808	-.3011	-.0226	.0054

APPENDIX - Continued

RUN 306		Q=149.40 PSF		RN/FT= 3.380		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-41.52	9.81	-2.3794	.0150	.0642	-.3070	.0231	.0227
-41.48	7.80	-2.4045	.0198	.0534	-.2434	.0096	.0153
-41.47	3.82	-2.4186	.0223	.0798	-.1168	.0003	.0122
-41.46	-.14	-2.4306	.0228	.0932	-.0027	-.0088	.0076
-41.45	-4.15	-2.4017	.0193	.0640	.0783	-.0149	-.0082
-41.45	-8.12	-2.4102	.0136	.0494	.1810	-.0255	-.0178
-41.43	-10.14	-2.3942	.0017	.0513	.2302	-.0295	-.0284
-41.38	-15.16	-2.3030	.0054	.0705	.3772	-.0293	-.0368
-41.34	-20.17	-2.1838	.0036	.0131	.4958	-.0314	-.0366
-41.24	-30.11	-1.9779	-.0055	-.0168	.6571	-.0215	-.0934

RUN 307		Q=212.40 PSF		RN/FT= 4.986		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-42.02	-.19	-2.4833	.0105	.0948	-.0051	-.0012	.0011
-52.23	-.18	-2.5713	.0044	.1310	-.0106	.0026	.0005
-61.95	-.18	-2.5943	-.0038	.1722	-.0140	.0006	.0003
-66.81	-.18	-2.5827	-.0123	.2001	-.0200	-.0019	-.0003
-71.66	-.18	-2.5561	-.0216	.2537	-.0171	-.0015	.0001
-76.50	-.16	-2.5378	-.0331	.3162	-.0169	-.0044	.0005
-81.43	-.16	-2.5338	-.0440	.3738	-.0214	-.0046	.0002
-86.57	-.16	-2.4634	-.0559	.4140	-.0189	-.0052	.0012
-91.84	-.17	-2.4494	-.0626	.4448	-.0123	.0012	.0016

APPENDIX - Continued

RUN 308		Q=228.90 PSF		RN/FT= 5.142		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-81.48	9.79	-2.4659	-.0353	.3582	-.3161	-.0137	.0142
-81.47	7.78	-2.4941	-.0397	.3567	-.2594	-.0213	.0120
-81.45	3.79	-2.5085	-.0425	.3812	-.1400	-.0185	.0074
-81.43	-.21	-2.5261	-.0460	.3685	-.0157	-.0047	.0004
-81.42	-4.14	-2.5127	-.0448	.3712	.1019	.0108	-.0066
-81.38	-8.18	-2.4822	-.0388	.3675	.2164	.0142	-.0138
-81.37	-10.19	-2.4748	-.0367	.3755	.2777	.0132	-.0160
-81.35	-15.07	-2.3910	-.0295	.3923	.4345	.0131	-.0207
-81.31	-20.09	-2.2968	-.0166	.3243	.5347	-.0160	-.0274
-81.24	-30.01	-2.0104	-.0068	.1880	.7963	-.0733	-.0405

RUN 309		Q=216.10 PSF		RN/FT= 4.984		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-61.78	-30.21	-2.0403	-.0003	.0113	.7978	-.0220	-.0420
-61.83	-20.23	-2.2984	-.0005	.1613	.6025	.0026	-.0189
-61.90	-15.20	-2.4230	-.0033	.1678	.4386	.0009	-.0120
-61.96	-10.22	-2.5051	-.0055	.1762	.3052	.0216	-.0071
-61.99	-8.23	-2.5327	-.0046	.1769	.2480	.0198	-.0047
-61.99	-4.18	-2.5640	-.0047	.1762	.1100	.0106	-.0022
-62.00	-.18	-2.5778	-.0048	.1759	-.0211	.0006	.0008
-62.03	3.80	-2.5901	-.0046	.1641	-.1578	-.0142	.0031
-61.96	7.89	-2.5325	-.0046	.1566	-.3011	-.0235	.0058
-61.94	9.85	-2.5010	-.0040	.1596	-.3661	-.0259	.0080

APPENDIX - Continued

RUN 310		Q=206.70 PSF		RN/FT= 4.857		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-42.05	9.84	-2.4905	.0204	-.0181	-.2887	.0017	.0293
-42.01	7.85	-2.4592	.0200	.0101	-.2170	.0080	.0238
-41.95	3.81	-2.4366	.0208	.0512	-.1118	-.0017	.0124
-41.98	-.20	-2.4964	.0116	.0993	-.0010	-.0016	.0028
-41.97	-4.23	-2.4615	.0183	.0556	.0954	-.0044	-.0136
-42.01	-8.25	-2.4856	.0122	.0394	.1856	-.0096	-.0259
-42.04	-10.23	-2.4685	.0094	.0405	.2422	-.0138	-.0296
-42.03	-15.24	-2.3820	.0014	.0255	.3963	-.0176	-.0422
-42.00	-20.26	-2.2872	.0016	-.0488	.5062	-.0301	-.0415
-41.91	-30.33	-2.0163	-.0049	-.0668	.7248	.0023	-.0873

RUN 311		Q=218.00 PSF		RN/FT= 4.973		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-42.58	-.16	-2.8939	.1059	-.1916	-.0205	-.0060	-.0033
-52.40	-.15	-2.7085	.1038	-.0525	-.0290	-.0042	-.0031
-62.06	-.16	-2.6381	.1009	.1134	-.0290	-.0039	.0012
-66.83	-.16	-2.6317	.0969	.1959	-.0270	-.0024	.0011
-71.66	-.15	-2.6202	.0946	.2735	-.0230	-.0027	.0005
-76.59	-.14	-2.5858	.0876	.2941	-.0229	-.0033	.0016
-81.55	-.15	-2.5933	.0773	.3050	-.0220	-.0037	.0008
-86.63	-.16	-2.5472	.0681	.3324	-.0266	-.0023	.0013
-91.96	-.16	-2.5487	.0634	.3297	-.0165	.0016	.0006

APPENDIX - Continued

RUN 312		Q=229.80 PSF		RN/FT= 5.101		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-81.57	9.73	-2.5482	.0842	.3215	-.3371	-.0223	.0179
-81.56	7.83	-2.5633	.0833	.3255	-.2766	-.0227	.0137
-81.52	3.79	-2.5772	.0781	.3104	-.1501	-.0189	.0083
-81.52	-.22	-2.5768	.0765	.3020	-.0186	-.0038	.0006
-81.46	-4.13	-2.5671	.0774	.3091	.1022	.0102	-.0072
-81.38	-8.15	-2.5705	.0797	.3062	.2184	.0112	-.0149
-81.36	-10.18	-2.5381	.0810	.3290	.2824	.0121	-.0172
-81.34	-15.11	-2.4702	.0808	.3474	.4500	.0137	-.0238
-81.33	-20.12	-2.3768	.0834	.3149	.5695	-.0082	-.0288
-81.22	-30.01	-2.0731	.0762	.1505	.8108	-.0746	-.0430

RUN 313		Q = 211.50 PSF		RN/FT = 4.899		MACH = 0.20	
<u>ALPHA</u>	<u>BETA</u>	<u>C_N</u>	<u>C_A</u>	<u>C_m</u>	<u>C_y</u>	<u>C_n</u>	<u>C_l</u>
-61.81	-30.19	-2.0515	.0766	-.0332	.8064	-.0190	-.0460
-61.86	-20.23	-2.3516	.0927	.1249	.6024	.0042	-.0231
-61.92	-15.26	-2.4456	.0948	.1480	.4453	.0077	-.0164
-61.91	-10.20	-2.5637	.0974	.1384	.3042	.0164	-.0107
-61.94	- 8.22	-2.5683	.0973	.1249	.2390	.0171	-.0090
-61.98	- 4.15	-2.6255	.0979	.1165	.1045	.0087	-.0036
-62.00	-.14	-2.6297	.0989	.1165	-.0259	-.0024	.0008
-61.99	3.87	-2.6303	.1003	.1126	-.1673	-.0168	.0052
-61.98	7.90	-2.5660	.1003	.1228	-.3055	-.0263	.0107
-61.98	9.90	-2.5477	.1000	.1270	-.3736	-.0277	.0122

APPENDIX - Continued

RUN 314 Q=212.70 PSF RN/FT= 4.910 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-42.41	9.89	-2.7555	.1068	-.2754	-.3156	-.0006	.0192
-42.41	7.86	-2.7910	.1067	-.2352	-.2482	.0032	.0135
-42.41	3.83	-2.8245	.1075	-.2146	-.1518	.0049	.0125
-42.43	-.19	-2.8848	.1044	-.1898	-.0187	-.0061	-.0032
-42.35	-4.14	-2.7934	.1053	-.2001	.0995	-.0150	-.0141
-42.36	-8.20	-2.7793	.1027	-.2072	.2022	-.0195	-.0206
-42.35	-10.24	-2.7052	.1014	-.2018	.2484	-.0266	-.0271
-42.33	-15.23	-2.6291	.0956	-.2316	.3682	-.0257	-.0328
-42.38	-20.30	-2.6150	.0908	-.3031	.4773	-.0190	-.0155
-42.07	-30.28	-2.1916	.0755	-.2576	.6975	-.0051	-.0669

APPENDIX - Continued

<div> <div>RUN 315</div> <div>Q= 57.40 PSF</div> <div>RN/FT= 1.386</div> <div>MACH=0.20</div> </div>							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-41.01	-.25	-2.7440	.1098	-.1466	-.0249	-.0074	-.0056
-51.03	-.23	-2.6135	.1054	-.0576	-.0326	-.0058	-.0026
-60.67	-.22	-2.5957	.1042	.1117	-.0318	-.0016	.0009
-70.32	-.22	-2.5661	.0975	.2465	-.0231	.0014	.0007
-80.27	-.22	-2.5500	.0866	.3161	-.0248	.0001	0.0000
-90.72	-.22	-2.4744	.0726	.4089	-.0289	.0034	.0008
<div> <div>RUN 316</div> <div>Q= 55.20 PSF</div> <div>RN/FT= 1.353</div> <div>MACH=0.20</div> </div>							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-80.18	9.71	-2.4884	.0875	.3326	-.3430	-.0247	.0160
-80.17	7.77	-2.4852	.0876	.3280	-.2759	-.0232	.0138
-80.17	3.78	-2.5336	.0883	.3079	-.1400	-.0088	.0077
-80.18	-.22	-2.5422	.0856	.3065	-.0219	-.0005	.0009
-80.17	-4.17	-2.5491	.0873	.3158	.0973	.0142	-.0070
-80.16	-8.11	-2.5004	.0901	.3193	.2305	.0311	-.0146
-80.19	-10.09	-2.5369	.0992	.1575	.1704	-.0515	-.0144
-80.19	-15.00	-2.4972	.1032	.1683	.3237	-.0574	-.0208
-80.19	-20.04	-2.3792	.1049	.1258	.4806	-.0478	-.0268
-80.15	-29.89	-2.0788	.1011	.0648	.7879	-.0535	-.0402

APPENDIX - Continued

RUN 317 Q= 56.90 PSF RN/FT= 1.369 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-60.63	-29.93	-2.0837	.0918	-.2394	.7433	-.0379	-.0399
-60.67	-20.09	-2.3677	.1007	-.0903	.5247	-.0166	-.0205
-60.70	-15.07	-2.4643	.1005	-.0233	.4147	-.0015	-.0151
-60.70	-10.13	-2.5278	.1015	.0976	.2779	.0188	-.0109
-60.62	-8.18	-2.5540	.1012	.1080	.2267	.0197	-.0080
-60.65	-4.12	-2.5949	.1021	.1162	.0924	.0098	-.0031
-60.66	-.15	-2.6218	.1030	.1147	-.0349	-.0009	.0011
-60.68	3.77	-2.6008	.1029	.1161	-.1643	-.0134	.0049
-60.68	7.79	-2.5429	.1012	.1070	-.2989	-.0214	.0092
-60.68	9.79	-2.5320	.1003	.1087	-.3682	-.0263	.0110

RUN 318 Q= 57.60 PSF RN/FT= 1.374 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-40.92	9.80	-2.6424	.1059	-.2248	-.2984	-.0029	.0192
-40.93	7.79	-2.6659	.1062	-.2056	-.2472	-.0029	.0127
-40.92	3.75	-2.7185	.1081	-.1710	-.1399	-.0056	.0060
-40.92	-.16	-2.7459	.1072	-.1494	-.0272	-.0066	-.0037
-40.90	-4.23	-2.7063	.1076	-.1720	.0955	-.0061	-.0132
-40.89	-8.17	-2.6868	.1057	-.2163	.2048	-.0040	-.0209
-40.88	-10.15	-2.6537	.1041	-.2308	.2496	-.0027	-.0236
-40.95	-15.13	-2.6501	.1022	-.2648	.3746	.0251	-.0340
-40.91	-20.10	-2.5338	.0959	-.2597	.4191	-.0150	-.0360
-40.86	-30.02	-2.3229	.0816	-.3550	.5984	-.0352	-.0410

APPENDIX - Continued

RUN 319 Q= 59.00 PSF RN/FT= 1.387 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-40.86	-.18	-2.4205	.0128	.0937	-.0187	-.0051	.0042
-50.94	-.17	-2.5311	.0087	.1295	-.0350	-.0033	-.0035
-60.69	-.16	-2.5540	-.0017	.1587	-.0293	-.0018	.0007
-70.35	-.17	-2.5574	-.0180	.2292	-.0319	-.0016	-.0001
-80.27	-.16	-2.4876	-.0369	.3667	-.0278	-.0027	.0003
-90.72	-.18	-2.3973	-.0543	.4763	-.0319	-.0011	.0006
RUN 320 Q= 60.70 PSF RN/FT= 1.406 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-80.24	9.71	-2.4258	-.0298	.3714	-.3496	-.0322	.0151
-80.23	7.77	-2.4381	-.0324	.3634	-.2807	-.0283	.0114
-80.23	3.75	-2.4754	-.0357	.3614	-.1433	-.0167	.0082
-80.22	-.26	-2.4783	-.0382	.3605	-.0234	-.0022	.0003
-80.21	-4.13	-2.4568	-.0363	.3563	.0881	.0119	-.0055
-80.19	-8.13	-2.4383	-.0309	.3751	.2190	.0237	-.0117
-80.19	-10.11	-2.4158	-.0305	.3794	.2903	.0278	-.0142
-80.19	-15.08	-2.4077	-.0133	.1946	.3106	-.0620	-.0173
-80.17	-20.03	-2.3186	.0028	.1704	.4615	-.0525	-.0238
-80.18	-29.97	-2.0062	.0191	.1153	.7760	-.0568	-.0388

APPENDIX - Continued

RUN 321 Q= 59.40 PSF RN/FT= 1.390 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-60.66	-30.02	-2.0833	.0113	-.1941	.7409	-.0327	-.0370
-60.70	-20.07	-2.3230	.0014	.0454	.6099	.0378	-.0164
-60.70	-15.10	-2.3917	-.0001	.1051	.4554	.0295	-.0105
-60.72	-10.16	-2.4671	-.0021	.1341	.2887	.0236	-.0060
-60.72	-8.15	-2.5150	-.0023	.1394	.2225	.0215	-.0035
-60.74	-4.11	-2.5437	-.0024	.1530	.0873	.0117	-.0011
-60.76	-.15	-2.5404	-.0017	.1575	-.0326	-.0002	.0004
-60.77	3.76	-2.5380	-.0023	.1531	-.1594	-.0146	.0026
-60.78	7.82	-2.5104	-.0025	.1435	-.2918	-.0233	.0050
-60.72	9.79	-2.4925	-.0034	.1425	-.3522	-.0275	.0065

RUN 322 Q= 56.50 PSF RN/FT= 1.355 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-40.86	9.78	-2.3796	.0163	.0135	-.2858	-.0029	.0212
-40.85	7.80	-2.3895	.0173	.0339	-.2293	-.0041	.0164
-40.83	3.77	-2.4091	.0174	.0670	-.1072	-.0093	.0102
-40.83	-.21	-2.4079	.0105	.0977	-.0046	-.0053	.0023
-40.82	-4.21	-2.3877	.0156	.0559	.0864	.0009	-.0067
-40.82	-8.13	-2.3980	.0161	.0129	.2106	.0020	-.0126
-40.83	-10.18	-2.4260	.0157	-.0062	.2630	.0008	-.0189
-40.84	-15.13	-2.4398	.0168	-.0350	.3786	.0195	-.0404
-40.83	-20.06	-2.1922	.0134	-.0318	.4802	-.0273	-.0500
-40.78	-30.03	-2.0370	.0078	-.1315	.5962	-.0335	-.0929

APPENDIX - Continued

<div> <div>RUN 323</div> <div>Q= 23.00 PSF</div> <div>RN/FT= .573</div> <div>MACH=0.20</div> </div>							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-40.62	-.20	-2.4792	-.0044	.0979	-.0341	-.0010	-.0011
-50.74	-.18	-2.6597	-.0020	.0457	-.0317	-.0019	-.0017
-60.45	-.17	-2.6906	-.0075	-.0302	.0121	.0333	.0001
-65.31	-.17	-2.7334	-.0115	-.0516	-.0139	.0190	-.0005
-70.09	-.17	-2.7091	-.0124	.0038	-.0303	.0039	.0004
-74.99	-.16	-2.6795	-.0151	.1011	-.0285	.0033	.0004
-80.01	-.17	-2.6462	-.0227	.1516	-.0293	.0022	.0001
-85.14	-.17	-2.6011	-.0297	.2201	-.0335	.0029	-.0012
-90.50	-.17	-2.5653	-.0341	.3161	-.0303	.0046	-.0001
<div> <div>RUN 324</div> <div>Q= 24.00 PSF</div> <div>RN/FT= .582</div> <div>MACH=0.20</div> </div>							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-79.96	9.74	-2.5536	-.0071	.1872	-.2739	.0402	.0130
-79.98	7.78	-2.5893	-.0126	.1804	-.2277	.0274	.0117
-79.98	3.72	-2.6300	-.0183	.1670	-.1162	.0092	.0068
-79.97	-.22	-2.6264	-.0219	.1461	-.0195	.0024	.0002
-79.96	-4.19	-2.6267	-.0175	.1623	.0568	-.0015	-.0080
-79.95	-8.15	-2.5844	-.0145	.1817	.1484	-.0221	-.0117
-79.94	-10.15	-2.5504	-.0088	.1895	.1948	-.0340	-.0143
-79.92	-15.06	-2.4748	.0028	.1855	.3401	-.0442	-.0208
-79.90	-20.05	-2.3521	.0137	.1521	.5039	-.0325	-.0281
-79.97	-29.96	-1.9827	.0226	.0061	.8806	-.0491	-.0455

APPENDIX - Continued

RUN 325		Q= 23.70 PSF		RN/FT= .577		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-60.38	-29.99	-2.0428	.0012	-.3184	.8605	.0122	-.0413
-60.42	-20.06	-2.3884	.0063	-.1290	.5890	-.0019	-.0179
-60.46	-15.14	-2.4983	.0024	-.0693	.4505	.0139	-.0114
-60.48	-10.08	-2.6077	.0008	-.0339	.2589	.0032	-.0077
-60.49	-8.13	-2.6203	-.0012	-.0215	.1974	.0006	-.0053
-60.50	-4.16	-2.6570	-.0027	-.0336	.1006	.0148	-.0029
-60.46	-.16	-2.6968	-.0088	-.0343	.0145	.0324	-.0002
-60.46	3.79	-2.6565	-.0040	-.0285	-.0524	.0624	.0022
-60.47	7.76	-2.5900	-.0018	-.0761	-.1770	.0666	.0043
-60.48	9.74	-2.6121	.0015	-.0966	-.2426	.0651	.0057

RUN 326		Q= 23.80 PSF		RN/FT= .579		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-40.63	9.73	-2.4146	.0072	-.1500	-.2168	.0648	.0198
-40.63	7.75	-2.4168	.0079	-.0901	-.1974	.0468	.0185
-40.60	3.75	-2.4119	.0075	.0036	-.1008	.0303	.0082
-40.60	-.22	-2.4444	.0013	.0945	-.0184	-.0012	-.0011
-40.59	-4.13	-2.4119	.0115	.0166	.0653	-.0310	-.0076
-40.59	-8.09	-2.4159	.0114	-.0973	.1206	-.0555	-.0169
-40.58	-10.13	-2.3801	.0071	-.1363	.1712	-.0605	-.0191
-40.59	-15.10	-2.3803	.0151	-.3385	.2256	-.1058	-.0219
-40.58	-20.09	-2.3463	.0099	-.2189	.4965	-.0125	-.0552
-40.54	-29.92	-2.2167	.0334	-.5860	.4868	-.1107	-.0900

APPENDIX - Continued

<div> <div>RUN 327</div> <div>Q= 23.10 PSF</div> <div>RN/FT= .582</div> <div>MACH=0.20</div> </div>							
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-40.65	-.19	-2.7552	.0997	-.1778	-.0171	.0025	.0031
-50.70	-.16	-2.7020	.0993	-.1630	-.0262	-.0047	.0001
-60.42	-.18	-2.7022	.1035	-.0944	.0113	.0243	.0007
-70.05	-.17	-2.6921	.1066	.0190	-.0136	.0026	.0009
-79.96	-.16	-2.6666	.0988	.1187	-.0247	.0015	.0005
-90.46	-.17	-2.6081	.0854	.2514	-.0277	.0047	-.0007
<div> <div>RUN 328</div> <div>Q= 24.80 PSF</div> <div>RN/FT= .601</div> <div>MACH=0.20</div> </div>							
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-79.98	9.72	-2.5909	.1037	.1461	-.2872	.0353	.0170
-79.99	7.74	-2.6013	.1024	.1425	-.2321	.0269	.0129
-79.99	3.80	-2.6507	.1013	.1311	-.1175	.0067	.0079
-79.98	-.19	-2.6449	.0985	.1308	-.0298	.0019	.0010
-79.97	-4.14	-2.6506	.1005	.1294	.0555	-.0032	-.0065
-79.95	-8.13	-2.6294	.1030	.1515	.1554	-.0236	-.0117
-79.94	-10.13	-2.6099	.1033	.1524	.2006	-.0315	-.0162
-79.93	-15.08	-2.5265	.1038	.1514	.3621	-.0367	-.0218
-79.91	-19.99	-2.4245	.1091	.1390	.5277	-.0254	-.0306
-79.88	-29.90	-2.0817	.0982	-.0466	.8561	-.0565	-.0481

APPENDIX - Continued

RUN 329		Q= 24.90 PSF	RN/FT= .602		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-60.35	-29.95	-2.0672	.0879	-.3059	.8282	.0063	-.0463
-60.39	-20.07	-2.4008	.0985	-.1490	.5502	-.0104	-.0223
-60.41	-15.07	-2.5362	.0966	-.1319	.4063	.0028	-.0168
-60.43	-10.08	-2.6306	.0988	-.0830	.2295	-.0090	-.0105
-60.43	-8.00	-2.6500	.0986	-.0745	.1618	-.0102	-.0085
-60.44	-5.14	-2.6853	.0989	-.0713	.0978	-.0051	-.0036
-60.46	-.15	-2.7082	.0996	-.0820	-.0079	.0255	-.0009
-60.48	3.83	-2.6580	.0990	-.0604	-.0797	.0586	.0025
-60.49	7.76	-2.6337	.0989	-.1064	-.1961	.0598	.0068
-60.49	9.78	-2.6004	.0980	-.1359	-.2679	.0555	.0097

RUN 330		Q= 23.10 PSF	RN/FT= .581		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-40.66	9.77	-2.7564	.0927	-.4526	-.2149	.0574	.0166
-40.64	7.75	-2.7396	.0955	-.3926	-.1735	.0472	.0149
-40.65	3.77	-2.8055	.0983	-.3007	-.0751	.0330	.0089
-40.62	-.15	-2.7730	.1003	-.1768	-.0179	.0019	.0019
-40.61	-4.12	-2.7494	.0982	-.2554	.0340	-.0304	-.0112
-40.61	-8.12	-2.7696	.0931	-.3973	.1004	-.0482	-.0143
-40.60	-10.08	-2.7269	.0925	-.4238	.1540	-.0564	-.0182
-40.63	-15.03	-2.7720	.0865	-.6278	.1997	-.1010	-.0139
-40.49	-20.00	-2.4197	.0974	-.4531	.4611	-.0443	-.0427
-40.56	-29.89	-2.4569	.0778	-.9550	.4512	-.1453	-.0378

APPENDIX - Continued

RUN 331		Q= 13.10 PSF		RN/FT= .328		MACH=0.20		
SEQ	ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
4	-40.57	-.17	-2.8208	.0903	-.2880	-.0166	-.0005	-.0031
5	-50.65	-.15	-2.8878	.0921	-.3963	-.0260	.0214	-.0097
6	-60.33	-.15	-2.7732	.0881	-.3265	-.0219	.0242	-.0012
7	-65.11	-.13	-2.7427	.1019	-.1378	-.0383	.0024	-.0001
8	-69.97	-.14	-2.7086	.1084	.0063	-.0548	.0007	-.0004
9	-74.83	-.13	-2.6860	.1042	.0616	-.0526	.0007	-.0009
10	-79.85	-.13	-2.6880	.0990	.1076	-.0542	.0010	-.0016
11	-85.01	-.14	-2.6779	.0901	.1478	-.0567	.0020	-.0014
12	-90.32	-.12	-2.6644	.0828	.2185	-.0506	.0038	-.0022

RUN 332		Q= 15.00 PSF		RN/FT= .354		MACH=0.20		
SEQ	ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
1	-90.35	-.15	-2.5351	-.0293	.2847	-.0437	.0031	.0010
2	-85.04	-.14	-2.5590	-.0266	.1955	-.0406	.0021	.0006
3	-79.88	-.12	-2.5943	-.0164	.1221	-.0414	.0007	.0001
4	-74.88	-.12	-2.6000	-.0065	.0684	-.0427	.0015	-.0006
5	-69.99	-.13	-2.6421	-.0017	-.0238	-.0359	.0015	.0006
6	-65.13	-.12	-2.6519	-.0053	-.1503	-.0312	.0020	.0002
7	-60.38	-.13	-2.7122	-.0233	-.2395	-.0073	.0341	-.0023
8	-50.68	-.14	-2.7297	-.0163	-.1927	-.0051	.0179	-.0026
9	-40.48	-.14	-2.4739	-.0065	-.0089	-.0286	-.0009	.0027

APPENDIX - Continued

RUN 333		Q= 56.40 PSF		RN/FT= 1.357		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-40.83	-.15	-2.4064	.0254	.1127	-.0622	.0260	-.0043
-50.96	-.16	-2.5315	.0216	.1403	-.0791	.0275	-.0100
-60.68	-.14	-2.5493	.0131	.1671	-.0785	.0259	-.0075
-65.50	-.13	-2.5812	.0036	.2023	-.0785	.0235	-.0068
-70.34	-.15	-2.5584	-.0048	.2399	-.0687	.0221	-.0068
-75.20	-.15	-2.5252	-.0147	.2859	-.0604	.0166	-.0046
-80.21	-.14	-2.4968	-.0265	.3740	-.0587	.0122	-.0043
-85.33	-.13	-2.4466	-.0382	.4248	-.0550	.0106	-.0027
-90.67	-.12	-2.4135	-.0422	.4974	-.0526	.0116	-.0055

RUN 334		Q= 56.60 PSF		RN/FT= 1.346		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-80.18	9.72	-2.4073	-.0189	.3775	-.3587	-.0248	.0119
-80.17	7.73	-2.4439	-.0212	.3732	-.2955	-.0166	.0089
-80.16	3.78	-2.4648	-.0229	.3733	-.1685	-.0010	.0021
-80.14	-.19	-2.4917	-.0267	.3708	-.0558	.0120	-.0047
-80.14	-4.14	-2.4760	-.0242	.3738	.0561	.0271	-.0105
-80.13	-8.13	-2.4356	-.0210	.3810	.1849	.0396	-.0176
-80.12	-10.14	-2.4169	-.0197	.3852	.2612	.0457	-.0195
-80.12	-15.08	-2.4141	-.0058	.1797	.2760	-.0428	-.0236
-80.10	-20.03	-2.2982	.0098	.1444	.4374	-.0372	-.0310
-80.05	-29.97	-2.0261	.0235	.1106	.7434	-.0389	-.0452

APPENDIX - Continued

RUN 335		Q= 55.20 PSF	RN/FT= 1.325		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-60.62	-30.01	-2.0776	.0177	-.2582	.6983	-.0235	-.0426
-60.65	-20.08	-2.3179	.0062	.0267	.5877	.0621	-.0224
-60.65	-15.14	-2.4072	.0075	.1037	.4373	.0481	-.0159
-60.69	-10.11	-2.4828	.0082	.1363	.2471	.0427	-.0120
-60.69	-8.14	-2.5172	.0117	.1512	.1772	.0452	-.0115
-60.71	-4.15	-2.5431	.0141	.1642	.0457	.0364	-.0094
-60.73	-.19	-2.5357	.0146	.1680	-.0848	.0248	-.0081
-60.75	3.79	-2.5501	.0110	.1634	-.2017	.0106	-.0047
-60.71	7.79	-2.5183	.0102	.1560	-.3318	.0003	-.0023
-60.71	9.78	-2.4759	.0098	.1469	-.3862	-.0086	.0007

RUN 336		Q= 57.50 PSF	RN/FT= 1.345		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-40.84	9.78	-2.4078	.0320	.0307	-.3354	.0203	.0159
-40.84	7.79	-2.4191	.0323	.0510	-.2905	.0264	.0085
-40.82	3.82	-2.4153	.0322	.0803	-.1654	.0209	.0030
-40.80	-.17	-2.3997	.0269	.1129	-.0626	.0252	-.0053
-40.80	-4.15	-2.4021	.0328	.0783	.0321	.0301	-.0158
-40.80	-8.17	-2.4142	.0315	.0289	.1669	.0262	-.0198
-40.79	-10.13	-2.3963	.0273	.0102	.2216	.0186	-.0243
-40.77	-15.07	-2.3272	.0209	-.0188	.3412	.0085	-.0491
-40.74	-20.06	-2.2251	.0021	-.0756	.4497	-.0108	-.0522
-40.67	-30.00	-2.0166	.0170	-.1416	.5659	-.0123	-.0999

APPENDIX - Continued

RUN 337		Q= 23.70 PSF		RN/FT= .580		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-40.57	-.19	-2.4338	.0096	.1062	-.0727	.0252	-.0083
-50.72	-.18	-2.5807	.0110	.0664	-.0658	.0249	-.0080
-60.42	-.17	-2.6476	.0025	-.0271	-.0244	.0514	-.0056
-65.26	-.16	-2.6674	.0003	-.0516	-.0453	.0379	-.0056
-70.06	-.16	-2.6831	-.0002	.0048	-.0563	.0245	-.0049
-74.94	-.15	-2.6432	-.0036	.1046	-.0563	.0205	-.0040
-79.95	-.15	-2.6098	-.0129	.1600	-.0521	.0167	-.0046
-85.09	-.16	-2.5841	-.0212	.2217	-.0500	.0144	-.0032
-90.48	-.16	-2.5480	-.0285	.3145	-.0432	.0138	-.0023

RUN 338		Q= 25.10 PSF		RN/FT= .593		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-79.94	9.75	-2.5161	-.0011	.1848	-.2709	.0484	.0122
-79.95	7.75	-2.5515	-.0040	.1810	-.2310	.0400	.0089
-79.94	3.79	-2.5912	-.0106	.1666	-.1410	.0237	.0020
-79.95	-.17	-2.6068	-.0130	.1567	-.0518	.0177	-.0039
-79.95	-4.14	-2.5834	-.0104	.1673	.0377	.0126	-.0123
-79.93	-8.10	-2.5637	-.0084	.1882	.1262	-.0069	-.0158
-79.93	-10.09	-2.5339	-.0065	.1874	.1753	-.0178	-.0185
-79.92	-15.06	-2.4570	.0034	.1736	.3186	-.0258	-.0256
-79.94	-19.99	-2.3333	.0147	.1420	.4917	-.0179	-.0322
-79.90	-29.94	-1.9576	.0219	.0020	.8523	-.0314	-.0497

APPENDIX - Continued

RUN 339		Q= 25.50 PSF		RN/FT= .600		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-60.37	-29.97	-1.9948	.0049	-.3070	.8447	.0328	-.0445
-60.44	-20.06	-2.3623	.0064	-.1392	.5461	.0175	-.0214
-60.45	-15.09	-2.4951	.0078	-.0602	.4204	.0336	-.0165
-60.46	-10.11	-2.5941	.0061	-.0247	.2345	.0216	-.0124
-60.46	-8.12	-2.6297	.0067	-.0132	.1601	.0227	-.0116
-60.46	-4.14	-2.6723	.0086	-.0211	.0503	.0384	-.0106
-60.46	-.17	-2.6772	.0008	-.0280	-.0345	.0539	-.0059
-60.45	3.78	-2.6394	.0045	-.0147	-.1012	.0867	-.0038
-60.42	7.76	-2.6177	.0070	-.0575	-.2275	.0907	-.0022
-60.43	9.73	-2.5901	.0075	-.0797	-.2836	.0820	.0001

RUN 340		Q= 26.20 PSF		RN/FT= .611		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-40.61	9.72	-2.3991	.0171	-.1181	-.2804	.0783	.0162
-40.60	7.75	-2.3842	.0178	-.0681	-.2527	.0723	.0115
-40.58	3.79	-2.3973	.0165	.0136	-.1614	.0609	.0007
-40.58	-.07	-2.4374	.0120	.1119	-.0737	.0253	-.0102
-40.56	-4.13	-2.3764	.0216	.0397	.0270	.0006	-.0122
-40.59	-8.09	-2.3857	.0165	-.0682	.1034	-.0288	-.0218
-40.60	-10.11	-2.3851	.0129	-.1087	.1686	-.0339	-.0253
-40.60	-15.04	-2.3549	.0100	-.2369	.2802	-.0511	-.0357
-40.59	-20.05	-2.3280	.0045	-.1979	.4927	.0132	-.0538
-40.55	-29.94	-2.1681	.0249	-.5266	.5085	-.0695	-.0918

APPENDIX - Continued

RUN 341 Q= 25.00 PSF RN/FT= .593 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-40.54	-.19	-2.1688	.0133	-.0106	-.0714	.0046	.0365
-50.70	-.17	-2.3947	.0083	-.0711	-.0796	.0031	.0330
-60.47	-.17	-2.5047	.0010	-.1316	-.0415	.0316	.0363
-70.13	-.16	-2.5282	-.0056	-.0876	-.0721	.0091	.0308
-79.99	-.17	-2.4883	-.0174	.0638	-.0655	.0065	.0256
-90.49	-.16	-2.3947	-.0362	.2199	-.0716	.0097	.0185

RUN 342 Q= 27.40 PSF RN/FT= .619 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-80.00	9.72	-2.3583	-.0064	.0668	-.3176	.0540	.0384
-80.01	7.74	-2.4041	-.0083	.0715	-.2700	.0416	.0355
-80.01	3.80	-2.4503	-.0120	.0679	-.1706	.0179	.0308
-80.01	-.17	-2.4749	-.0173	.0564	-.0714	.0074	.0255
-79.99	-4.13	-2.4694	-.0175	.0772	.0224	.0018	.0194
-79.98	-8.13	-2.4545	-.0156	.1158	.1076	-.0232	.0160
-79.97	-10.09	-2.4297	-.0133	.1174	.1634	-.0326	.0152
-79.95	-15.03	-2.3514	-.0096	.1155	.3162	-.0412	.0074
-79.93	-20.05	-2.2492	-.0024	.1157	.4915	-.0302	-.0007
-79.90	-29.95	-1.8882	.0010	-.0262	.8660	-.0438	-.0223

APPENDIX - Continued

RUN 343		Q= 27.90 PSF		RN/FT= .627		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-60.38	-29.98	-1.9120	-.0107	-.3360	.8415	.0157	-.0145
-60.42	-20.07	-2.2465	-.0004	-.1741	.5512	.0026	.0176
-60.44	-15.08	-2.3607	.0009	-.1113	.4092	.0191	.0206
-60.45	-10.11	-2.4370	.0009	-.0820	.2243	.0126	.0255
-60.45	-8.11	-2.4696	.0002	-.0786	.1604	.0108	.0280
-60.47	-4.17	-2.5097	.0015	-.0929	.0441	.0223	.0315
-60.48	-.18	-2.4999	.0004	-.1119	-.0522	.0402	.0353
-60.48	3.75	-2.4541	.0038	-.1213	-.1291	.0674	.0382
-60.50	7.74	-2.4439	.0074	-.1744	-.2618	.0703	.0410
-60.50	9.70	-2.4047	.0105	-.1936	-.3305	.0679	.0427

RUN 344		Q= 26.60 PSF		RN/FT= .616		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
-40.56	9.72	-2.1280	.0180	-.2599	-.3505	.0563	.0561
-40.55	7.77	-2.1313	.0192	-.2057	-.3004	.0430	.0527
-40.55	3.83	-2.1686	.0193	-.1022	-.1810	.0340	.0467
-40.54	-.15	-2.2054	.0133	-.0038	-.0806	.0043	.0357
-40.53	-4.13	-2.1990	.0195	-.0604	.0242	-.0210	.0325
-40.55	-8.10	-2.2086	.0122	-.1644	.1101	-.0406	.0207
-40.54	-10.12	-2.1944	.0093	-.1919	.1666	-.0410	.0125
-40.53	-15.03	-2.1533	.0100	-.2993	.2707	-.0673	.0161
-40.51	-20.05	-2.0695	.0174	-.2453	.4826	.0045	-.0118
-40.51	-29.96	-2.0632	.0178	-.5118	.5300	-.0794	-.0374

APPENDIX - Continued

RUN 345		Q= 56.90 PSF		RN/FT= 1.319		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-40.74	-.21	-2.1475	.0308	-.0181	-.0676	-.0025	.0458
-50.87	-.20	-2.3260	.0252	.0029	-.0775	.0004	.0461
-60.64	-.21	-2.3724	.0171	.0690	-.0744	.0025	.0446
-70.30	-.19	-2.4221	-.0027	.1437	-.0707	.0024	.0391
-80.22	-.21	-2.3703	-.0295	.2711	-.0643	-.0010	.0314
-90.69	-.20	-2.3204	-.0504	.4071	-.0628	.0028	.0229

RUN 346		Q= 61.60 PSF		RN/FT= 1.367		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-80.18	9.73	-2.2725	-.0191	.2589	-.4042	-.0286	.0451
-80.18	7.75	-2.3100	-.0201	.2574	-.3356	-.0263	.0428
-80.18	3.81	-2.3546	-.0239	.2648	-.1927	-.0133	.0371
-80.17	-.14	-2.3719	-.0291	.2732	-.0625	-.0010	.0322
-80.17	-4.21	-2.3834	-.0317	.2817	.0618	.0149	.0247
-80.16	-8.13	-2.3484	-.0322	.3054	.1978	.0275	.0185
-80.15	-10.14	-2.3225	-.0312	.3163	.2672	.0343	.0155
-80.19	-15.05	-2.3200	-.0219	.1538	.3239	-.0453	.0105
-80.15	-20.04	-2.2261	-.0104	.1482	.4840	-.0364	.0019
-80.08	-29.92	-1.9514	-.0011	.0817	.7906	-.0533	-.0175

APPENDIX - Continued

RUN 347		Q= 57.00 PSF		RN/FT= 1.314		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-60.64	-29.95	-1.9967	-.0018	-.3131	.7450	-.0357	-.0138
-60.67	-20.06	-2.1943	-.0014	-.0087	.6069	.0399	.0195
-60.66	-15.07	-2.2556	.0054	.0486	.4414	.0348	.0284
-60.65	-10.13	-2.3392	.0118	.0651	.2611	.0256	.0355
-60.65	-8.12	-2.3588	.0145	.0682	.1883	.0234	.0383
-60.67	-4.12	-2.3763	.0189	.0695	.0484	.0147	.0432
-60.67	-.17	-2.3674	.0208	.0674	-.0822	.0035	.0465
-60.68	3.79	-2.3620	.0189	.0557	-.2162	-.0097	.0479
-60.69	7.79	-2.3269	.0137	.0362	-.3436	-.0192	.0468
-60.70	9.79	-2.3193	.0125	.0306	-.4141	-.0262	.0487

RUN 348		Q= 56.80 PSF		RN/FT= 1.310		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
-40.74	9.78	-2.0997	.0344	-.1150	-.3644	.0019	.0568
-40.74	7.77	-2.1073	.0341	-.0937	-.3093	.0018	.0519
-40.75	3.83	-2.1231	.0357	-.0558	-.1834	-.0048	.0423
-40.74	-.18	-2.1587	.0323	-.0138	-.0616	-.0013	.0473
-40.73	-4.15	-2.1249	.0334	-.0318	.0362	.0070	.0413
-40.73	-8.11	-2.1302	.0370	-.0702	.1513	.0082	.0338
-40.72	-10.17	-2.1148	.0379	-.0778	.2080	.0012	.0256
-40.71	-15.07	-2.1017	.0231	-.1024	.3510	-.0008	.0072
-40.70	-20.08	-1.9818	.0224	-.0867	.4543	-.0222	-.0169
-40.69	-29.90	-1.9084	.0141	-.1253	.5706	-.0259	-.0475

APPENDIX - Continued

RUN 349 Q= 57.10 PSF RN/FT= 1.331 MACH=0.20							
ALPHA	BETA	CN	CA	CLM	CY	CLN	CLL
-40.79	-.20	-2.3053	-.0099	.0563	-.0051	-.0045	.0010
-50.93	-.16	-2.4408	-.0124	.0865	-.0258	-.0025	-.0062
-60.64	-.16	-2.5052	-.0223	.1256	-.0271	-.0014	-.0010
-65.50	-.16	-2.5178	-.0311	.1543	-.0251	-.0013	-.0010
-70.34	-.16	-2.5190	-.0402	.1949	-.0299	.0005	-.0014
-75.22	-.16	-2.4708	-.0491	.2396	-.0268	.0001	-.0020
-80.23	-.15	-2.4429	-.0599	.3292	-.0265	-.0026	-.0005
-85.32	-.16	-2.4186	-.0681	.3975	-.0255	-.0004	-.0004
-90.68	-.15	-2.3832	-.0739	.4638	-.0229	.0028	.0004

RUN 350 Q= 24.50 PSF RN/FT= .577 MACH=0.20							
ALPHA	BETA	CN	CA	CLM	CY	CLN	CLL
-40.45	-.21	-2.3179	-.0178	.0506	-.0090	-.0016	-.0011
-50.76	-.17	-2.5000	-.0202	-.0010	-.0237	-.0069	-.0028
-60.46	-.17	-2.5994	-.0261	-.0686	.0218	.0281	-.0003
-65.28	-.18	-2.6108	-.0276	-.1006	-.0001	.0129	-.0006
-70.05	-.17	-2.6107	-.0312	-.0354	-.0169	.0028	-.0003
-74.97	-.17	-2.5759	-.0347	.0633	-.0122	.0020	-.0008
-80.02	-.16	-2.5664	-.0437	.1126	-.0128	.0016	0.0000
-85.11	-.16	-2.5279	-.0496	.1875	-.0183	.0016	-.0004
-90.45	-.17	-2.4912	-.0589	.2667	-.0258	.0046	.0004

APPENDIX - Continued

RUN 351 Q= 56.40 PSF RN/FT= 1.324 MACH=0.20							
ALPHA	BETA	CN	CA	CLM	CY	CLN	CLL
-40.76	-.19	-2.1580	-.0342	-.0761	-.0035	-.0041	-.0005
-50.91	-.18	-2.3656	-.0390	.0005	-.0199	-.0026	-.0045
-60.70	-.16	-2.4443	-.0505	.0587	-.0240	-.0017	-.0009
-65.51	-.17	-2.4747	-.0588	.1036	-.0240	-.0014	-.0011
-70.34	-.17	-2.4678	-.0674	.1555	-.0249	.0019	-.0018
-75.19	-.16	-2.4637	-.0777	.2124	-.0248	-.0002	-.0014
-80.15	-.16	-2.4240	-.0885	.3100	-.0241	-.0024	.0000
-85.34	-.17	-2.3898	-.0987	.3745	-.0234	.0004	.0002
-90.67	-.17	-2.3765	-.1062	.4501	-.0253	.0026	.0008

RUN 352 Q= 24.70 PSF RN/FT= .587 MACH=0.20							
ALPHA	BETA	CN	CA	CLM	CY	CLN	CLL
-40.59	-.20	-2.2092	-.0447	-.0844	-.0115	-.0015	-.0021
-50.74	-.16	-2.4734	-.0506	-.0806	-.0248	-.0071	-.0023
-60.44	-.18	-2.5444	-.0561	-.1377	.0156	.0274	-.0008
-65.23	-.17	-2.5822	-.0586	-.1414	-.0115	.0160	-.0011
-70.09	-.17	-2.6103	-.0618	-.0723	-.0232	.0027	-.0008
-74.92	-.16	-2.5692	-.0652	.0346	-.0195	.0022	.0002
-79.98	-.17	-2.5587	-.0723	.0904	-.0227	.0029	-.0013
-85.11	-.15	-2.5342	-.0803	.1740	-.0234	.0033	-.0003
-90.42	-.16	-2.4901	-.0869	.2777	-.0241	.0046	-.0005

APPENDIX - Continued

RUN 353	Q= 24.70 PSF	RN/FT= .597	MACH=0.20				
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.45	.18	2.0249	-.0532	-.1748	.0132	.0214	-.0046
50.63	.16	2.2468	-.0827	-.2020	.0131	.0389	-.0089
60.38	.18	2.3741	-.1115	-.1272	.0559	.0370	-.0111
70.06	.15	2.3918	-.1326	-.0602	.0387	.0188	-.0021
79.92	.16	2.3711	-.1228	-.2967	.0036	-.0013	.0003
90.42	.17	2.2306	-.1227	-.4657	.0102	.0004	-.0003

RUN 354	Q= 24.00 PSF	RN/FT= .586	MACH=0.20				
ALPHA	BETA	CN	CA	CLM	CY	CLN	CLL
79.92	-9.71	2.3338	-.1183	-.3620	-.0127	-.0132	.0242
79.93	-7.76	2.3535	-.1191	-.3670	-.0134	-.0187	.0190
79.93	-3.80	2.3525	-.1199	-.3498	-.0128	-.0115	.0092
79.92	.16	2.3824	-.1250	-.2997	.0092	.0008	-.0004
79.91	4.16	2.3639	-.1189	-.3510	.0463	.0118	-.0110
79.90	8.13	2.3369	-.1154	-.3654	.0546	.0138	-.0196
79.89	10.08	2.3267	-.1148	-.3566	.0509	.0140	-.0245
79.92	15.05	2.2865	-.1119	-.3425	.0054	-.0006	-.0354
79.91	20.01	2.2421	-.1027	-.3295	-.0589	-.0230	-.0444
79.89	29.92	2.1503	-.0929	-.3104	-.2171	-.0803	-.0617

APPENDIX - Continued

RUN 355		Q= 25.30 PSF		RN/FT= .604		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.44	29.95	2.3591	-.1067	.1526	-.2351	-.0720	-.0782
60.43	20.00	2.3892	-.1146	.1039	-.0315	-.0359	-.0356
60.43	15.03	2.3892	-.1157	.0645	.0675	.0067	-.0272
60.44	10.05	2.4387	-.1243	.0362	.1039	.0385	-.0178
60.43	8.11	2.4174	-.1253	.0131	.1109	.0446	-.0134
60.44	4.14	2.4017	-.1208	-.0351	.1125	.0708	-.0179
60.45	.15	2.3619	-.1171	-.1247	.0605	.0356	-.0114
60.45	-3.79	2.4172	-.1216	-.0792	-.0870	-.0549	.0156
60.47	-7.75	2.4375	-.1241	.0486	-.0900	-.0641	.0182
60.48	-9.72	2.4529	-.1251	.0335	-.0472	-.0273	.0155

RUN 356		Q= 25.60 PSF		RN/FT= .611		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.53	-9.73	2.0625	-.0665	-.0077	.0289	-.0236	.0322
40.51	-7.73	2.0323	-.0656	-.0511	.0630	-.0158	.0205
40.47	-3.79	1.9655	-.0608	-.1390	.0644	-.0209	.0086
40.47	.13	2.0114	-.0627	-.1773	.0151	.0232	-.0047
40.45	4.15	1.9815	-.0649	-.1177	-.0334	.0429	-.0039
40.53	8.12	2.0050	-.0654	-.0185	-.0018	.0468	-.0235
40.53	10.11	2.0295	-.0660	.0230	.0012	.0512	-.0286
40.53	15.06	2.0198	-.0695	.1357	-.0532	.0562	-.0425
40.54	20.02	2.0369	-.0751	.2500	-.0974	.0408	-.0498
40.59	29.90	2.1326	-.0943	.4773	-.1551	.0340	-.0860

APPENDIX - Continued

RUN 357 Q=130.40 PSF RN/FT= 3.013 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
41.29	30.13	2.0947	-.0880	-.1464	-.3702	-.0762	-.0971
51.46	30.07	2.3064	-.1039	-.2368	-.2729	-.0924	-.0965
61.18	30.00	2.2320	-.1012	-.2546	-.2402	-.0828	-.0734
70.72	29.98	2.0658	-.1001	-.4566	-.2607	-.0928	-.0560
80.62	29.93	2.1179	-.1045	-.5337	-.2192	-.0703	-.0617
91.06	29.88	2.1146	-.1090	-.6223	-.1866	-.0414	-.0702

RUN 358 Q= 57.00 PSF RN/FT= 1.376 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.68	30.01	1.8322	-.0808	-.1324	-.3737	-.0694	-.1004
50.91	29.96	2.2637	-.0978	-.2057	-.2127	-.0840	-.1007
60.65	29.94	2.2105	-.0974	-.1810	-.2296	-.0783	-.0744
70.24	29.97	2.0536	-.0987	-.4357	-.3614	-.1674	-.0553
80.11	29.92	2.0777	-.0903	-.4192	-.2480	-.0983	-.0595
90.60	29.89	2.0811	-.0897	-.5074	-.2198	-.0663	-.0677

APPENDIX - Continued

RUN 359		Q= 89.60 PSF	RN/FT= 2.171		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.93	-9.76	2.0728	-.0685	-.1841	.0703	.0346	.0214
40.86	-7.80	1.9880	-.0664	-.1810	.1046	.0142	.0239
40.84	-3.81	1.9491	-.0619	-.2232	.0765	-.0048	.0091
40.83	.17	1.9979	-.0619	-.2333	-.0256	.0093	-.0014
40.82	4.12	1.9768	-.0620	-.2098	-.0723	.0027	-.0127
40.85	8.15	2.0191	-.0654	-.1712	-.0864	-.0173	-.0223
40.87	10.15	2.0715	-.0664	-.1767	-.0485	-.0254	-.0213
40.89	15.09	2.1332	-.0686	-.1798	-.0516	-.0342	-.0348
40.88	20.05	2.0906	-.0674	-.1891	-.1258	-.0531	-.0642
40.87	30.07	2.0171	-.0851	-.2197	-.3276	-.1073	-.1017

RUN 360		Q= 94.00 PSF	RN/FT= 2.213		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.87	30.00	2.2173	-.0974	-.2872	-.2524	-.0731	-.0786
60.87	20.06	2.2670	-.0972	-.2641	-.1135	-.0373	-.0381
60.86	15.05	2.2690	-.0961	-.2690	-.0701	-.0307	-.0272
60.87	10.14	2.2447	-.0970	-.2688	-.0462	-.0213	-.0137
60.87	8.14	2.2585	-.0980	-.2855	-.0154	-.0080	-.0100
60.85	4.14	2.2371	-.0991	-.3298	.0240	.0107	-.0038
60.84	.16	2.2100	-.1011	-.3799	-.0023	-.0056	-.0010
60.86	-3.78	2.2240	-.1003	-.3775	-.0062	-.0117	.0044
60.90	-7.78	2.2662	-.1002	-.3114	.0259	.0102	.0094
60.92	-9.80	2.2668	-.1002	-.2925	.0370	.0203	.0135

APPENDIX - Continued

RUN 361							
Q= 98.30 PSF RN/FT= 2.252 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.34	-9.78	2.2153	-.1149	-.6226	.1060	.0528	.0216
80.33	-7.78	2.2164	-.1149	-.6278	.0849	.0458	.0178
80.31	-3.80	2.1974	-.1162	-.6364	.0579	.0282	.0090
80.32	.14	2.2268	-.1160	-.6063	.0245	.0069	.0004
80.30	4.12	2.2206	-.1125	-.6175	-.0397	-.0207	-.0099
80.30	8.11	2.2117	-.1107	-.6216	-.0913	-.0411	-.0170
80.31	10.10	2.2217	-.1098	-.6160	-.1181	-.0502	-.0226
80.29	15.07	2.1931	-.1070	-.6416	-.1831	-.0709	-.0348
80.28	20.04	2.1540	-.1053	-.6656	-.2414	-.0827	-.0461
80.27	29.98	2.0730	-.0997	-.5709	-.2449	-.0558	-.0637

RUN 362							
Q= 57.60 PSF RN/FT= 1.431 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.95	-9.75	2.0496	-.0707	-.1640	.0754	.0351	.0223
40.93	-7.76	1.9882	-.0684	-.1676	.0940	.0157	.0214
40.90	-3.81	1.9560	-.0647	-.2147	.0652	-.0004	.0104
40.89	.15	1.9662	-.0637	-.2295	-.0287	.0091	-.0027
40.90	4.13	1.9716	-.0643	-.1996	-.0565	.0040	-.0134
40.90	8.11	2.0045	-.0688	-.1319	-.0858	-.0165	-.0232
40.91	10.12	2.0478	-.0707	-.1214	-.0829	-.0303	-.0258
40.93	15.07	2.1283	-.0701	-.1633	-.0291	-.0327	-.0281
40.91	20.05	2.1032	-.0703	-.1616	-.0823	-.0464	-.0613
40.86	30.04	1.8702	-.0865	-.1520	-.3237	-.0951	-.0989

APPENDIX - Continued

RUN 363		Q= 59.20 PSF		RN/FT= 1.393		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.61	30.00	2.1874	-.1000	-.1709	-.2467	-.0733	-.0728
60.60	20.10	2.1673	-.0936	-.2510	-.2163	-.0913	-.0362
60.62	15.11	2.2447	-.1027	-.1781	-.1416	-.0694	-.0238
60.62	10.07	2.2690	-.1030	-.2278	-.0563	-.0311	-.0139
60.61	8.13	2.2378	-.1019	-.2515	-.0251	-.0170	-.0098
60.62	4.16	2.2414	-.1021	-.2931	.0204	.0043	-.0033
60.61	.18	2.2064	-.1012	-.3478	.0037	-.0043	-.0010
60.63	-3.81	2.2478	-.1021	-.3203	-.0089	-.0081	.0014
60.65	-7.81	2.2549	-.1026	-.2810	.0250	.0151	.0083
60.66	-9.79	2.2400	-.1027	-.2515	.0519	.0273	.0122

RUN 364		Q= 59.40 PSF		RN/FT= 1.385		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.15	-9.76	2.2686	-.1127	-.4550	-.0181	-.0253	.0251
80.14	-7.77	2.2697	-.1125	-.4658	-.0330	-.0326	.0200
80.12	-3.80	2.2393	-.1120	-.4978	-.0003	-.0132	.0094
80.10	.17	2.2345	-.1168	-.5563	.0040	.0087	-.0007
80.09	4.13	2.2372	-.1133	-.5689	-.0407	-.0195	-.0101
80.09	8.14	2.2442	-.1073	-.5037	.0025	.0109	-.0208
80.08	10.08	2.2336	-.1071	-.5003	-.0247	.0019	-.0230
80.07	15.08	2.2171	-.1042	-.4828	-.0983	-.0238	-.0339
80.07	20.04	2.1982	-.1009	-.4820	-.1984	-.0606	-.0437
80.08	29.95	2.1023	-.0926	-.3968	-.2788	-.0805	-.0611

APPENDIX - Continued

RUN 365		Q= 24.20 PSF		RN/FT= .590		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.53	-9.70	2.0978	-.0592	-.0042	.0054	-.0211	.0324
40.52	-7.77	2.0679	-.0606	-.0443	.0391	-.0157	.0217
40.49	-3.80	2.0163	-.0541	-.1345	.0317	-.0155	.0112
40.49	.16	2.0283	-.0537	-.1754	.0161	.0199	-.0051
40.48	4.12	2.0178	-.0548	-.1243	-.0135	.0375	-.0062
40.48	8.10	2.0413	-.0558	-.0172	.0150	.0419	-.0238
40.49	10.10	2.0504	-.0569	.0255	.0233	.0459	-.0294
40.50	15.08	2.0777	-.0625	.0450	-.1087	-.0071	-.0441
40.50	20.06	2.0731	-.0609	.0207	-.2013	-.0558	-.0679
40.49	29.93	1.9894	-.0754	.3072	-.2742	-.0252	-.0867

RUN 366		Q= 25.60 PSF		RN/FT= .600		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.43	29.95	2.3419	-.1012	.1565	-.2682	-.0788	-.0763
60.40	20.03	2.3062	-.1040	-.0027	-.1745	-.0728	-.0377
60.41	15.06	2.3476	-.1041	-.0302	-.0792	-.0395	-.0267
60.41	10.06	2.3561	-.1073	-.0752	.0001	-.0077	-.0144
60.42	8.09	2.4020	-.1139	-.0315	.0560	.0416	-.0121
60.42	4.16	2.3721	-.1126	-.0287	.0943	.0709	-.0178
60.42	.15	2.3929	-.1136	-.1102	.0657	.0374	-.0098
60.45	-3.74	2.4139	-.1166	-.0699	-.1136	-.0594	.0148
60.47	-7.75	2.4486	-.1190	.0661	-.0967	-.0699	.0195
60.47	-9.74	2.4180	-.1204	.0518	-.0359	-.0402	.0169

APPENDIX - Continued

RUN 367		Q= 25.70 PSF		RN/FT= .599		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.93	-9.76	2.3147	-.1167	-.3525	-.0361	-.0232	.0253
79.95	-7.73	2.3039	-.1175	-.3592	-.0478	-.0274	.0200
79.93	-3.79	2.3151	-.1186	-.3479	-.0409	-.0149	.0104
79.92	.19	2.3327	-.1222	-.3119	-.0227	-.0010	.0000
79.92	4.12	2.3221	-.1193	-.3439	.0120	.0131	-.0109
79.90	8.12	2.3111	-.1153	-.3644	.0198	.0235	-.0219
79.90	10.09	2.3033	-.1139	-.3570	.0068	.0247	-.0266
79.89	15.05	2.2743	-.1119	-.3256	-.0323	.0121	-.0373
79.88	20.03	2.2368	-.1039	-.3211	-.1003	-.0075	-.0466
79.87	29.91	2.1298	-.0931	-.2901	-.2817	-.0665	-.0642

RUN 369		Q= 90.60 PSF		RN/FT= 2.147		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.19	.22	.3030	.1084	.3954	-.0362	.0163	-.0006
50.39	.20	.4316	.0153	.5539	.0106	.0027	-.0002
60.17	.20	.4949	-.0157	.5857	-.0089	.0038	-.0004
65.02	.20	.5271	-.0159	.5959	-.0039	-.0021	-.0001
69.90	.18	.5677	-.0275	.5930	-.0022	-.0015	-.0002
74.88	.19	.5843	-.0199	.5150	-.0161	-.0021	-.0003
79.89	.20	.5908	-.0334	.4647	-.0252	-.0030	-.0006
85.05	.20	.6102	-.0517	.4136	-.0073	-.0007	-.0008
90.49	.19	.6610	-.0550	.3893	-.0167	-.0013	-.0005

APPENDIX - Continued

RUN 370		Q= 91.70 PSF		RN/FT= 2.144		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.98	-9.73	.7512	-.1336	.5487	.1154	.0111	.0025
79.97	-7.76	.7506	-.1332	.5667	.0611	.0036	.0013
79.94	-3.83	.7209	-.1221	.5661	-.0500	-.0030	-.0009
79.88	.15	.5997	-.0270	.4652	-.0212	-.0020	-.0007
79.90	4.11	.6179	-.0583	.4847	-.0902	.0017	-.0027
79.95	8.10	.7675	-.1108	.5163	-.0511	-.0199	-.0029
79.96	10.10	.7855	-.1166	.4987	-.0811	-.0346	-.0037
79.97	15.06	.7899	-.1272	.4891	-.1976	-.0532	-.0070
79.98	20.04	.8051	-.1359	.4459	-.2972	-.0647	-.0101
80.01	29.95	.7782	-.1339	.4268	-.3640	-.0599	-.0130

RUN 371		Q= 91.50 PSF		RN/FT= 2.133		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.33	30.01	.7264	-.0596	.4996	-.3437	-.0605	-.0080
60.34	20.02	.8380	-.0649	.5975	-.1161	-.0175	-.0082
60.32	15.06	.7703	-.0509	.6728	-.1242	.0191	-.0072
60.30	10.09	.7295	-.0322	.6462	-.0487	-.0064	-.0052
60.25	8.15	.6525	-.0097	.5712	-.1264	-.0199	-.0045
60.21	4.16	.5371	-.0087	.6016	-.0703	.0073	-.0027
60.21	.14	.4962	-.0131	.5957	-.0018	.0022	0.0000
60.23	-3.81	.5279	-.0060	.5936	.0455	-.0124	.0026
60.29	-7.80	.5931	-.0107	.5939	.1285	.0033	.0041
60.30	-9.77	.6279	-.0147	.5760	.1803	.0144	.0048

APPENDIX - Continued

RUN 372		Q= 90.00 PSF		RN/FT= 2.109		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.21	-9.77	.4180	.0902	.3739	.0859	.0375	.0039
40.17	-7.80	.3922	.1040	.3215	.0868	.0429	.0026
40.13	-3.83	.3509	.1147	.3214	.0243	.0275	.0015
40.11	.20	.2945	.1116	.3923	-.0336	.0158	-.0005
40.13	4.16	.3730	.1167	.3337	-.0712	-.0236	-.0013
40.13	8.17	.4022	.1026	.3412	-.0796	-.0418	-.0029
40.14	10.11	.4201	.0936	.3725	-.0617	-.0301	-.0040
40.29	15.07	.5971	.0719	.4130	-.0171	-.0112	-.0045
40.31	20.05	.6215	.0592	.4090	-.1290	-.0246	-.0061
40.32	30.04	.6313	.0415	.3172	-.3630	-.0588	-.0069

RUN 373		Q= 89.20 PSF		RN/FT= 2.092		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.21	.20	.4163	-.0280	.5763	-.0148	.0155	-.0005
50.48	.19	.5777	-.0732	.7368	.0023	.0034	-.0008
60.30	.20	.6630	-.0843	.7341	-.0119	.0027	-.0010
65.10	.19	.6772	-.0809	.7408	-.0101	-.0038	-.0004
69.97	.18	.6810	-.0590	.6614	-.0157	-.0048	-.0001
74.90	.18	.6798	-.0518	.5860	-.0040	-.0005	-.0002
79.97	.19	.6999	-.0554	.5656	-.0038	.0013	-.0006
85.16	.17	.7186	-.0575	.5226	-.0058	.0015	-.0007
90.55	.18	.7488	-.0614	.4957	-.0013	.0031	-.0007

APPENDIX - Continued

RUN 374		Q= 91.00 PSF		RN/FT= 2.107		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.99	-9.75	.7321	-.0632	.5641	.2943	.0080	.0079
79.98	-7.75	.7112	-.0593	.5761	.2657	.0018	.0062
79.96	-3.84	.7025	-.0568	.5734	.1356	-.0001	.0029
79.95	.16	.7071	-.0563	.5740	-.0034	.0012	-.0003
79.95	4.17	.7024	-.0544	.5734	-.1481	.0041	-.0042
79.94	8.11	.7490	-.0571	.5105	-.2091	-.0321	-.0064
79.95	10.11	.7560	-.0590	.4978	-.2632	-.0370	-.0078
79.97	15.06	.8187	-.0716	.4435	-.3229	-.0600	-.0106
79.98	20.05	.8237	-.0837	.4036	-.3795	-.0671	-.0141
80.01	29.91	.8718	-.1370	.4980	-.3239	-.0454	-.0209

RUN 375		Q= 91.00 PSF		RN/FT= 2.101		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.41	29.96	.9194	-.1238	.6321	-.2365	-.0520	-.0240
60.36	20.04	.8499	-.1073	.6659	-.1569	-.0456	-.0201
60.34	15.13	.8095	-.0958	.6368	-.1520	-.0569	-.0174
60.33	10.14	.7664	-.0963	.7350	-.1751	-.0176	-.0133
60.32	8.12	.7268	-.0898	.7344	-.1568	-.0104	-.0119
60.29	4.15	.6685	-.0825	.7269	-.1000	.0050	-.0067
60.30	.20	.6588	-.0850	.7336	-.0096	.0010	-.0007
60.32	-3.81	.6710	-.0832	.7317	.0602	-.0079	.0056
60.34	-7.80	.7018	-.0847	.7113	.1491	.0079	.0108
60.38	-9.80	.7723	-.0976	.7189	.1406	.0189	.0121

APPENDIX - Continued

RUN 376		Q= 90.10 PSF		RN/FT= 2.083		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.27	-9.78	.5322	-.0280	.5412	.0474	.0238	.0082
40.23	-7.79	.4967	-.0274	.5198	.0739	.0272	.0050
40.21	-3.82	.4699	-.0270	.5225	.0359	.0126	.0023
40.15	.18	.4155	-.0277	.5757	-.0166	.0154	-.0006
40.18	4.16	.4737	-.0272	.5228	-.0548	-.0120	-.0020
40.19	8.14	.4998	-.0279	.5270	-.0654	-.0269	-.0064
40.19	10.16	.5070	-.0243	.5238	-.0662	-.0190	-.0087
40.20	15.13	.5414	-.0208	.5082	-.1222	-.0278	-.0119
40.20	20.11	.5187	-.0134	.4586	-.2303	-.0455	-.0145
40.26	30.04	.6471	-.0253	.3625	-.3633	-.0613	-.0136

RUN 377		Q= 89.90 PSF		RN/FT= 2.075		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.43	.17	.6610	-.0714	.7961	-.0071	.0144	-.0005
50.55	.17	.7062	-.0512	.8358	.0032	.0036	-.0002
60.35	.17	.7790	-.0328	.7318	.0009	.0019	-.0001
65.12	.15	.7864	-.0298	.7279	.0030	-.0040	.0002
70.04	.16	.7979	-.0299	.6974	.0058	-.0033	.0002
74.96	.15	.8072	-.0327	.6484	.0096	.0019	-.0005
80.02	.16	.8309	-.0374	.6226	.0046	.0014	-.0006
85.19	.16	.8468	-.0408	.5865	-.0032	-.0004	-.0003
90.66	.16	.8776	-.0444	.5699	.0039	.0030	-.0001

APPENDIX - Continued

RUN 378		Q= 89.60 PSF		RN/FT= 2.067		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.01	-9.73	.8223	-.0387	.6327	.2918	-.0008	.0063
80.02	-7.77	.8372	-.0404	.6397	.2231	.0008	.0052
79.99	-3.78	.8290	-.0387	.6255	.1174	-.0001	.0024
79.98	.06	.8338	-.0368	.6236	.0048	.0003	.0001
79.98	4.14	.8283	-.0373	.6312	-.1165	.0046	-.0030
79.98	8.16	.8609	-.0402	.5747	-.1598	-.0248	-.0053
79.97	10.13	.8569	-.0397	.5558	-.1928	-.0316	-.0064
79.98	15.09	.8826	-.0437	.5206	-.2940	-.0535	-.0089
79.98	20.01	.8838	-.0480	.4596	-.3848	-.0665	-.0113
79.99	29.96	.9222	-.0599	.4593	-.3446	-.0365	-.0167

RUN 379		Q= 89.20 PSF		RN/FT= 2.055		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.39	30.01	.8841	-.0855	.6333	-.2993	-.0651	-.0253
60.37	20.06	.8949	-.0613	.6730	-.2114	-.0345	-.0168
60.36	15.07	.8757	-.0441	.6529	-.2456	-.0275	-.0133
60.36	10.13	.8446	-.0409	.6952	-.1770	-.0273	-.0092
60.35	8.11	.7936	-.0361	.7486	-.1768	.0026	-.0080
60.34	4.17	.7860	-.0343	.7348	-.0817	.0097	-.0048
60.33	.15	.7832	-.0335	.7364	.0030	.0016	.0000
60.35	-3.80	.7886	-.0345	.7351	.0799	-.0112	.0046
60.37	-6.89	.7923	-.0360	.7376	.1493	-.0040	.0071
60.38	-7.79	.7948	-.0368	.7401	.1651	-.0012	.0079
60.40	-9.80	.8291	-.0408	.7130	.1745	.0175	.0091

APPENDIX - Continued

RUN 380		Q= 88.30 PSF		RN/FT= 2.040		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.39	-9.78	.7056	-.0656	.7429	.0446	.0174	.0137
40.37	-7.79	.6946	-.0657	.7403	.0399	.0157	.0105
40.35	-3.80	.6726	-.0638	.7464	.0091	.0055	.0046
40.33	.16	.6586	-.0706	.7943	-.0050	.0148	-.0006
40.34	4.16	.6837	-.0638	.7430	-.0154	-.0079	-.0041
40.33	8.12	.6966	-.0674	.7507	-.0433	-.0162	-.0109
40.33	10.09	.6989	-.0678	.7439	-.0461	-.0110	-.0136
40.32	15.09	.7174	-.0664	.7251	-.0854	-.0108	-.0179
40.31	20.07	.7034	-.0627	.6706	-.1701	-.0264	-.0205
40.29	30.02	.6903	-.0513	.4509	-.3086	-.0630	-.0219

RUN 381		Q= 56.10 PSF		RN/FT= 1.336		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.24	.21	.6530	-.0687	.7952	-.0022	.0108	-.0003
50.40	.19	.7350	-.0522	.8368	-.0037	.0031	-.0003
60.20	.20	.8145	-.0338	.7569	.0026	-.0019	.0000
65.01	.19	.8282	-.0305	.7212	.0043	-.0035	.0000
69.89	.17	.8265	-.0289	.6842	.0029	-.0029	.0001
74.84	.20	.8398	-.0322	.6465	.0142	.0103	-.0007
79.89	.20	.8601	-.0360	.6191	.0096	.0084	-.0007
85.07	.19	.8795	-.0391	.6021	-.0005	.0031	-.0006
90.47	.19	.9256	-.0392	.6660	-.0173	-.0105	.0003

APPENDIX - Continued

RUN 382		Q= 56.30 PSF		RN/FT= 1.295		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.92	-9.74	.9291	-.0353	.7647	.1600	-.0750	.0092
79.89	-7.75	.9232	-.0358	.7516	.1133	-.0755	.0081
79.87	-3.82	.9126	-.0359	.7099	.0278	-.0621	.0052
79.85	.20	.8817	-.0348	.6698	-.0483	-.0351	.0015
79.84	4.13	.8787	-.0361	.6875	-.0532	.0428	-.0044
79.83	8.09	.8932	-.0384	.6970	-.1488	.0480	-.0072
79.89	10.09	.9306	-.0415	.7764	-.1236	.0831	-.0105
79.90	15.02	.9845	-.0486	.7775	-.1696	.0480	-.0126
79.90	20.03	.9605	-.0455	.6470	-.3360	-.0292	-.0119
79.92	29.95	1.0047	-.0560	.5824	-.3548	-.0713	-.0141

RUN 383		Q= 56.60 PSF		RN/FT= 1.293		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.24	29.96	.9225	-.0869	.7722	-.2921	-.0587	-.0237
60.22	20.08	.8924	-.0599	.8256	-.3920	-.0603	-.0169
60.22	15.10	.9088	-.0531	.8035	-.3041	-.0614	-.0124
60.20	10.13	.8323	-.0420	.8216	-.2194	-.0151	-.0088
60.19	8.11	.8252	-.0396	.7977	-.1800	-.0039	-.0074
60.19	4.12	.8152	-.0349	.7651	-.0884	.0009	-.0041
60.20	.17	.8033	-.0339	.7541	.0045	-.0022	.0000
60.21	-3.81	.8106	-.0344	.7539	.0951	-.0058	.0039
60.24	-7.81	.8180	-.0356	.7769	.2064	-.0054	.0078
60.25	-9.79	.8144	-.0373	.7945	.2485	.0038	.0090

APPENDIX - Continued

RUN 384		Q= 56.60 PSF		RN/FT= 1.288		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.22	-9.75	.6873	-.0658	.7474	.0684	.0150	.0127
40.22	-7.78	.7016	-.0668	.7349	.0236	.0243	.0096
40.19	-3.81	.6804	-.0649	.7360	-.0062	.0178	.0045
40.17	.17	.6452	-.0687	.7903	.0001	.0123	-.0005
40.17	4.12	.6812	-.0655	.7387	-.0157	-.0141	-.0035
40.17	8.11	.6957	-.0676	.7510	-.0492	-.0205	-.0101
40.17	10.10	.6893	-.0684	.7532	-.0762	-.0202	-.0134
40.17	15.03	.7125	-.0661	.7444	-.0945	-.0027	-.0187
40.15	20.04	.6938	-.0624	.7037	-.1723	-.0154	-.0208
40.17	29.94	.7177	-.0567	.5778	-.2492	-.0463	-.0223

RUN 385		Q= 56.40 PSF		RN/FT= 1.285		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.16	.21	.4102	-.0268	.5670	-.0146	.0092	-.0003
50.35	.20	.5985	-.0744	.7304	-.0102	.0000	-.0003
60.17	.20	.8325	-.1229	.8069	.0085	-.0008	-.0008
65.04	.19	.8923	-.1195	.7716	.0009	-.0022	-.0002
69.88	.19	.8599	-.0922	.6898	.0193	-.0045	.0005
74.78	.18	.7428	-.0552	.5847	-.0135	.0081	-.0010
79.84	.18	.7610	-.0587	.5675	.0031	.0113	-.0009
85.07	.18	.7925	-.0568	.6094	-.0376	-.0188	0.0000
90.46	.19	.8108	-.0583	.5921	-.0212	-.0076	-.0004

APPENDIX - Continued

RUN 386		Q= 56.10 PSF		RN/FT= 1.281		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.87	-9.77	.9107	-.0740	.6428	-.0219	-.0338	.0094
79.87	-7.73	.8929	-.0712	.6263	-.0689	-.0338	.0079
79.85	-3.78	.8620	-.0655	.5808	-.1243	-.0205	.0046
79.81	.19	.7576	-.0582	.5785	-.0249	-.0047	-.0005
79.79	4.12	.7740	-.0550	.6178	-.0590	.0443	-.0055
79.80	8.11	.8587	-.0668	.5836	-.0126	.0140	-.0082
79.82	10.07	.9119	-.0795	.7032	.0094	.0497	-.0113
79.84	15.05	.9211	-.0868	.7139	-.0924	.0311	-.0135
79.89	19.99	.9160	-.0914	.6813	-.2504	-.0154	-.0148
79.93	29.92	.9317	-.1263	.6200	-.3584	-.0837	-.0179

RUN 387		Q= 56.60 PSF		RN/FT= 1.286		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.25	29.95	.8909	-.1157	.7154	-.2775	-.0777	-.0206
60.23	20.09	.8344	-.1054	.7947	-.3568	-.0775	-.0192
60.21	15.09	.7893	-.0981	.7932	-.2934	-.0751	-.0162
60.21	10.13	.8106	-.1012	.8324	-.1940	-.0198	-.0124
60.21	8.09	.8167	-.1051	.8330	-.1221	-.0126	-.0097
60.21	4.12	.8322	-.1135	.8222	-.0379	-.0061	-.0060
60.22	.15	.8348	-.1236	.8067	.0067	.0003	-.0009
60.24	-3.80	.8139	-.1131	.8013	.0142	-.0024	.0054
60.25	-7.79	.7954	-.1021	.8050	.1059	.0057	.0092
60.26	-9.78	.7937	-.1023	.8098	.1581	.0123	.0113

APPENDIX - Continued

RUN 388		Q= 56.40 PSF		RN/FT= 1.282		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.17	-9.78	.5305	-.0329	.5394	.0393	.0341	.0062
40.16	-7.78	.5149	-.0325	.5283	.0171	.0375	.0042
40.14	-3.81	.4537	-.0265	.5218	.0245	.0190	.0017
40.17	.15	.4123	-.0264	.5671	-.0166	.0086	-.0003
40.17	4.13	.4518	-.0269	.5301	-.0515	-.0140	-.0018
40.17	8.13	.5103	-.0323	.5390	-.0483	-.0363	-.0049
40.17	10.10	.5497	-.0293	.5378	-.0412	-.0381	-.0072
40.17	15.05	.5276	-.0182	.5254	-.1253	-.0196	-.0132
40.16	20.06	.5093	-.0107	.4838	-.2407	-.0336	-.0151
40.22	29.97	.6795	-.0312	.5139	-.2567	-.0615	-.0127

RUN 389		Q= 56.10 PSF		RN/FT= 1.279		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.11	.18	.2832	.1061	.3970	-.0338	.0067	-.0004
50.33	.16	.4678	.0120	.5620	.0003	.0031	-.0002
60.14	.16	.7343	-.0589	.6500	.0114	.0032	-.0008
65.02	.16	.8027	-.0835	.6804	.0020	-.0035	-.0008
69.87	.17	.8361	-.0880	.6543	-.0149	-.0083	-.0003
74.82	.16	.8452	-.1127	.6200	-.0095	-.0023	-.0003
79.86	.15	.8618	-.1461	.6177	-.0054	.0057	.0001
85.07	.15	.8419	-.1094	.5598	-.0084	-.0081	.0004
90.45	.16	.8431	-.0623	.5142	.0011	-.0114	.0004

APPENDIX - Continued

RUN 390		Q= 55.90 PSF		RN/FT= 1.277		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.89	-9.72	.8942	-.1408	.7627	.0770	-.0778	.0082
79.89	-7.77	.9073	-.1384	.7522	.0330	-.0753	.0070
79.87	-3.84	.8775	-.1436	.6450	.0281	-.0233	.0030
79.85	.15	.8639	-.1454	.6157	-.0031	.0103	-.0003
79.84	4.13	.8835	-.1389	.6585	-.0519	.0409	-.0041
79.84	8.13	.8686	-.1267	.6740	-.1234	.0502	-.0067
79.87	10.10	.8823	-.1185	.6251	-.0783	.0221	-.0064
79.87	15.03	.8577	-.1245	.6306	-.1179	.0041	-.0085
79.88	20.02	.8765	-.1362	.6832	-.2460	-.0371	-.0088
79.90	29.93	.8766	-.1328	.5468	-.3587	-.1013	-.0094

RUN 391		Q= 56.50 PSF		RN/FT= 1.282		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.18	29.97	.7731	-.0550	.6264	-.3292	-.0703	-.0079
60.18	20.06	.8187	-.0440	.7695	-.2898	-.0505	-.0082
60.19	15.08	.7819	-.0461	.7776	-.2433	-.0279	-.0060
60.17	10.10	.7547	-.0350	.7335	-.0833	-.0035	-.0054
60.16	8.13	.7318	-.0315	.7087	-.0384	.0025	-.0049
60.16	4.14	.7394	-.0367	.6725	-.0014	.0082	-.0035
60.16	.16	.7327	-.0592	.6490	.0111	.0021	-.0006
60.17	-3.80	.7379	-.0482	.6590	-.0284	-.0151	.0028
60.18	-7.79	.7155	-.0340	.6784	.0242	-.0064	.0045
60.20	-9.79	.7150	-.0340	.6933	.0852	-.0018	.0049

APPENDIX - Continued

RUN 392		Q= 56.60 PSF		RN/FT= 1.284		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.14	-9.79	.4273	.0869	.3677	.0626	.0436	.0026
40.12	-7.77	.4057	.0992	.3656	.0688	.0338	.0023
40.08	-3.79	.3325	.1086	.3497	.0308	.0234	.0011
40.11	.20	.2860	.1072	.3983	-.0376	.0071	-.0005
40.11	4.18	.3166	.1087	.3781	-.0882	-.0106	-.0017
40.12	8.14	.3966	.0982	.3982	-.1129	-.0271	-.0028
40.13	10.15	.4449	.0881	.4074	-.0741	-.0485	-.0033
40.16	15.08	.6017	.0728	.4467	.0067	-.0021	-.0055
40.18	20.05	.6537	.0639	.4686	-.0910	-.0001	-.0073
40.20	30.01	.6622	.0338	.4635	-.3030	-.0413	-.0073

RUN 393		Q= 13.70 PSF		RN/FT= .332		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.05	.19	.4054	.1204	.3629	.0179	.0012	-.0001
50.22	.17	.7108	.0194	.6648	-.1075	.0660	-.0040
59.98	.16	.9629	-.0251	.7652	-.0163	.0141	-.0030
64.83	.15	1.0639	-.0624	.8415	-.0827	.0415	-.0019
69.72	.16	1.1585	-.1312	1.0051	-.0061	.0415	-.0016
74.65	.16	1.1740	-.1526	1.0018	.0089	.0236	-.0010
79.74	.15	1.1578	-.1526	.9037	-.0185	.0052	-.0002
84.92	.17	1.1365	-.1496	.7014	-.0868	.0287	-.0012
90.26	.16	1.0306	-.0804	.4889	-.0286	.0076	-.0003

APPENDIX - Continued

RUN 394		Q= 15.30 PSF		RN/FT= .349		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.72	-9.75	1.1188	-.1425	.7532	-.1833	.0125	.0055
79.71	-7.77	1.0955	-.1423	.7390	-.1912	.0092	.0049
79.71	-3.78	1.1321	-.1513	.8557	-.1094	.0159	.0012
79.70	.17	1.1455	-.1545	.9059	-.0183	.0050	.0001
79.69	4.12	1.1285	-.1550	.8328	.0247	.0214	-.0030
79.71	8.13	1.1413	-.1443	.7726	.0942	.0039	-.0047
79.70	10.11	1.1209	-.1394	.7649	.1210	-.0116	-.0062
79.69	15.05	1.0810	-.1229	.7180	.0973	-.0196	-.0075
79.68	20.02	1.0701	-.1349	.7122	-.0113	-.0444	-.0101
79.69	29.91	1.0171	-.1476	.7109	-.3837	-.0334	-.0141

RUN 395		Q= 15.20 PSF		RN/FT= .348		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.03	29.90	1.1023	-.0763	.9790	-.3126	-.0228	-.0124
60.00	20.05	1.1402	-.0705	.9796	.1143	-.0277	-.0095
60.00	15.03	1.1151	-.0750	.9886	.2337	.0008	-.0088
60.02	10.07	1.0887	-.0924	1.0290	.1748	.0211	-.0052
60.03	8.08	1.0800	-.0761	.9736	.1884	.0196	-.0025
60.02	4.10	.9941	-.0239	.8208	.1644	.0415	-.0017
60.03	.14	.9778	-.0292	.7719	-.0160	.0149	-.0027
60.05	-3.81	.9824	-.0134	.7907	.0151	-.0249	.0039
60.07	-7.73	1.0197	-.0288	.9686	-.1433	-.0476	.0043
60.08	-9.78	1.0733	-.0729	1.0307	-.1406	-.0154	.0041

APPENDIX - Continued

RUN 396		Q= 14.50 PSF		RN/FT= .342		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.09	-9.75	.5679	.1320	.5246	-.0153	.0027	.0106
40.07	-7.76	.5233	.1094	.4933	-.0336	.0003	.0076
40.05	-3.81	.4690	.1126	.3752	.0548	-.0242	.0047
40.04	.15	.4168	.1114	.3732	.0202	.0022	.0002
40.04	4.12	.4475	.1192	.4146	-.0973	.0537	-.0058
40.04	8.11	.5370	.1195	.5031	.0276	.0195	-.0080
40.04	10.06	.5655	.1464	.4761	-.0374	.0018	-.0109
40.06	15.06	.6318	.1413	.4944	-.1034	-.0244	-.0101
40.07	19.99	.7164	.1292	.5473	-.1193	.0072	-.0138
40.09	29.93	.8451	.0988	.9576	-.1722	.0535	-.0212

RUN 397		Q= 14.60 PSF		RN/FT= .345		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.05	.19	.5349	-.0119	.5460	.0144	.0225	-.0009
50.22	.19	.7889	-.0662	.8013	-.0038	.0518	-.0028
60.03	.18	1.0685	-.1103	.9373	-.0918	.0329	.0003
64.84	.19	1.0874	-.0978	.8889	-.1183	.0488	.0011
69.75	.19	1.0965	-.0796	.8326	-.0107	.0204	.0010
74.68	.17	1.1468	-.0923	.8490	-.0666	.0371	-.0012
79.73	.17	1.1115	-.0789	.6736	-.0939	.0366	-.0010
84.89	.19	1.0783	-.0685	.5714	-.0831	.0325	-.0009
90.28	.17	1.0586	-.0672	.5137	-.0406	.0146	-.0005

APPENDIX - Continued

RUN 398 Q= 15.30 PSF RN/FT= .354 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.70	-9.74	1.0591	-.0778	.6448	-.1236	.0356	.0075
79.70	-7.77	1.0579	-.0715	.6267	-.1578	.0386	.0057
79.69	-3.81	1.0597	-.0678	.6561	-.1792	.0529	.0017
79.71	.12	1.1038	-.0772	.6594	-.0978	.0331	-.0009
79.70	4.16	1.0873	-.0757	.6441	-.0259	.0013	-.0039
79.68	8.10	1.0220	-.0665	.6217	.0899	-.0122	-.0072
79.68	10.14	1.0402	-.0710	.6246	.0517	-.0156	-.0089
79.69	14.96	1.0832	-.0894	.6499	.0024	-.0390	-.0105
79.69	20.05	1.0995	-.1052	.7051	-.0934	-.0552	-.0137
79.69	29.94	1.0585	-.1362	.7541	-.3892	-.0258	-.0212

RUN 399 Q= 15.50 PSF RN/FT= .359 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.07	29.95	1.2009	-.1350	1.0388	-.2499	-.0255	-.0248
60.04	20.03	1.1736	-.1302	1.0694	.0629	-.0411	-.0208
60.05	15.07	1.1296	-.1303	1.0724	.1505	-.0179	-.0172
60.06	10.08	1.1621	-.1461	1.1349	.2100	.0079	-.0090
60.06	8.11	1.1594	-.1474	1.1307	.2621	.0254	-.0074
60.06	4.18	1.0453	-.0995	.8722	.0753	.0332	-.0017
60.07	.15	1.0445	-.1126	.9530	-.0875	.0478	-.0006
60.06	-3.84	1.0187	-.0928	.8428	-.0146	-.0161	.0024
60.09	-7.78	1.0696	-.1237	1.0355	-.1307	-.0052	.0042
60.10	-9.77	1.2080	-.1564	1.1787	-.1713	-.0089	.0064

APPENDIX - Continued

RUN 400 Q= 14.80 PSF RN/FT= .352 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.11	-9.76	.6530	-.0149	.6457	.0581	-.0091	.0129
40.09	-7.80	.6158	-.0171	.6344	.0191	-.0078	.0110
40.08	-3.77	.5573	-.0218	.5941	-.0288	.0030	.0051
40.07	.17	.5241	-.0137	.5469	.0177	.0257	-.0005
40.06	4.13	.5701	-.0176	.5962	.0237	.0264	-.0053
40.06	8.12	.6162	-.0122	.6691	.0017	.0307	-.0107
40.06	10.14	.6410	-.0074	.6903	-.0216	.0261	-.0121
40.08	15.05	.7044	-.0086	.6255	-.1010	-.0137	-.0112
40.08	20.05	.7553	-.0014	.6188	-.2360	.0133	-.0160
40.09	29.93	.7578	.0085	.9526	-.4047	.0469	-.0245

RUN 401 Q= 15.10 PSF RN/FT= .357 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.11	.19	.7311	-.0591	.7620	.0371	.0267	-.0011
50.27	.20	.8771	-.0465	.9210	-.0125	.0402	.0021
60.02	.20	.9886	-.0433	1.0049	.0218	.0362	.0041
64.85	.18	1.0296	-.0386	1.0125	.0007	.0189	.0030
69.72	.17	1.0432	-.0339	.9796	.0123	.0085	.0014
74.69	.17	1.0544	-.0281	.8789	-.0133	.0012	.0005
79.70	.18	1.0756	-.0238	.7063	-.0523	.0138	.0000
84.92	.17	1.0769	-.0270	.6232	-.0097	.0120	.0006
90.28	.17	1.1000	-.0340	.5672	-.0700	.0340	-.0005

APPENDIX - Continued

RUN 402		Q= 15.00 PSF	RN/FT= .357		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.70	-9.71	1.0887	-.0341	.6170	.0077	.0131	.0072
79.70	-7.77	1.0685	-.0323	.6207	-.0037	.0121	.0063
79.69	-3.81	1.0647	-.0270	.6351	-.0176	.0357	.0023
79.67	.12	1.0460	-.0252	.7017	-.0325	.0167	.0003
79.66	4.17	1.0540	-.0325	.6512	.0081	-.0398	-.0020
79.65	8.12	1.0639	-.0340	.6079	.0280	-.0213	-.0053
79.73	10.12	1.0786	-.0370	.6064	.0155	-.0248	-.0063
79.71	15.07	1.0816	-.0422	.6247	-.0877	-.0333	-.0091
79.71	20.04	1.0822	-.0461	.6298	-.2200	-.0332	-.0121
79.71	29.95	1.0697	-.0758	.7065	-.4095	-.0239	-.0169

RUN 403		Q= 15.20 PSF	RN/FT= .360		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.02	29.96	1.1508	-.1061	1.0122	-.3465	-.0284	-.0275
60.05	20.02	1.0672	-.0643	.9838	-.1803	-.0158	-.0179
60.04	15.07	1.0537	-.0572	.9768	-.0550	-.0008	-.0146
60.04	10.09	1.0311	-.0521	.9411	.0047	.0166	-.0112
60.03	8.13	1.0164	-.0495	.9594	.0352	.0388	-.0099
60.04	4.06	.9564	-.0473	1.0216	-.0316	.0721	-.0009
60.04	.18	.9602	-.0480	1.0161	.0100	.0364	.0036
60.05	-3.81	1.0012	-.0502	.9068	-.0569	-.0062	-.0006
60.06	-7.72	1.1023	-.0667	1.0486	-.0549	-.0208	.0047
60.05	-9.75	1.0673	-.0614	1.0395	-.0911	-.0235	.0110

APPENDIX - Continued

RUN 404		Q= 15.20 PSF		RN/FT= .361		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.08	-9.73	.8514	-.0703	.9494	-.0636	-.0267	.0117
40.07	-7.74	.7868	-.0691	.9138	-.0711	-.0158	.0086
40.06	-3.78	.7219	-.0677	.8318	-.0750	.0099	.0025
40.04	.21	.7179	-.0645	.7750	.0214	.0268	-.0016
40.09	4.15	.7769	-.0665	.8518	.0579	.0208	-.0055
40.09	10.14	.8821	-.0724	1.0118	.0716	.0417	-.0125
40.09	15.07	.8814	-.0732	.9766	-.0017	.0097	-.0140
40.09	8.12	.8458	-.0714	.9670	.0758	.0407	-.0104
40.08	20.00	.9763	-.0795	.9653	-.0483	.0107	-.0178
40.10	29.91	1.0030	-.0848	1.2249	-.1838	.0574	-.0271

RUN 405		Q= 24.30 PSF		RN/FT= .569		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.16	.20	.7061	-.0606	.7875	.0235	.0149	-.0006
50.32	.19	.7991	-.0503	.8796	.0041	.0278	-.0006
60.05	.18	.8924	-.0377	.8925	.0232	.0272	-.0008
64.88	.19	.9209	-.0300	.8591	-.0564	-.0293	-.0001
69.76	.18	.9588	-.0323	.8621	-.0597	-.0358	.0009
74.73	.17	1.0056	-.0329	.8770	-.0181	-.0091	.0003
79.76	.18	1.0180	-.0285	.7635	.0083	-.0054	.0003
84.97	.17	1.0307	-.0301	.6873	.0267	-.0137	.0009
90.38	.17	1.0718	-.0384	.6266	.0181	-.0098	.0004

APPENDIX - Continued

RUN 406		Q= 25.90 PSF		RN/FT= .595		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.76	-9.77	1.0730	-.0384	.6133	-.0019	.0083	.0078
79.76	-7.77	1.0732	-.0350	.6049	-.0222	.0071	.0068
79.75	-3.83	1.0178	-.0270	.7155	.0490	.0000	.0040
79.74	.20	1.0092	-.0283	.7567	.0081	-.0054	.0006
79.74	4.19	.9993	-.0309	.7532	-.0580	.0114	-.0035
79.77	8.12	1.0463	-.0356	.6593	.0188	.0058	-.0062
79.78	10.09	1.0540	-.0372	.6625	-.0059	.0088	-.0074
79.78	15.07	1.0677	-.0437	.6889	-.0960	.0048	-.0102
79.78	20.03	1.0765	-.0449	.6746	-.1978	-.0170	-.0121
79.78	29.94	1.0656	-.0656	.6412	-.3832	-.0348	-.0152

RUN 407		Q= 25.80 PSF		RN/FT= .598		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.11	29.96	1.1299	-.1011	.9969	-.2766	-.0543	-.0252
60.08	20.07	1.0144	-.0630	.9383	-.2905	-.0691	-.0156
60.05	15.07	.9581	-.0488	.8841	-.2861	-.0482	-.0123
60.03	10.10	.9020	-.0405	.8825	-.2489	-.0145	-.0091
60.04	8.16	.8917	-.0384	.8648	-.1963	-.0098	-.0073
60.05	4.16	.8707	-.0332	.8329	-.1003	-.0022	-.0034
60.06	.13	.8895	-.0378	.8790	.0163	.0180	-.0006
60.08	-3.79	.9270	-.0457	.9544	.0211	-.0499	.0008
60.11	-7.80	.9784	-.0496	1.0139	-.0197	-.0765	.0109
60.11	-9.77	.9937	-.0506	1.0196	.0316	-.0609	.0124

APPENDIX - Continued

RUN 408		Q= 25.90 PSF		RN/FT= .605		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.14	-9.76	.7902	-.0742	.9257	-.0283	-.0099	.0102
40.13	-7.69	.7418	-.0686	.8763	-.0099	.0003	.0062
40.11	-3.77	.6870	-.0581	.8004	-.0197	-.0074	.0030
40.09	.18	.6722	-.0574	.7625	.0074	.0112	-.0031
40.08	4.15	.7001	-.0553	.8126	-.0206	.0291	-.0076
40.10	8.08	.7504	-.0705	.9047	.0144	.0211	-.0090
40.13	10.10	.7094	-.0613	.7660	-.0773	-.0410	-.0119
40.12	15.03	.7070	-.0590	.7521	-.1436	-.0478	-.0161
40.12	20.06	.7529	-.0644	.7673	-.1556	-.0691	-.0170
40.15	29.96	.9101	-.0839	1.0146	-.1770	-.0096	-.0218

RUN 409		Q= 25.90 PSF		RN/FT= .609		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.10	.21	.4602	-.0210	.5596	-.0017	.0123	-.0002
50.31	.21	.6689	-.0738	.7556	-.0200	.0274	-.0008
60.07	.15	.9215	-.1121	.8576	.0056	.0566	.0005
64.90	.15	.9938	-.1276	.8840	-.0996	.0020	-.0010
69.76	.14	1.0042	-.1177	.8528	-.2060	-.0237	-.0005
74.70	.15	1.0294	-.1141	.8244	-.0853	-.0436	.0010
79.82	.14	1.0288	-.0865	.7288	-.0073	-.0016	.0000
84.93	.16	1.0219	-.0746	.5929	.0014	-.0091	.0001
90.35	.20	1.0181	-.0752	.5238	.0081	-.0092	.0002

APPENDIX - Continued

RUN 410		Q= 25.60 PSF	RN/FT= .608		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.73	-9.72	1.0023	-.0829	.6184	-.1149	.0176	.0082
79.79	-7.77	.9880	-.0753	.6065	-.1146	.0058	.0070
79.78	-3.81	.9707	-.0747	.6764	-.0829	-.0010	.0041
79.78	.15	1.0369	-.0848	.7293	.0065	-.0032	.0004
79.76	4.14	1.0089	-.0826	.6720	-.0316	.0113	-.0039
79.75	8.10	.9579	-.0713	.6605	.0466	.0158	-.0079
79.75	10.05	.9532	-.0747	.6738	.0032	.0256	-.0099
79.75	15.05	.9810	-.0893	.7293	-.0863	.0310	-.0131
79.76	20.06	1.0182	-.1103	.7871	-.0933	.0001	-.0126
79.76	29.94	1.0338	-.1355	.6396	-.2911	-.0708	-.0176

RUN 411		Q= 26.20 PSF	RN/FT= .620		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.10	29.94	1.0909	-.1287	.9708	-.2265	-.0668	-.0221
60.06	19.97	.9617	-.1156	.9319	-.2192	-.0902	-.0191
60.05	14.99	.9177	-.1053	.8794	-.1898	-.0735	-.0168
60.04	10.01	.8829	-.0959	.8583	-.1249	-.0512	-.0122
60.04	8.05	.9007	-.1035	.8815	-.0716	-.0426	-.0104
60.05	4.14	.9480	-.1194	.8701	.0008	-.0125	-.0046
60.06	.16	.9141	-.1152	.8840	-.0337	.0039	-.0019
60.07	-3.81	.9100	-.0960	.8943	-.0888	-.0470	.0043
60.11	-7.75	1.0441	-.1432	1.1240	-.0954	-.0479	.0073
60.12	-9.79	1.0650	-.1490	1.1535	-.1106	-.0406	.0106

APPENDIX - Continued

RUN 412		Q= 24.70 PSF		RN/FT= .605		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.09	-9.77	.5731	-.0268	.6601	.0368	.0060	.0104
40.07	-7.78	.5542	-.0276	.6206	.0385	.0140	.0078
40.05	-3.78	.5032	-.0233	.5724	.0124	.0021	.0036
40.04	.14	.4731	-.0206	.5505	.0106	.0113	.0001
40.04	4.09	.5170	-.0233	.5829	-.0362	.0134	-.0031
40.04	8.15	.5554	-.0236	.6433	-.0259	.0103	-.0080
40.04	10.13	.5713	-.0199	.6497	-.0366	.0152	-.0100
40.04	15.04	.6436	-.0137	.6572	-.1233	.0102	-.0118
40.04	20.03	.6003	-.0222	.5924	-.2270	-.0743	-.0112
40.06	29.97	.7214	-.0089	.7673	-.3044	-.0215	-.0191

RUN 413		Q= 25.40 PSF		RN/FT= .621		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.03	.09	.3672	.1048	.3742	-.0129	.0128	-.0002
50.22	.09	.6160	.0119	.5598	.0162	.0239	.0007
60.01	.14	.8466	-.0644	.7914	-.1112	.0549	-.0006
64.88	.14	.9372	-.1045	.8345	-.0712	.0472	-.0013
69.73	.16	.9600	-.1058	.7768	-.1790	-.0188	.0012
74.77	.15	.9884	-.1241	.7711	-.1796	-.0223	.0021
79.76	.14	1.0135	-.1462	.8235	-.0633	-.0009	.0006
84.91	.15	.9944	-.1447	.7237	-.0156	-.0057	.0004
90.36	.16	.9881	-.0850	.5040	.0095	-.0142	.0004

APPENDIX - Continued

RUN 414 Q= 25.20 PSF RN/FT= .622 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.81	-9.78	1.0432	-.1453	.7224	-.1477	-.0076	.0071
79.80	-7.79	1.0071	-.1395	.7359	-.0706	-.0416	.0064
79.80	-3.78	1.0216	-.1472	.7578	-.1471	-.0270	.0040
79.79	.18	.9992	-.1441	.8328	-.0464	-.0055	.0003
79.77	4.09	.9601	-.1365	.7679	-.0134	.0439	-.0041
79.76	8.04	1.0168	-.1382	.6991	.0424	.0227	-.0057
79.76	10.01	1.0142	-.1358	.6973	.0240	.0207	-.0063
79.76	14.98	.9773	-.1155	.7083	-.0150	.0214	-.0076
79.76	20.03	.9564	-.1377	.7595	-.0611	-.0003	-.0105
79.76	29.94	.9757	-.1454	.5848	-.2678	-.0787	-.0100

RUN 415 Q= 25.90 PSF RN/FT= .634 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.06	29.96	.9914	-.0673	.8750	-.2840	-.0671	-.0097
60.03	20.03	.9079	-.0578	.8682	-.2199	-.0598	-.0072
60.02	15.07	.8613	-.0536	.8545	-.1432	-.0076	-.0070
60.02	10.05	.8725	-.0517	.8272	-.0319	.0109	-.0056
60.03	8.12	.8951	-.0564	.8159	-.0064	.0306	-.0053
60.04	4.09	.9028	-.0804	.8883	-.0546	.0841	-.0038
60.04	.15	.8546	-.0668	.7915	-.1149	.0558	-.0003
60.05	-3.77	.8495	-.0258	.8113	-.1469	-.0401	.0036
60.08	-7.77	.9265	-.0670	.9855	-.1395	-.0464	.0046
60.09	-9.84	.8953	-.0763	1.0199	-.0520	-.0692	.0061

APPENDIX - Continued

RUN 416		Q= 25.10 PSF		RN/FT= .629		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.08	-9.72	.4807	.0990	.5131	-.0042	.0150	.0077
40.07	-7.80	.4265	.1039	.4593	.0431	.0150	.0065
40.05	-3.82	.3964	.1067	.3781	.0182	.0139	.0026
40.03	.16	.3600	.1044	.3801	-.0177	.0148	-.0002
40.03	4.14	.3952	.1148	.3880	-.0479	.0008	-.0028
40.02	8.13	.4233	.1092	.4694	-.0505	.0078	-.0068
40.03	10.10	.4655	.1066	.5080	-.0126	.0114	-.0078
40.04	20.07	.5880	.0644	.5297	-.2000	-.0680	-.0054
40.06	29.91	.6865	.0257	.6229	-.2689	-.0536	-.0062
40.02	15.01	.4971	.0772	.4741	-.2049	-.0588	-.0051

RUN 417		Q= 92.30 PSF		RN/FT= 2.182		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.37	.09	.7832	.0138	.8083	.0345	.0137	-.0025
50.58	.09	.8650	.0180	.8580	-.0038	.0042	-.0010
60.39	.09	.9072	.0206	.7585	-.0065	.0001	-.0002
65.22	.09	.9116	.0210	.7740	.0047	-.0035	.0000
70.09	.09	.9103	.0191	.7375	-.0021	-.0029	-.0002
75.01	.12	.9185	.0198	.6703	-.0050	.0025	-.0006
80.09	.13	.9345	.0180	.6593	-.0072	.0029	-.0006
85.26	.14	.9465	.0163	.6267	-.0067	.0042	-.0006
90.68	.16	.9455	.0164	.5940	-.0029	.0054	-.0006

APPENDIX - Continued

RUN 418 Q= 94.30 PSF RN/FT= 2.208 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.07	-9.74	.9199	.0145	.6540	.2191	.0067	.0052
80.07	-7.78	.9212	.0150	.6652	.1809	.0011	.0042
80.06	-3.79	.9360	.0171	.6650	.0905	.0002	.0019
80.05	.14	.9311	.0181	.6550	-.0021	.0028	-.0006
80.06	4.15	.9282	.0177	.6686	-.1029	.0080	-.0034
80.09	8.12	.9418	.0154	.6422	-.1496	-.0091	-.0052
80.09	10.08	.9507	.0137	.6141	-.1787	-.0251	-.0060
80.08	15.08	.9547	.0122	.5762	-.2813	-.0348	-.0084
80.08	20.06	.9522	.0057	.5260	-.3190	-.0470	-.0115
80.09	29.98	.9554	-.0067	.5267	-.3183	-.0216	-.0161

RUN 419 Q= 93.30 PSF RN/FT= 2.195 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.44	29.99	.9750	-.0047	.6910	-.2293	-.0417	-.0178
60.44	20.10	1.0372	.0024	.7299	-.1150	-.0303	-.0125
60.43	15.06	1.0304	.0086	.7395	-.0939	-.0340	-.0104
60.43	10.12	.9937	.0146	.7434	-.0985	-.0330	-.0072
60.42	8.10	.9565	.0168	.7711	-.1071	-.0130	-.0065
60.40	4.17	.9155	.0203	.7734	-.0550	.0077	-.0040
60.39	.14	.9155	.0206	.7702	-.0053	.0007	-.0001
60.41	-3.78	.9196	.0200	.7733	.0427	-.0081	.0035
60.44	-7.78	.9373	.0171	.7801	.1163	.0016	.0061
60.48	-9.81	1.0205	.0107	.7366	.0397	.0446	.0067

APPENDIX - Continued

RUN 420		Q= 91.60 PSF		RN/FT= 2.172		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.43	-9.80	.8495	.0086	.8103	-.0671	.0188	.0096
40.42	-7.80	.8093	.0096	.8020	-.0140	.0113	.0064
40.40	-3.82	.8021	.0127	.8112	-.0189	.0026	.0030
40.37	.13	.7910	.0128	.8085	.0383	.0118	-.0018
40.36	4.13	.7918	.0131	.8011	.0111	-.0019	-.0030
40.35	8.12	.8217	.0096	.8142	.0524	-.0115	-.0070
40.38	10.12	.8509	.0097	.8183	.0779	-.0067	-.0092
40.46	15.05	.9283	.0096	.7982	.0851	.0026	-.0142
40.47	20.01	.9697	.0057	.7974	-.0037	.0112	-.0179
40.43	29.99	.9102	.0014	.5965	-.2076	-.0397	-.0224

RUN 421		Q= 15.20 PSF		RN/FT= .363		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.09	.17	.8767	.0218	.7907	.0384	.0214	-.0012
50.23	.16	1.0205	.0186	.9048	-.0226	.0205	.0034
60.04	.15	1.0943	.0131	1.0368	.0069	.0282	.0028
64.90	.13	1.1155	.0114	1.0396	-.0158	.0187	.0019
69.75	.15	1.1312	.0117	1.0044	-.0167	.0094	.0005
74.75	.16	1.1416	.0140	.8957	-.0258	.0130	.0000
79.76	.17	1.1384	.0252	.7167	-.0306	.0118	.0002
84.95	.16	1.1572	.0234	.6533	-.0993	.0337	-.0014
90.42	.16	1.1622	.0213	.5885	-.0537	.0192	-.0006

APPENDIX - Continued

RUN 422		Q= 14.20 PSF	RN/FT= .348		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.78	-9.75	1.1926	.0124	.6646	-.0895	.0179	.0060
79.78	-7.77	1.1671	.0163	.6563	-.0592	.0090	.0047
79.77	-3.78	1.1605	.0198	.6581	-.0399	.0313	.0018
79.75	.16	1.1256	.0253	.7301	-.0270	.0029	-.0001
79.74	4.12	1.1376	.0185	.6660	.0155	-.0339	-.0020
79.73	8.14	1.1441	.0153	.6359	.0401	-.0130	-.0052
79.72	10.10	1.1482	.0112	.6541	.0081	-.0037	-.0076
79.72	15.07	1.1685	-.0021	.6928	.0126	-.0132	-.0097
79.73	19.98	1.1764	-.0078	.6768	-.0737	-.0306	-.0120
79.71	29.94	1.1379	-.0217	.6468	-.2941	-.0286	-.0155

RUN 423		Q= 14.30 PSF	RN/FT= .351		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.04	29.94	1.2168	-.0331	1.0643	-.2491	-.0173	-.0200
60.03	20.04	1.2418	-.0228	1.1134	.0383	-.0407	-.0138
60.03	15.06	1.2155	-.0224	1.1299	.1303	-.0229	-.0111
60.04	8.05	1.2048	-.0148	1.1006	.1648	.0114	-.0072
60.05	4.12	1.1032	.0049	1.0045	-.0044	.0551	-.0006
60.06	.18	1.0763	.0060	1.0390	.0151	.0278	.0029
60.08	-3.79	1.1395	.0018	.9390	-.0602	-.0052	-.0008
60.10	-7.78	1.2472	-.0171	1.1444	-.1747	-.0204	.0055
60.11	-9.74	1.2648	-.0230	1.1863	-.2020	-.0070	.0077

APPENDIX - Continued

RUN 424		Q= 14.30 PSF		RN/FT= .352		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.12	-9.75	1.0548	0.0000	1.0466	-.1276	-.0105	.0084
40.11	-7.77	.9889	-.0005	1.0059	-.0930	.0040	.0049
40.09	-3.83	.9082	.0069	.9000	.0272	.0163	.0001
40.08	.16	.8892	.0127	.7871	.0461	.0204	-.0007
40.08	4.09	.9323	.0066	.8964	.0745	.0150	-.0023
40.08	8.07	.9989	.0037	1.0262	.1462	.0172	-.0063
40.08	10.07	1.0585	.0036	1.0663	.1602	.0305	-.0098
40.07	15.04	1.0693	-.0036	1.0896	.1281	.0306	-.0117
40.08	20.00	1.1251	-.0107	1.1451	.1328	.0233	-.0140
40.07	29.93	1.2100	-.0256	1.3487	-.0837	.0851	-.0239

RUN 425		Q= 24.60 PSF		RN/FT= .594		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.13	.19	.8112	.0163	.8172	.0471	.0130	-.0015
50.26	.18	.9205	.0183	.9222	.0180	.0084	.0009
60.10	.17	1.0154	.0136	.9405	.0256	.0304	-.0009
64.89	.20	1.0166	.0148	.8986	-.0598	-.0362	-.0002
69.80	.17	1.0291	.0121	.8981	-.0645	-.0391	.0006
74.77	.17	1.0746	.0132	.9249	-.0220	-.0119	.0005
79.79	.18	1.0730	.0206	.8050	.0061	-.0067	-.0003
85.01	.17	1.1002	.0204	.7347	.0175	-.0167	.0000
90.43	.17	1.1247	.0173	.6541	.0189	-.0095	-.0002

APPENDIX - Continued

RUN 426 Q= 24.80 PSF RN/FT= .602 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.85	-9.80	1.1365	.0107	.6725	-.0421	-.0059	.0067
79.84	-7.81	1.0962	.0140	.6954	-.0200	-.0220	.0054
79.82	-3.84	1.0610	.0211	.7954	.0416	-.0303	.0032
79.82	.17	1.0607	.0192	.8014	.0060	-.0066	-.0005
79.80	4.10	1.0412	.0203	.7935	-.0534	.0175	-.0040
79.80	8.11	1.0920	.0159	.6927	.0142	.0147	-.0067
79.80	10.11	1.1041	.0119	.7055	-.0114	.0225	-.0082
79.80	15.01	1.1034	.0017	.7952	-.0849	.0463	-.0118
79.80	19.98	1.1188	-.0061	.8080	-.1047	.0098	-.0125
79.68	29.96	-.0065	-.2736	.2693	-.1606	-.0272	.0465

RUN 427 Q= 25.40 PSF RN/FT= .612 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.10	20.03	1.1190	-.0111	1.0112	-.1761	-.0677	-.0135
60.09	15.04	1.1084	-.0032	.9826	-.1229	-.0640	-.0101
60.07	10.10	1.0717	.0041	.9551	-.0848	-.0470	-.0075
60.06	8.16	1.0393	.0098	.9250	-.1006	-.0311	-.0065
60.06	4.14	.9827	.0172	.8698	-.0976	-.0051	-.0032
60.07	.11	1.0034	.0137	.9279	.0060	.0130	-.0011
60.10	-3.79	1.0423	.0063	.9989	.0124	-.0547	.0008
60.15	-7.73	1.1092	-.0048	1.1034	-.0921	-.0571	.0083
60.16	-9.78	1.1682	-.0111	1.1455	-.0908	-.0313	.0082

APPENDIX - Continued

RUN 428		Q= 25.20 PSF		RN/FT= .609		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.13	-9.77	.9754	-.0029	1.0249	-.0762	-.0026	.0070
40.11	-7.75	.9365	-.0012	.9779	-.0674	.0048	.0062
40.08	-3.81	.8583	.0119	.8790	-.0804	-.0020	.0051
40.07	.14	.8167	.0140	.8245	.0405	.0114	-.0014
40.07	4.10	.8775	.0104	.8989	.1082	.0175	-.0048
40.07	8.09	.8920	.0013	.9284	.0026	-.0163	-.0040
40.06	10.12	.8843	.0074	.8552	.0589	-.0372	-.0082
40.06	15.05	.9174	.0040	.8488	.0284	-.0320	-.0128
40.07	20.04	.9611	.0001	.8755	-.0065	-.0428	-.0145
40.08	29.91	1.1052	-.0276	1.1244	-.0399	.0107	-.0198

RUN 429		Q= 54.10 PSF		RN/FT= 1.287		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.28	.19	.7605	.0157	.8251	.0337	.0085	-.0019
50.43	.20	.8514	.0193	.8613	-.0058	.0023	-.0007
60.22	.18	.9164	.0221	.7770	-.0073	-.0033	-.0002
65.10	.19	.9175	.0221	.7527	.0007	-.0034	-.0001
69.92	.18	.9170	.0227	.7127	-.0023	-.0023	-.0004
74.90	.17	.9226	.0208	.6693	-.0049	.0031	-.0008
79.92	.17	.9311	.0191	.6414	-.0051	.0053	-.0009
85.11	.19	.9372	.0178	.6133	-.0078	.0029	-.0002
90.56	.19	.9601	.0181	.6198	.0003	.0174	-.0014

APPENDIX - Continued

RUN 430		Q= 59.20 PSF		RN/FT= 1.369		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.98	-9.69	.9916	.0166	.7908	.1137	-.0842	.0084
80.00	-7.76	.9954	.0179	.7782	.0700	-.0814	.0072
79.97	-3.80	.9742	.0203	.7176	.0384	-.0475	.0037
79.94	.17	.9386	.0199	.6501	-.0032	.0058	-.0009
79.93	4.14	.9394	.0213	.6732	-.0779	.0207	-.0036
79.94	8.09	.9622	.0210	.7427	-.1435	.0546	-.0074
79.93	10.09	.9920	.0179	.6933	-.1194	.0262	-.0079
79.94	15.04	1.0163	.0123	.6839	-.1874	.0139	-.0102
79.94	20.04	1.0103	.0073	.6713	-.2725	-.0197	-.0113
79.95	29.94	1.0292	-.0067	.6662	-.3125	-.0531	-.0140

RUN 431		Q= 59.00 PSF		RN/FT= 1.365		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.29	29.96	.9555	-.0018	.7043	-.2488	-.0448	-.0167
60.32	20.05	.9894	.0052	.8878	-.2999	-.0320	-.0131
60.31	15.01	.9846	.0076	.8641	-.2431	-.0453	-.0096
60.29	10.09	.9571	.0156	.8464	-.1635	-.0226	-.0072
60.28	8.11	.9310	.0187	.8252	-.1406	-.0060	-.0061
60.27	4.15	.9204	.0209	.7960	-.0721	-.0008	-.0036
60.27	.15	.9073	.0216	.7741	-.0030	-.0031	-.0002
60.29	-3.80	.9080	.0210	.7784	.0549	-.0041	.0027
60.32	-7.78	.9264	.0178	.8092	.1252	.0046	.0053
60.33	-9.80	.9501	.0133	.8138	.1003	.0277	.0060

APPENDIX - Continued

RUN 432		Q= 57.50 PSF		RN/FT= 1.344		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.25	-9.75	.8268	.0081	.8136	-.0758	.0185	.0086
40.23	-7.77	.8010	.0088	.8144	-.0435	.0173	.0061
40.21	-3.82	.7835	.0122	.8104	-.0264	.0078	.0028
40.20	.14	.7566	.0145	.8272	.0276	.0076	-.0016
40.20	4.12	.7923	.0120	.8096	.0082	-.0051	-.0032
40.21	8.12	.8274	.0083	.8333	.0440	-.0213	-.0068
40.22	10.09	.8526	.0084	.8282	.0773	-.0256	-.0095
40.23	15.43	.9209	.0107	.8081	.0580	.0047	-.0141
40.25	19.97	.9523	.0066	.8125	.0071	.0102	-.0181
40.23	29.89	.9334	0.0000	.7416	-.0952	-.0354	-.0218

RUN 433		Q=277.90 PSF		RN/FT= 6.370		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.65	.12	.4201	.0060	.4778	-.0361	.0423	-.0010
50.94	.20	.6504	-.0006	.5960	-.1382	.0367	.0003
60.51	.14	.7648	-.0072	.6109	.0180	.0183	-.0004
64.10	.17	.7737	-.0036	.6013	-.0112	.0168	.0001
70.63	.18	.7196	.0097	.5837	.0102	.0014	-.0002
75.61	.17	.7066	.0132	.5282	.0069	.0027	.0000
80.62	.19	.6993	.0140	.4753	.0116	-.0010	.0001
85.79	.17	.7089	.0145	.4484	.0185	-.0027	.0003
91.20	.18	.7132	.0280	.3887	.0032	-.0028	.0002

APPENDIX - Continued

RUN 434 Q=280.50 PSF RN/FT= 6.370 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.60	-9.78	.7338	.0111	.4687	-.0192	-.0015	.0023
80.59	-7.76	.7353	.0077	.4594	.0750	.0071	.0015
80.55	-3.83	.7038	.0124	.4748	.0765	-.0004	.0008
80.53	.11	.7001	.0144	.4735	.0137	-.0011	.0002
80.53	4.07	.6973	.0154	.4747	-.0831	-.0020	-.0008
80.51	8.09	.7244	.0159	.3889	-.0574	-.0258	-.0014
80.49	10.05	.7254	.0143	.3942	-.0212	-.0220	-.0017
80.66	15.14	.7857	.0021	.3831	-.0713	-.0593	-.0026
80.76	20.09	.8184	-.0146	.4639	-.1304	-.0552	-.0046
80.85	30.04	.7845	-.0299	.4684	-.3170	-.0724	-.0056

RUN 435 Q=273.20 PSF RN/FT= 6.257 MACH=0.20							
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
61.34	30.23	.8591	-.0258	.6323	-.3536	-.0863	-.0060
61.25	20.16	.9126	-.0113	.6643	-.1263	-.0550	-.0058
61.22	15.15	.8634	-.0032	.6504	-.0543	-.0344	-.0046
61.05	10.07	.7949	.0023	.6794	.0337	-.0006	-.0040
61.06	8.04	.7679	.0032	.6847	.0683	.0078	-.0036
61.00	4.08	.7663	-.0001	.6568	.0900	.0234	-.0025
60.25	.10	.7608	-.0059	.6079	.0129	.0136	.0000
61.09	-3.68	.7591	-.0029	.6476	-.1398	-.0092	.0030
60.98	-7.73	.8019	-.0038	.6560	-.1870	.0163	.0033
61.15	-9.76	.8175	-.0041	.6438	-.1604	.0325	.0034

APPENDIX - Continued

RUN 436		Q=267.10 PSF		RN/FT= 6.154		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.73	-9.94	.5523	.0047	.3925	.1240	.0467	.0033
40.71	-7.92	.5538	.0084	.3665	.0863	.0442	.0017
40.64	-3.86	.4801	.0106	.4092	.0127	.0240	.0005
40.58	.10	.4074	.0074	.4815	-.0160	.0324	-.0006
40.68	4.18	.4576	.0122	.4736	-.0836	.0021	-.0004
40.77	8.27	.5386	.0086	.4091	-.1317	-.0335	-.0020
40.78	10.29	.5550	.0036	.4321	-.1566	-.0390	-.0036
40.81	15.27	.6071	-.0016	.4792	-.2282	-.0366	-.0060
40.92	20.24	.6341	-.0099	.5541	-.2773	-.0307	-.0076

RUN 437		Q=210.40 PSF		RN/FT= 4.949		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _y	C _n	C _l
40.47	.10	.4001	.0074	.4731	-.0193	.0315	-.0005
50.82	.14	.6455	-.0039	.5895	-.1272	.0226	.0002
60.38	.12	.7380	-.0059	.5850	.0250	.0147	.0004
65.47	.15	.6846	.0049	.5830	.0046	.0067	.0003
70.35	.15	.6891	.0107	.5630	.0040	.0008	.0003
75.33	.15	.6902	.0133	.5269	.0120	.0005	.0002
80.36	.16	.6960	.0171	.4766	-.0159	-.0093	.0002
85.57	.16	.6981	.0230	.4363	.0399	.0000	.0000
90.89	.15	.7086	.0270	.3731	.0376	-.0047	.0001

APPENDIX - Continued

RUN 438		Q=225.50 PSF		RN/FT= 5.072		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
80.36	-9.74	.6800	.0113	.4568	.0547	-.0064	.0022
80.39	-7.78	.7057	.0104	.4732	.0907	-.0002	.0017
80.36	-3.82	.6864	.0147	.4749	.0646	-.0107	.0009
80.36	.16	.6916	.0167	.4754	-.0191	-.0090	.0000
80.36	4.12	.7030	.0215	.4700	-.0499	-.0027	-.0006
80.31	8.09	.7077	.0197	.4003	-.0346	-.0080	-.0012
80.31	10.09	.7106	.0178	.3689	-.0368	-.0174	-.0014
80.36	15.05	.7355	.0090	.3461	-.1636	-.0386	-.0028
80.53	20.04	.7920	-.0092	.4678	-.1576	-.0316	-.0049
80.62	29.97	.7865	-.0275	.4677	-.3053	-.0470	-.0062

RUN 439		Q=227.90 PSF		RN/FT= 5.073		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
61.02	30.13	.8352	-.0250	.5817	-.3274	-.0846	-.0061
61.01	20.11	.8919	-.0113	.6205	-.0970	-.0387	-.0058
60.93	15.08	.8222	-.0020	.6189	-.0458	-.0032	-.0050
60.82	10.06	.7671	.0045	.6335	.0304	.0163	-.0042
60.78	8.07	.7507	.0046	.6477	.0671	.0178	-.0036
60.79	4.05	.7296	.0021	.6357	.1233	.0191	-.0022
60.38	.10	.7447	-.0047	.5862	.0233	.0138	.0003
60.64	-3.79	.6821	-.0011	.5607	-.1418	-.0068	.0025
60.77	-7.67	.7857	-.0035	.6035	-.2047	.0225	.0031
60.80	-9.72	.8191	-.0022	.6019	-.1690	.0320	.0035

APPENDIX - Continued

RUN 440		Q=215.20 PSF		RN/FT= 4.913		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.60	-9.90	.5288	.0050	.3899	.1370	.0505	.0034
40.56	-7.86	.5261	.0079	.3600	.0939	.0504	.0018
40.52	-3.86	.4704	.0100	.3996	.0063	.0322	.0003
40.48	.17	.4022	.0073	.4760	-.0308	.0330	-.0006
40.52	4.20	.4486	.0114	.4517	-.0875	-.0097	-.0004
40.53	8.25	.5263	.0097	.3794	-.1286	-.0405	-.0020
40.54	10.29	.5273	.0055	.4083	-.1673	-.0422	-.0037
40.63	15.21	.5713	-.0011	.4733	-.2161	-.0368	-.0064
40.72	20.18	.6246	-.0126	.6267	-.1855	-.0112	-.0088
40.15	30.25	.7437	-.0394	.8272	-.3014	-.0193	-.0123

RUN 441		Q= 98.60 PSF		RN/FT= 2.254		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.21	.12	.3564	.0125	.4631	-.0255	.0201	-.0002
50.42	.15	.4581	.0097	.5275	.0256	-.0008	-.0007
60.22	.17	.5505	.0111	.5448	.0431	-.0127	.0005
65.04	.18	.6455	.0054	.5507	.0624	-.0053	.0006
69.94	.17	.6951	-.0003	.5511	.0160	-.0037	.0004
74.91	.18	.7295	.0027	.5097	-.0095	-.0138	.0000
79.94	.19	.7437	-.0016	.4805	.0181	-.0041	.0001
85.14	.18	.7306	-.0054	.4279	.0245	-.0019	.0002
90.55	.19	.7254	-.0023	.3800	.0195	-.0005	-.0002

APPENDIX - Continued

RUN 442		Q= 92.10 PSF		RN/FT= 2.156		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.96	-9.75	.6597	.0032	.4797	.0757	-.0106	.0022
79.97	-7.77	.6606	.0049	.4704	.0162	-.0143	.0018
79.99	-3.85	.7381	-.0054	.4787	.0900	-.0083	.0010
79.98	.14	.7395	-.0021	.4796	.0176	-.0041	.0002
79.97	4.15	.7376	-.0010	.4823	-.0578	.0047	-.0010
79.97	8.17	.7415	-.0003	.4875	-.1287	.0101	-.0018
79.95	10.11	.7194	.0064	.4328	-.0063	-.0111	-.0013
79.94	15.05	.6998	.0027	.3856	-.1891	-.0384	-.0027
79.95	20.01	.6993	-.0018	.3525	-.2972	-.0485	-.0041
79.96	29.91	.6917	-.0121	.3658	-.3784	-.0356	-.0056

RUN 443		Q= 92.70 PSF		RN/FT= 2.155		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.34	30.00	.7554	-.0101	.5187	-.3154	-.0514	-.0063
60.32	20.06	.7890	-.0035	.5743	-.1566	-.0003	-.0058
60.31	15.10	.7544	.0049	.6366	-.1187	.0229	-.0052
60.31	10.07	.7440	.0068	.6396	-.0210	.0112	-.0032
60.28	8.08	.6810	.0117	.6129	-.0231	.0178	-.0025
60.23	4.14	.5789	.0158	.5856	.0125	.0152	-.0013
60.23	.15	.5637	.0090	.5429	.0612	-.0154	.0007
60.27	-3.78	.5784	.0160	.5851	-.0648	-.0295	.0019
60.32	-7.76	.6840	.0097	.6013	-.0443	-.0169	.0028
60.31	-9.79	.7029	.0076	.6127	.0059	-.0151	.0035

APPENDIX - Continued

RUN 444		Q= 90.50 PSF		RN/FT= 2.123		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.24	-9.83	.4546	.0059	.4306	.0959	.0425	.0051
40.22	-7.80	.4654	.0104	.3539	.0909	.0513	.0020
40.19	-3.77	.4170	.0145	.3838	.0342	.0263	.0004
40.17	.22	.3474	.0117	.4625	-.0230	.0153	.0000
40.20	4.17	.4272	.0135	.3897	-.0670	-.0304	.0000
40.23	8.17	.4610	.0099	.3724	-.1133	-.0475	-.0027
40.23	10.19	.4467	.0075	.4234	-.1007	-.0316	-.0052
40.25	15.10	.4890	.0050	.4179	-.1315	-.0344	-.0073
40.35	20.06	.6365	-.0017	.4550	-.1607	-.0282	-.0075
40.33	30.08	.6137	-.0048	.3211	-.4004	-.0737	-.0088

RUN 445		Q= 14.70 PSF		RN/FT= .347		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.04	.15	.5647	.0291	.4062	-.1237	.0416	-.0023
50.24	.15	.7674	.0152	.5664	-.0423	.0130	-.0014
60.01	.16	.9535	.0005	.7483	-.0501	.0130	.0008
64.86	.15	1.0070	-.0171	.8265	-.1106	.0312	-.0005
69.69	.16	1.0271	-.0347	.8817	-.0909	.0616	-.0025
74.69	.15	1.0302	-.0370	.8676	-.0716	.0477	-.0022
79.68	.17	1.0038	-.0297	.7655	-.0966	.0458	-.0018
84.87	.15	.9388	-.0072	.5721	-.0881	.0199	-.0010
90.25	.15	.9300	.0087	.4623	-.0437	.0091	-.0008

APPENDIX - Continued

RUN 446		Q= 14.50 PSF	RN/FT= .345		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.70	-9.76	.9537	-.0189	.6374	-.1629	.0016	.0029
79.69	-7.75	.9451	-.0171	.6281	-.1630	-.0018	.0027
79.70	-3.80	.9474	-.0184	.6653	-.0904	-.0015	.0011
79.70	.14	.9816	-.0280	.7560	-.0958	.0428	-.0021
79.69	4.09	.9422	-.0191	.6922	.0245	.0246	-.0022
79.68	8.06	.9583	-.0195	.6726	.0421	.0320	-.0040
79.68	10.07	.9532	-.0171	.6640	.0835	.0203	-.0045
79.69	15.05	.9006	-.0112	.6271	.1460	.0098	-.0053
79.69	20.01	.9332	-.0198	.6205	.0167	-.0312	-.0047
79.69	29.92	.8842	-.0251	.5231	-.3201	-.0508	-.0058

RUN 447		Q= 14.80 PSF	RN/FT= .349		MACH=0.20		
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.00	29.93	1.0250	-.0339	.8898	-.3212	-.0338	-.0075
60.05	19.99	1.0737	-.0224	.9191	.1079	-.0323	-.0077
60.05	15.06	.9923	-.0197	.9272	.1966	.0040	-.0062
60.03	10.06	.9912	-.0232	.9119	.2153	.0306	-.0049
60.03	8.13	.9911	-.0282	.9107	.0670	.0167	-.0034
60.04	4.13	.9823	-.0181	.8172	.0495	.0294	-.0019
60.00	.14	.9502	-.0041	.7443	-.0611	.0138	.0003
60.01	-3.80	.9713	-.0088	.7553	-.0566	-.0155	.0009
60.02	-7.74	.9856	-.0210	.8846	-.1497	-.0141	.0029
60.01	-9.73	.9803	-.0258	.9258	-.1576	-.0011	.0038

APPENDIX - Continued

RUN 448		Q= 14.70 PSF		RN/FT= .348		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.03	-9.75	.6248	.0051	.6655	-.0366	-.0098	.0065
40.02	-7.77	.5575	.0110	.5940	.0109	-.0109	.0060
40.00	-3.81	.4963	.0162	.4867	.0617	-.0246	.0043
40.05	.15	.5538	.0208	.4134	-.1190	.0390	-.0022
40.04	4.08	.5524	.0201	.4884	-.1194	.0555	-.0045
40.04	8.09	.6000	.0167	.5716	-.0331	.0327	-.0059
40.04	10.08	.6389	.0105	.6510	.0115	.0232	-.0066
40.05	15.05	.6902	.0049	.6158	-.0861	-.0097	-.0060
40.05	19.98	.7920	-.0106	.7477	-.0531	.0033	-.0080
40.07	29.92	1.0017	-.0336	1.1140	-.1206	.0567	-.0137

RUN 449		Q= 24.80 PSF		RN/FT= .575		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.07	.20	.4550	.0172	.4501	.0889	-.0150	.0008
50.24	.18	.7283	.0064	.5727	-.0735	.0146	.0005
60.08	.20	.8458	-.0087	.7441	-.1013	.0429	-.0009
64.88	.20	.9016	-.0143	.7568	-.0850	.0181	-.0012
69.78	.19	.9028	-.0139	.7305	-.1556	-.0126	.0003
74.72	.19	.9123	-.0165	.7166	-.1697	-.0208	.0012
79.78	.19	.9451	-.0166	.7080	-.1234	.0035	.0004
84.97	.17	.9267	-.0079	.5924	-.0821	.0009	.0001
90.35	.17	.9022	.0069	.4834	-.0563	.0239	-.0010

APPENDIX - Continued

RUN 450		Q= 25.50 PSF		RN/FT= .589		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.75	-9.74	.9281	-.0200	.6386	-.1145	-.0204	.0034
79.75	-7.76	.9210	-.0179	.6375	-.0847	-.0325	.0032
79.75	-3.82	.9252	-.0160	.6621	-.1210	-.0308	.0023
79.74	.17	.9293	-.0178	.7067	-.1031	-.0051	.0002
79.78	4.12	.8581	-.0051	.6562	-.0146	.0383	-.0029
79.77	8.08	.8927	-.0096	.5939	.0380	.0227	-.0032
79.76	10.09	.9027	-.0122	.6116	.0147	.0212	-.0038
79.77	15.05	.8456	-.0103	.6734	.0363	.0311	-.0054
79.77	19.98	.8714	-.0134	.6810	-.0579	-.0034	-.0057
79.76	29.89	.8815	-.0254	.5275	-.2937	-.0553	-.0049

RUN 451		Q= 26.20 PSF		RN/FT= .597		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.07	29.91	.9677	-.0284	.8411	-.2655	-.0748	-.0062
60.09	20.02	.9077	-.0121	.8462	-.1765	-.0685	-.0063
60.05	15.04	.8221	-.0007	.8301	-.1543	-.0114	-.0060
60.04	10.09	.8087	-.0002	.7940	-.0376	.0018	-.0050
60.04	8.11	.8127	-.0023	.7680	-.0102	.0114	-.0042
60.05	4.13	.8306	-.0074	.7085	-.0559	.0321	-.0025
60.06	.19	.8323	-.0130	.7460	-.1014	.0387	-.0014
60.04	-3.77	.8678	-.0134	.7857	-.0855	-.0502	.0023
60.06	-7.73	.8695	-.0210	.9554	-.0883	-.0676	.0045
60.04	-9.74	.8700	-.0194	.9774	-.1324	-.0693	.0055

APPENDIX - Continued

RUN 452		Q= 24.80 PSF		RN/FT= .581		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.08	-9.75	.5475	-.0018	.6301	-.0397	.0071	.0052
40.06	-7.75	.4862	.0057	.5491	.0323	.0140	.0041
40.04	-3.81	.4277	.0142	.4931	.0342	.0004	.0016
40.03	.15	.4341	.0133	.4549	.0661	-.0098	.0004
40.03	4.15	.5079	.0177	.4598	-.0123	-.0007	-.0017
40.07	8.08	.4974	.0125	.5714	-.0664	.0186	-.0056
40.07	10.10	.5257	.0096	.5610	-.0981	-.0144	-.0051
40.07	15.04	.5421	-.0003	.5251	-.2373	-.0715	-.0054
40.08	20.04	.6038	-.0082	.5782	-.2442	-.0849	-.0064
40.13	29.93	.9227	-.0279	.9936	-.0873	.0202	-.0122

RUN 453		Q= 55.90 PSF		RN/FT= 1.295		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.12	.18	.3353	.0131	.4692	-.0223	.0084	.0001
50.32	.17	.4302	.0125	.5447	.0029	-.0005	-.0003
60.14	.17	.6912	.0009	.5845	.0005	-.0011	-.0001
64.97	.16	.6993	.0011	.5710	.0006	-.0044	.0002
69.90	.16	.7381	.0014	.5692	-.0124	-.0069	.0001
74.79	.15	.7411	.0005	.5217	-.0087	-.0045	0.0000
79.87	.15	.7426	-.0046	.4849	.0128	.0059	0.0000
85.04	.16	.7459	-.0063	.4516	.0066	.0085	-.0005
90.44	.16	.7532	.0016	.4575	-.0372	-.0226	.0006

APPENDIX - Continued

RUN 454		Q= 57.40 PSF		RN/FT= 1.335		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
79.86	-9.73	.7643	-.0037	.6437	.0916	-.0786	.0045
79.88	-7.74	.7811	-.0041	.6194	.0621	-.0772	.0040
79.84	-3.81	.7454	-.0043	.4971	.0783	-.0051	.0006
79.83	.16	.7470	-.0041	.4882	.0099	.0064	-.0004
79.82	4.18	.7445	-.0020	.5039	-.0679	.0280	-.0022
79.83	8.09	.7555	-.0020	.5531	-.1222	.0496	-.0038
79.83	10.10	.7609	-.0013	.5639	-.1643	.0488	-.0044
79.83	15.02	.7611	.0061	.5498	-.1076	.0232	-.0048
79.85	20.00	.7381	-.0052	.5889	-.2823	-.0184	-.0040
79.87	29.98	.7527	-.0121	.4606	-.3933	-.0861	-.0032

RUN 455		Q= 58.30 PSF		RN/FT= 1.347		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
60.18	30.00	.7335	-.0124	.5571	-.3059	-.0593	-.0051
60.20	20.03	.7740	0.0000	.6914	-.2658	-.0466	-.0047
60.19	15.06	.7550	.0025	.7188	-.1991	-.0121	-.0043
60.18	10.12	.7485	.0061	.6927	-.0477	.0033	-.0037
60.17	8.13	.7307	.0073	.6637	.0123	.0104	-.0033
60.16	4.14	.7257	.0040	.6126	.0507	.0118	-.0021
60.16	.16	.6899	.0014	.5793	.0151	.0007	.0001
60.19	-3.81	.6926	.0044	.5879	-.0084	-.0129	.0024
60.21	-7.81	.6834	.0096	.6390	.0204	-.0105	.0032
60.22	-9.76	.7087	.0073	.6732	.0302	-.0108	.0034

APPENDIX - Concluded

RUN 456		Q= 57.60 PSF		RN/FT= 1.339		MACH=0.20	
ALPHA	BETA	C _N	C _A	C _m	C _Y	C _n	C _l
40.16	-9.79	.4804	.0057	.4333	.0428	.0405	.0036
40.13	-7.77	.4399	.0086	.4184	.0684	.0351	.0022
40.10	-3.82	.3647	.0142	.4517	.0836	.0047	.0010
40.11	.18	.3364	.0129	.4705	-.0157	.0068	.0002
40.13	4.14	.4034	.0130	.4304	-.0628	-.0177	-.0003
40.14	8.18	.4910	.0050	.4275	-.1007	-.0487	-.0018
40.15	10.14	.5081	.0011	.4799	-.0925	-.0457	-.0036
40.18	15.10	.6366	.0054	.4872	-.0033	-.0115	-.0064
40.20	20.04	.6746	.0018	.4980	-.1081	-.0098	-.0080
40.20	30.00	.6341	-.0097	.4785	-.2958	-.0790	-.0079

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16. Abstract A 1/8-scale model of the X-29A airplane was tested in the Ames 12-Foot Pressure Wind Tunnel at a Mach number of 0.20 and Reynolds numbers of 0.13×10^6 to 2.00×10^6 based on a fuselage forebody depth of 0.4 ft. For the test series presented herein, the angle of attack ranged from 40° to 90° and the angle of sideslip ranged from -10° to 30° for the erect attitude. Tests with the model inverted covered angles of attack from -40° to -90° and angles of sideslip from -30° to 10° . Data were obtained for the basic design and for several forebody strakes. An alternate forebody design was also tested. The results provided information for selection of forebody strakes for compensation of Reynolds number effect on the 1/25-scale free-spinning model tested in the Langley Spin Tunnel.					
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